

DESCRIPTION

GAIT GENERATING DEVICE OF LEGGED MOBILE ROBOT AND CONTROL
DEVICE OF LEGGED MOBILE ROBOT

5 Technical Field

The present invention relates to a gait generating device and a control device suited not only to walking but also running of a legged mobile robot.

10 Background Art

Hitherto, a major object of generating gaits (desired gaits) for making a legged mobile robot, e.g., a bipedal mobile robot, carry out a traveling motion has been focused mainly on generating gaits (walking gaits) to make the robot carry out a smooth walking motion. In recent years, however, as the development of legged mobile robots advances, it has come to be desired to generate gaits that enable the robots not only to walk but to run also. Furthermore, it has come to be desired to generate gaits that enable the robots to move without trouble even on a slippery floor (so-called low- μ path) on which a sufficient frictional force cannot be produced.

Since the Chinese characters for "gait" include a character meaning "walking," the gait tends to be misinterpreted that the definition thereof is limited to walking. However, "gait" originally presents a concept that includes running, as it is used as a term indicating

a running mode of a horse, such as "trot."

The description will now be given of the difference in characteristics between walking and running.

5 A traveling mode that has an instant at which all legs are simultaneously floating is usually defined as running. This definition, however, does not necessarily make it possible to clearly distinguish between walking and running. For instance, most humans have instants at which all legs float at the same time in fast jogging, 10 whereas many humans have one of the legs always in contact with the ground in slow jogging. It is somehow perceptually unreasonable to define fast jogging as running and slow jogging as walking.

15 Fig. 51 shows a pattern of a vertical body position and a floor reaction force vertical component (a sum of floor reaction force vertical components acting on right and left legs) in typical running, and Fig. 52 shows a pattern of a vertical body position and a floor reaction force vertical component in typical walking.

20 A vertical body position/velocity means a vertical position of a representative point of a body and a velocity thereof. A horizontal body position/velocity means a horizontal position of a representative point of the body and a velocity thereof. A vertical body 25 position/velocity and a horizontal body position/velocity together will be referred to as body position/velocity.

Strictly speaking, the "floor reaction force vertical

component" should be described as "translational floor reaction force vertical component" to distinguish it from a moment component about a vertical axis of a floor reaction force; however, the term is too long, so that the
5 term "translational" will be omitted. Hereinafter, the "translational floor reaction force horizontal component" will be described as "floor reaction force horizontal component," omitting "translational."

10 First, attention will be focused on the movement of the body. In walking, the body reaches a highest level at the instant the body passes over a supporting leg, while it reaches a lowest level at this instant in running. In other words, the phase of a vertical motion pattern of the body reverses between walking and running.

15 Meanwhile, a floor reaction force remains relatively constant in walking, whereas it considerably varies in running, the floor reaction force reaching its maximum at the moment the body passes over a supporting leg.

Needless to say, the floor reaction force is zero at the
20 instant when all legs are simultaneously floating. More detailed observation reveals that a floor reaction force of a magnitude that is substantially proportional to a compression amount of the supporting leg is generated while running. In other words, it may be said that the
25 legs are used like springs to jump for traveling while running.

Slow jogging has the same body vertical motion phase

as that of typical running. In addition, slow jogging frequently has no instants at which all legs are simultaneously floating; however, even in this case, a floor reaction force reaches substantially zero, although not completely zero, at an instant when a supporting leg and an idle leg are switched.

Hence, distinguishing between walking and running on the basis of the aforesaid characteristics of the vertical motions of the body or floor reaction force patterns as described above may be more appropriate and perceptually reasonable, because slow jogging is regarded also as running.

In particular, to distinguish between the two on the basis of a most characteristic aspect, running may be defined as a traveling mode in which the floor reaction force becomes zero or substantially zero at the instant a supporting leg is switched, while walking may be defined as a traveling mode (a floor reaction force vertical component remaining relatively constant) other than that.

The present applicant has previously proposed, in PCT Kokai publication WO/02/40224, an art for generating freely and in real time a gait of a legged mobile robot that includes a floor reaction force while substantially satisfying dynamic balance conditions (This means the conditions of balance among gravity, an inertial force, and a floor reaction force of a desired gait. In a narrow sense, it means that the horizontal component of a moment

about a desired ZMP by the resultant force of gravity and an inertial force produced by a motion of a desired gait is zero. Detailed description will be given hereinafter). This art and a series of the control devices of legged mobile robots proposed by the present applicant in, for example, Japanese Unexamined Patent Application Publication No. 10-86081 and Japanese Unexamined Patent Application Publication No. 10-277969 can be applied to walking and also to running.

The present applicant has also proposed in PCT/JP02/13784 an art in which a dynamic model having high approximation accuracy is used to correct a provisional gait such that a translational floor reaction force horizontal component and a floor reaction force moment horizontal component fall within a predetermined permissible range, thereby generating a desired gait.

These arts, however, have not considered the magnitude of a floor reaction force moment vertical component about ZMP of a desired gait. Hence, there has been a danger in that the floor reaction force moment vertical component unduly increases and exceeds a frictional limit, leading to a spin. The term "spin" refers to a state in which a yaw angle (a rotational angle about a vertical axis) of an actual robot deviates from a desired yaw angular velocity.

When a robot walks on a floor surface having a high friction coefficient (in this case, at least one leg is

always in contact with the ground), a floor reaction force vertical component is always substantially equivalent to a robot's own weight, thus providing a higher limit of a frictional force (i.e., the floor reaction force moment vertical component). This makes it difficult for a spin to occur.

In running, however, the floor reaction force vertical component becomes zero or substantially zero, and in this case, therefore, the limit of a moment vertical component of the frictional force of a floor surface becomes zero or substantially zero even if a friction coefficient is high. Hence, there has been a danger in that the floor reaction force moment vertical component of a desired gait exceeds a limit, resulting in a spin and a fall.

Further, in the case of walking also, there has been a danger of spinning and falling if a floor has a low friction coefficient.

Meanwhile, the present applicant has previously proposed an arrangement, in which an arm is swung so as to cancel a moment vertical component generated by anything other than arms in a desired gait, in an embodiment described in, for example, PCT application PCT/JP02/13596.

In this case, the moment vertical component of a desired gait is substantially zero. However, if legs are briskly swung to move, then the arms will be also briskly swung.

Generally, the mass of an arm in a human-type robot is smaller than the mass of a leg. Accordingly, it is necessary to swing arms more briskly than legs in order to fully cancel a moment vertical component.

5 However, there is a restriction in the range of arm motion, and there are also restrictions in torque and velocity of arm actuators. Hence, there have been some cases where a moment vertical component cannot be fully canceled by arms when a robot moves while briskly swinging
10 its legs.

 Furthermore, there has been a danger in that, if arms are swung to cancel out a moment vertical component produced by anything other than arms in a desired gait, then the center of arm swing is gradually offset, causing
15 the swings of the right and left arms to be asymmetrical. Specifically, to make a left turn, if a robot swings its arms to fully offset a moment vertical component generated by anything other than arms, then the left arm is swung more toward the front and swung less toward the rear,
20 while the right arm is swung less toward the front and swung more toward the rear in order to offset the change in an angular momentum caused by the legs and the body having turned to the left. This may cause the left arm to reach a motion limit of the swing toward the front, and
25 the right arm to reach a motion limit of the swing toward the rear.

 Furthermore, if a motion is made to correct the

center of the arm swinging so as to prevent the swings of the right and left arms from becoming asymmetrical, then a floor reaction force moment vertical component is generated. This in turn causes a floor reaction force moment vertical component of a desired gait to exceed a limit, possibly causing the robot to spin.

Accordingly, an object of the present invention is to provide a gait generating device and a control device which solve the problems described above and which are capable of generating a further ideal gait regardless of gait types, such as walking and running, and a friction condition of a floor surface.

More specifically, an object of the present invention is to provide a gait generating device and a control device capable of generating gaits that make it possible to prevent a robot from spinning or falling from a spin, considering limitation of a moment vertical component of the force of a friction between the robot and a floor surface. Another object is to provide a gait generating device and a control device capable of generating a gait motion pattern that satisfies a dynamic balance condition even in a leg-floating period or even if the limit of a moment vertical component of a frictional force is extremely low. Still another object is to prevent lateral asymmetry of a desired gait from increasing so as to secure continuity of a motion.

Disclosure of Invention

According to a first invention of a gait generating device of a legged mobile robot in accordance with the present invention,

5 there is provided a gait generating device for generating a desired gait of a legged mobile robot that travels by moving a plurality of legs extended from its body, comprising:

 permissible range setting means for setting a
10 permissible range of a restriction object amount, the restriction object amount being a vertical component of a floor reaction force moment or a component of the floor reaction force moment in floor surface normal line direction, or a vertical component of an angular momentum
15 changing rate of the robot or a component of the angular momentum changing rate in floor surface normal line direction, to be applied to the robot;

 provisional instantaneous value determining means for determining a provisional instantaneous value of a desired
20 motion constituting the desired gait;

 model calculating means for supplying at least a provisional instantaneous value of the desired motion to a dynamic model that indicates a relationship between a motion of the robot and the restriction object amount so
25 as to determine an instantaneous value of a model restriction object amount as an output of the dynamic model; and

desired instantaneous value determining means for
determining an instantaneous value of a desired motion by
correcting the provisional instantaneous value of the
desired motion such that at least the instantaneous value
5 of the model restriction object amount falls within the
permissible range.

According to the first invention, an instantaneous
value of a desired motion is determined by correcting the
provisional instantaneous value of the desired motion such
10 that the instantaneous value of the model restriction
object amount as an output of the dynamic model falls
within the permissible range. In other words, the
provisional instantaneous value of the desired motion is
corrected such that the instantaneous value of the
15 restriction object amount that balances with the
instantaneous value of the desired motion after a
correction on the dynamic model falls within the
permissible range when the instantaneous value of the
desired motion after the correction is supplied to the
20 dynamic model. This makes it possible to generate a
motion of a desired gait that allows a restriction object
amount, such as a floor reaction force moment vertical
component, to fall within a permissible range. This means
that an instantaneous value of a desired motion is
25 determined, considering the limitation of a frictional
force moment vertical component on the dynamic model.
Thus, a desired gait can be generated that makes it

possible to prevent the robot from spinning and falling caused by the spinning. Moreover, it is not required to always maintain the restriction object amount to zero or substantially zero as long as a restriction object amount remains within a permissible range, thus making it possible to generate a desired gait that prevents the motion of a certain part of the robot from becoming unduly intense.

Basically, a dynamic model with high approximation accuracy is preferably used.

In the first invention, the desired instantaneous value determining means preferably determines an instantaneous value of a floor reaction force moment that corresponds to a restriction object amount that substantially balances with the instantaneous value of the desired motion on the dynamic model as an instantaneous value of a desired floor reaction force moment constituting the desired gait (a second invention).

With this arrangement, it is possible to determine an instantaneous value of a desired floor reaction force moment with high dynamic accuracy with respect to an instantaneous value of a desired motion.

In these first and second inventions, the desired instantaneous value determining means preferably comprises a perturbation model representing a relationship between a perturbative motion of the robot and a perturbation portion of a restriction object amount, means for

determining a perturbation model manipulated variable for manipulating the perturbation portion of the restriction object amount of the perturbation model on the basis of at least the instantaneous value of a model restriction

5 object amount determined by the model calculating means and the permissible range, means for determining a correction amount of the desired motion by supplying the determined perturbation model manipulated variable to the perturbation model, and

10 means for determining an instantaneous value of the desired motion by correcting the provisional instantaneous value of the desired motion on the basis of the correction amount (a third invention).

In other words, the high linearity of the
15 perturbation model permits easier calculation processing of a proper correction amount of a desired motion to make the restriction object amount fall within a permissible range and also permits easier processing of correcting a provisional instantaneous value of the desired motion on
20 the basis of the correction amount.

In the third invention, the means for determining the perturbation model manipulated amount preferably comprises means for determining an estimated value of the
restriction object amount when it is assumed that the
25 perturbation model manipulated amount is zero on the basis of at least an instantaneous value of a model restriction object amount determined by the model calculating means,

and means for comparing the determined estimated value with the permissible range to determine a restricted restriction object amount that has been restricted to fall within the permissible range on the basis of the comparison, wherein the perturbation model manipulated variable is determined on the basis of at least the difference between the instantaneous value of the model restriction object amount determined by the model calculating means and the restricted restriction object amount (a fourth invention).

According to the fourth invention, an estimated value of the restriction object amount when it is assumed that the perturbation model manipulated amount is zero, that is, when a perturbation portion of a restriction object amount additionally generated for correcting a provisional instantaneous value of a desired motion on the basis of a perturbation model is set to be zero, is determined on the basis of at least the instantaneous value of the model restriction object amount, and a restricted restriction object amount is determined on the basis of the comparison between the estimated value and a permissible range. In this case, an estimated value of a restriction object amount may be determined, considering gyro effect. The restricted restriction object amount is preferably determined to be a value as close to an estimated value of a restriction object amount as possible within the permissible range. And, a perturbation model manipulated

variable is determined on the basis of at least the difference between the instantaneous value of the model restriction object amount and the restricted restriction object amount. This makes it possible to properly
5 determine a perturbation model manipulated variable that prevents a restriction object amount from exceeding a permissible range.

The third invention further preferably comprises means for determining a required value of the perturbation
10 model manipulated variable on the basis of at least a state amount of the perturbation model, wherein the means for determining the perturbation model manipulated variable determines a perturbation model manipulated variable to be supplied to the perturbation model on the
15 basis of at least an instantaneous value of a model restriction object amount determined by the model calculating means, the permissible range, and the required value (a fifth invention).

With this arrangement, the perturbation model
20 manipulated variable is determined, considering a required value of a state amount of a perturbation model (a rotational angle of a rotor constituting an element of the perturbation model and an angular velocity thereof, etc.) in addition to the permissible range and the instantaneous
25 value of a model restriction object amount. This makes it possible to prevent a state amount of the perturbation model from considerably deviating from a state amount

corresponding to the required value, thereby preventing an improper correction amount of a desired motion from being determined.

In the fifth invention, the means for determining a
5 required value of the perturbation model manipulated
variable sequentially determines the required value
according to a feedback control law based on a deviation
between a state amount of the perturbation model and a
desired value for the state amount (a sixth invention).

10 According to the sixth invention, a perturbation
model manipulated variable is determined such that a state
amount of a perturbation model is substantially maintained
in the vicinity of a certain desired state amount. Thus,
a correction amount of a desired motion determined by the
15 perturbation model can be set to be ideal for a
restriction object amount to fall within a permissible
range while stably maintaining the state of the
perturbation model.

Furthermore, in the fifth and sixth inventions, the
20 means for determining the perturbation model manipulated
variable comprises means for determining an estimated
value of the restriction object amount when it is assumed
that the perturbation model manipulated variable has been
matched with the required value on the basis of at least
25 an instantaneous value of a model restriction object
amount determined by the model calculating means and the
required value and means for comparing the determined

estimated value with the permissible range to determine a restricted restriction object amount that has been restricted to fall within the permissible range on the basis of the comparison, wherein the perturbation model manipulated variable is determined on the basis of at least the difference between the instantaneous value of the model restriction object amount determined by the model calculating means and the restricted restriction object amount (a seventh invention).

With this arrangement, first, an estimated value of a restriction object amount when it is assumed that the perturbation model manipulated variable has been matched with the required value, that is, when it is assumed that only the required value has been supplied to a perturbation model, is determined on the basis of at least an instantaneous value of the model restriction object amount and the required value, and a restricted restriction object amount is determined on the basis of the comparison between the estimated value and a permissible range. In this case, the estimated value of a restriction object amount may be determined, considering gyro effect. The restricted restriction object amount is preferably determined to be a value as close as possible to an estimated value of a restriction object amount within the permissible range. And, a perturbation model manipulated variable is determined on the basis of at least the difference between the instantaneous value of

the model restriction object amount and the restricted
restriction object amount. This makes it possible to
properly determine a perturbation model manipulated
variable that prevents a restriction object amount from
5 exceeding a permissible range and also to secure stability
of the perturbation model.

In the aforesaid fourth to seventh inventions, the
desired instantaneous value determining means preferably
determines an instantaneous value of a floor reaction
10 force moment corresponding to the restricted restriction
object amount as an instantaneous value of a desired floor
reaction force moment constituting the desired gait (an
eighth invention).

With this arrangement, a restriction object amount
15 corresponding to the instantaneous value of a desired
floor reaction force moment securely falls within a
permissible range.

In the aforesaid fourth to eighth inventions, the
desired instantaneous value determining means may comprise
20 means for additionally supplying a correction amount of
the desired motion to the dynamic model (a ninth
invention).

With this arrangement, a correction amount of a
desired motion is additionally supplied to the dynamic
25 model, so that a restriction object amount balancing with
an instantaneous value of the desired motion can be
directly determined from the dynamic model. This permits

easier processing for determining an estimated value of the restriction object amount.

In this ninth invention, the desired instantaneous value determining means preferably determines an instantaneous value of a floor reaction force moment corresponding to the restricted restriction object amount as an instantaneous value of a desired floor reaction force moment constituting the desired gait (a tenth invention).

With this arrangement, a restriction object amount corresponding to the instantaneous value of a desired floor reaction force moment securely falls within a permissible range.

In the aforesaid third to tenth inventions, the perturbation model is preferably a model representing a relationship between a perturbative motion for perturbing a vertical component or a component in floor surface normal line direction of an angular momentum changing rate of the robot and the perturbation portion of a restriction object amount (an eleventh invention).

With this arrangement, a correction amount of a desired motion for making the restriction object amount fall within a permissible range can be properly determined.

In the eleventh invention, the perturbative motion is ideally a perturbative motion for maintaining the center-of-gravity position of the robot substantially constant (a twelfth invention).

With this arrangement, a correction of a desired motion by a perturbation model can be made without influencing a translational floor reaction force of a robot.

5 Further, in the aforesaid eleventh and twelfth inventions, the perturbative motion is preferably a perturbative motion of a body of the robot and/or an arm extended from the body (a thirteenth invention).

10 This arrangement permits easier processing for calculating a correction amount of a desired motion.

According to a fourteenth invention of a gait generating device of a legged mobile robot in accordance with the present invention,

15 there is provided a gait generating device for generating a desired gait of a legged mobile robot that travels by moving a plurality of legs extended from its body, comprising:

permissible range setting means for setting a permissible range of a restriction object amount, the
20 restriction object amount being a vertical component of a floor reaction force moment or a component of the floor reaction force moment in floor surface normal line direction, or a vertical component of an angular momentum changing rate of the robot or a component of the angular
25 momentum changing rate in floor surface normal line direction, to be applied to the robot;

desired floor reaction force provisional

instantaneous value determining means for sequentially
determining a provisional instantaneous value of at least
a desired floor reaction force among a desired motion and
a desired floor reaction force constituting the desired
5 gait;

first model calculating means for supplying at least
a provisional instantaneous value of the desired floor
reaction force to a first dynamic model that indicates a
relationship between a motion of the robot and a floor
10 reaction force so as to determine a provisional
instantaneous value of a desired motion as an output of
the first dynamic model;

second model calculating means for supplying at least
a provisional instantaneous value of the desired motion to
15 a second dynamic model that indicates a relationship
between a motion of the robot and the restriction object
amount so as to determine an instantaneous value of a
model restriction object amount as an output of the second
dynamic model; and

20 first model input correcting means for determining a
floor reaction force moment correction amount of a desired
floor reaction force such that at least the instantaneous
value of the model restriction object amount falls within
the permissible range, and for additionally supplying the
25 determined floor reaction force moment correction amount
to the first dynamic model,

wherein a desired instantaneous value of the desired

motion is determined on the basis of at least an input of the second dynamic model.

According to the fourteenth invention, a floor reaction force moment correction amount of a desired floor reaction force is determined such that the instantaneous value of a model restriction object amount as an output of a second dynamic model falls within a permissible range, and the determined floor reaction force moment correction amount is additionally supplied to the first dynamic model.

Hence, an instantaneous value of a desired motion that allows the restriction object amount to fall within a permissible range can be obtained on the basis of at least an input of the second dynamic model. This means that an instantaneous value of a desired motion, which is an input to the second dynamic model, is determined through the intermediary of the first dynamic model such that a restriction object amount occurring on the second dynamic model falls within a permissible range. Therefore, it is possible to generate a motion of a desired gait that causes a restriction object amount, such as a floor reaction force moment vertical component, fall within the permissible range. This means that an instantaneous value of a desired motion is determined, considering the limitation of a vertical component of a frictional force moment on the dynamic models. Thus, a desired gait can be generated that makes it possible to prevent a robot from spinning and falling from the spinning. In addition, it

is not required to always maintain the restriction object amount to zero or substantially zero as long as a restriction object amount remains within a permissible range, thus making it possible to generate a desired gait that prevents the motion of a certain part of the robot from becoming unduly intense.

Ideally, the aforesaid second dynamic model basically has higher approximation accuracy than the first dynamic model.

The fourteenth invention preferably comprises means for determining an instantaneous value of a floor reaction force moment that substantially corresponds to the instantaneous value of the model restriction object amount output by the second dynamic model as an instantaneous value of a desired floor reaction force moment constituting the desired gait (a fifteenth invention).

This arrangement makes it possible to determine an instantaneous value of a desired floor reaction force moment with high dynamic accuracy with respect to an instantaneous value of a desired motion.

Further, in the aforesaid fourteenth and fifteenth inventions, preferably, the first model input correcting means comprises means for estimating, on the basis of at least an instantaneous value of a model restriction object amount determined by the second model calculating means, an estimated value of an instantaneous value of a model restriction object amount output by the second dynamic

model if it is assumed that at least a floor reaction
force moment correction amount of the desired floor
reaction force is zero, and means for comparing the
estimated value of an instantaneous value of the model
restriction object amount with the permissible range to
5 determine a restricted restriction object amount that has
been restricted to fall within the permissible range on
the basis of the comparison, wherein the floor reaction
force moment correction amount is determined on the basis
10 of at least the difference between the instantaneous value
of the model restriction object amount determined by the
second model calculating means and the restricted
restriction object amount (a sixteenth invention).

According to the sixteenth invention, first, an
15 estimated value of a restriction object amount when it is
assumed that the correction amount of a floor reaction
force moment is zero, is determined on the basis of at
least an instantaneous value of the model restriction
object amount, and a restricted restriction object amount
20 is determined on the basis of the comparison between the
estimated value and a permissible range. In this case,
the estimated value of a restriction object amount may be
determined, considering gyro effect. The restricted
restriction object amount is preferably determined to be a
25 value as close as possible to an estimated value of a
restriction object amount within the permissible range.
And, a floor reaction force moment correction amount is

determined on the basis of at least the difference between the instantaneous value of the model restriction object amount and the restricted restriction object amount. This makes it possible to determine a proper floor reaction
5 force moment correction amount that permits prevention of a restriction object amount from exceeding a permissible range.

The fourteenth and the fifteenth inventions further preferably comprises means for determining a required
10 value of a floor reaction force moment correction amount of the desired floor reaction force, wherein the first model input correcting means comprises means for estimating, on the basis of at least an instantaneous value of a model restriction object amount determined by
15 the second model calculating means and the required value, an estimated value of an instantaneous value of a model restriction object amount output by the second dynamic model if it is assumed that at least a floor reaction force moment correction amount of the desired floor
20 reaction force is matched to the required value, and means for comparing the estimated value of an instantaneous value of the model restriction object amount with the permissible range to determine a restricted restriction object amount that has been restricted to fall within the
25 permissible range on the basis of the comparison, and wherein the floor reaction force moment correction amount is determined on the basis of at least the difference

between the instantaneous value of the model restriction object amount determined by the second model calculating means and the restricted restriction object amount (a seventeenth invention).

5 According to the seventeenth invention, first, an estimated value of a restriction object amount when it is assumed that the floor reaction force moment correction amount has been matched with the required value is determined on the basis of at least an instantaneous value
10 of the model restriction object amount and the required value, and a restricted restriction object amount is determined on the basis of the comparison between the estimated value and a permissible range. In this case, the estimated value of a restriction object amount may be
15 determined, considering gyro effect. The restricted restriction object amount is preferably determined to be a value as close as possible to an estimated value of a restriction object amount within the permissible range. And, a floor reaction force moment correction amount is
20 determined on the basis of at least the difference between the instantaneous value of the model restriction object amount and the restricted restriction object amount. Thus, a proper floor reaction force moment correction amount can be determined that makes it possible to prevent the
25 restriction object amount from exceeding the permissible range and that is as close to the required value as possible at the same time.

The aforesaid fourteenth to seventeenth inventions may comprise a second model input correcting means for determining a correction amount of the desired motion on the basis of at least an instantaneous value of a model
5 restriction object amount determined by the second model calculating means and the permissible range, and additionally supplying the determined correction amount to the second dynamic model (an eighteenth invention).

10 With this arrangement, an instantaneous value of a desired motion for making a restriction object amount further properly fall within a permissible range can be supplied to the second dynamic model, while enhancing the stability of the first dynamic model at the same time.

15 Preferably, the eighteenth invention comprises a perturbation model representing a relationship between a perturbative motion of the robot and a perturbation portion of a restriction object amount, means for determining a manipulated variable of a floor reaction force moment on the basis of at least an instantaneous
20 value of a model restriction object amount determined by the second model calculating means and the permissible range, and dividing means for dividing the determined manipulated variable of a floor reaction force moment into a floor reaction force moment correction amount of the
25 desired floor reaction force to be supplied to the first dynamic model and a perturbation model manipulated variable to be supplied to the perturbation model, wherein

the second model input correcting means supplies the perturbation model manipulated variable to the perturbation model so as to determine a correction amount of the desired motion (a nineteenth invention).

5 With this arrangement, the manipulated variable of the floor reaction force moment is divided into a floor reaction force moment correction amount to be supplied to the first dynamic model and a perturbation model manipulated variable to be supplied to the perturbation model, so that inputs suited to the characteristics of the first dynamic model and the perturbation model can be supplied to the individual models. Hence, an instantaneous value of a desired motion that allows a restriction object amount to fall within a permissible range can be properly determined, while preventing the first dynamic model or the perturbation model from becoming unstable. Moreover, using a perturbation model permits easier processing for calculating a correction amount of a desired motion to be additionally supplied to the second dynamic model.

 A floor reaction force moment correction amount to be supplied to the first dynamic model is preferably a low-frequency component (DC component) of the manipulated variable of a floor reaction force moment, and a perturbation model manipulated variable to be supplied to a perturbation model is preferably a high-frequency component of the manipulated variable of a floor reaction

force moment.

Preferably, the nineteenth invention comprises means for determining a required value of a manipulated variable of the floor reaction force moment on the basis of at least a state amount of the perturbation model, wherein the means for determining a manipulated variable of the floor reaction force moment determines a manipulated variable of a floor reaction force moment to be supplied to the dividing means on the basis of at least the instantaneous value of the model restriction object amount determined by the second model calculating means, the permissible range, and the required value (a twentieth invention).

According to the twentieth invention, a state amount of a perturbation model (a rotational angle of a rotor as an element of the perturbation model and an angular velocity thereof, etc.) is taken into account in addition to the permissible range when determining the manipulated variable of a floor reaction force moment to be supplied to the dividing means. This makes it possible to prevent a state amount of the perturbation model from considerably deviating from a state amount corresponding to the required value, thereby preventing an improper correction amount of a desired motion from being determined by the perturbation model.

In the twentieth invention, ideally, the means for determining the required value of the manipulated variable

of a floor reaction force moment sequentially determines the required value according to a feedback control law on the basis of a deviation between the state amount of the perturbation model and a desired value for the state amount (a twenty-first invention).

According to the twenty-first invention, a perturbation model manipulated variable is determined such that a state amount of a perturbation model is substantially maintained in the vicinity of a certain desired state amount. Thus, a correction amount of a desired motion determined by the perturbation model can be set to be ideal for a restriction object amount to fall within a permissible range while stably maintaining the state of the perturbation model.

In the nineteenth to twenty-first inventions comprising the perturbation models, the perturbation model is preferably a model representing a relationship between a perturbative motion perturbing a component about a vertical axis or a floor surface normal line axis of an angular momentum changing rate of a robot and a perturbation portion of the restriction object amount (a twenty-second invention).

This arrangement makes it possible to properly determine a correction amount of a desired motion for making the restriction object amount fall within a permissible range.

In the twenty-second invention, the perturbative

motion is ideally a perturbative motion for maintaining the center-of-gravity position of the robot substantially constant (a twenty-third invention).

5 With this arrangement, a correction of a desired motion by a perturbation model can be made without influencing a translational floor reaction force of a robot.

10 Further, in the aforesaid twenty-second and twenty-third inventions, the perturbative motion is preferably a perturbative motion of a body of the robot and/or an arm extended from the body (a twenty-fourth invention).

This arrangement permits easier processing for calculating a correction amount of a desired motion.

15 Preferably, in the nineteenth invention, the means for determining a manipulated variable of the floor reaction force moment comprises means for estimating, on the basis of at least an instantaneous value of a model restriction object amount determined by the second model calculating means, an estimated value of an instantaneous value of a model restriction object amount output by the
20 second dynamic model when it is assumed that the perturbation model manipulated variable is zero, and means for comparing the estimated value of an instantaneous value of the model restriction object amount with the
25 permissible range to determine a restricted restriction object amount that has been restricted to fall within the permissible range on the basis of the comparison, wherein

the manipulated variable of the floor reaction force moment is determined on the basis of at least a difference between the instantaneous value of the model restriction object amount determined by the second model calculating means and the restricted restriction object amount (a
5 twenty-fifth invention).

According to the twenty-fifth invention, first, an estimated value of a restriction object amount when it is assumed that a perturbation model manipulated variable is
10 zero, that is, when a perturbation portion of a restriction object amount additionally generated by correcting a provisional instantaneous value of a desired motion by a perturbation model is assumed to be zero, is determined on the basis of at least an instantaneous value
15 of the model restriction object amount, and a restricted restriction object amount is determined on the basis of the comparison between the estimated value and a permissible range. In this case, the estimated value of a restriction object amount may be determined, considering
20 gyro effect. The restricted restriction object amount is preferably determined to be a value as close as possible to an estimated value of a restriction object amount within the permissible range. And, a manipulated variable of a floor reaction force moment is determined on the
25 basis of at least the difference between the instantaneous value of the model restriction object amount and the restricted restriction object amount. This makes it

possible to properly determine a manipulated variable of a floor reaction force moment that permits prevention of a restriction object amount from exceeding a permissible range.

5 In the aforesaid twentieth invention, the means for determining the manipulated variable of a floor reaction force moment comprises means for estimating, on the basis of at least an instantaneous value of a model restriction object amount determined by the second model calculating means and the required value, an estimated value of an
10 instantaneous value of a model restriction object amount output by the second dynamic model if it is assumed that the perturbation model manipulated variable is matched to the required value, and means for comparing the estimated
15 value of an instantaneous value of the model restriction object amount with the permissible range to determine a restricted restriction object amount that has been restricted to fall within the permissible range on the basis of the comparison, wherein the manipulated variable
20 of the floor reaction force moment is determined on the basis of at least the difference between the instantaneous value of the model restriction object amount determined by the second model calculating means and the restricted restriction object amount (a twenty-sixth invention).

25 According to the twenty-sixth invention, first, an estimated value of a restriction object amount when it is assumed that the perturbation model manipulated variable

has been matched with the required value, that is, when it is assumed that only the required value has been supplied to a perturbation model, is determined on the basis of at least an instantaneous value of the model restriction object amount and the required value, and a restricted restriction object amount is determined on the basis of the comparison between the estimated value and a permissible range. In this case, the estimated value of a restriction object amount may be determined, taking gyro effect into account. The restricted restriction object amount is preferably determined to be a value as close as possible to an estimated value of a restriction object amount within the permissible range. And, a perturbation model manipulated variable is determined on the basis of at least the difference between the instantaneous value of the model restriction object amount and the restricted restriction object amount. This makes it possible to properly determine a manipulated variable of a floor reaction force moment that prevents a restriction object amount from exceeding a permissible range and also to secure stability of the perturbation model.

According to a twenty-seventh invention of a gait generating device of a legged mobile robot in accordance with the present invention,

there is provided a gait generating device for generating a desired gait of a legged mobile robot that travels by moving a plurality of legs extended from its

body, comprising:

permissible range setting means for setting a permissible range of a restriction object amount, the restriction object amount being a vertical component of a floor reaction force moment or a component of the floor reaction force moment in floor surface normal line direction, or a vertical component of an angular momentum changing rate of the robot or a component of the angular momentum changing rate in floor surface normal line direction, to be applied to the robot;

desired floor reaction force provisional instantaneous value determining means for sequentially determining a provisional instantaneous value of at least a desired floor reaction force among a desired motion and a desired floor reaction force constituting the desired gait;

first model calculating means for supplying at least a provisional instantaneous value of the desired floor reaction force to a first dynamic model that indicates a relationship between a motion of the robot and a floor reaction force so as to determine a first provisional instantaneous value of a desired motion as an output of the first dynamic model;

second model calculating means with restriction for supplying at least a provisional instantaneous value of the desired floor reaction force to a second dynamic model that indicates a relationship between a motion of the

robot and the restriction object amount so as to determine
a second provisional instantaneous value of a desired
motion as an output of the second dynamic model such that
an instantaneous value of a restriction object amount
5 substantially balancing with the second provisional
instantaneous value of the desired motion on the second
dynamic model falls within the permissible range;

manipulated variable calculating means for
determining a manipulated variable of a floor reaction
10 force moment on the basis of at least a difference between
the first provisional instantaneous value and the second
provisional instantaneous value of the desired motion such
that the difference approximates to zero; and

model input correcting means for additionally
15 supplying the manipulated variable of the floor reaction
force moment to at least one of the first dynamic model
and the second dynamic model,

wherein the second provisional instantaneous value of
the desired motion is determined as the instantaneous
20 value of the desired motion.

According to the twenty-seventh invention, a
provisional instantaneous value of a desired floor
reaction force is supplied to the first dynamic model to
determine a first provisional instantaneous value of a
25 desired motion, while a provisional instantaneous value of
a desired floor reaction force is also supplied to the
second dynamic model, and a second provisional

instantaneous value of the desired motion is determined using the second dynamic model. In this case, however, the second provisional instantaneous value of the desired motion is determined such that an instantaneous value of a restriction object amount that substantially balances with the second provisional instantaneous value on the second dynamic model falls within the permissible range. And, the manipulated variable of a floor reaction force moment is determined on the basis of at least a difference between the first provisional instantaneous value and the second provisional instantaneous value of the desired motion such that the difference approximates to zero, and this is additionally supplied to at least one of the first dynamic model and the second dynamic model. Furthermore, the second provisional instantaneous value of a desired motion is determined as a desired instantaneous value of the desired motion.

Thus, the second provisional instantaneous value of a desired motion determined by a restricted second model calculating means exhibits high stability, while making the restriction object amount fall within a permissible range. As a result, it is possible to generate a motion of a desired gait that makes a restriction object amount, such as a floor reaction force moment vertical component, fall within a permissible range. This means that the instantaneous value of a desired motion is determined, taking into account the limitation of a vertical component

of a frictional force moment on the dynamic model. With this arrangement, a desired gait can be generated that makes it possible to prevent a robot from spinning and falling from the spinning. In addition, it is not
5 required to always maintain the restriction object amount to zero or substantially zero as long as a restriction object amount remains within a permissible range, thus making it possible to generate a desired gait that prevents the motion of a certain part of the robot from
10 becoming unduly intense.

The first dynamic model may have relatively low dynamic approximation accuracy. The second dynamic model preferably has higher dynamic approximation accuracy than the first dynamic model.

15 In the twenty-seventh invention, the difference between the first provisional instantaneous value and the second provisional instantaneous value of the desired motion preferably includes a difference in a state amount of a posture of a predetermined part of the robot about a
20 vertical axis or about a floor surface normal line axis (a twenty-eighth invention).

With this arrangement, the stability of a posture state amount of the predetermined part (e.g., the body) in the yaw direction can be ideally improved.

25 The aforesaid twenty-seventh and twenty-eighth inventions preferably comprise means for determining an instantaneous value of a floor reaction force moment

corresponding to a restriction object amount substantially
balancing with an instantaneous value of the desired
motion on the second dynamic model as an instantaneous
value of a desired floor reaction force moment
5 constituting the desired gait (a twenty-ninth invention).

This arrangement makes it possible to determine an
instantaneous value of a desired floor reaction force
moment that has high dynamic accuracy relative to an
instantaneous value of a desired motion.

10 The twenty-seventh invention described above can be
easily implemented by using, for example, the arrangement
according to the aforesaid seventeenth invention. More
specifically, the seventeenth invention comprises third
model calculating means for supplying at least the
15 provisional instantaneous value of the desired floor
reaction force to a third dynamic model representing a
relationship between a motion of the robot and a floor
reaction force so as to determine a third provisional
instantaneous value of a desired motion as an output of
20 the third dynamic model, wherein the means for determining
a required value of a floor reaction force moment
correction amount of the desired floor reaction force
determines the required value on the basis of a difference
between a desired instantaneous value of the determined
25 desired motion and a third provisional instantaneous value
of the desired motion such that the difference
approximates to zero (a thirtieth invention).

In the thirtieth invention, the third dynamic model and the third model calculating means correspond to the first dynamic model and the first model calculating means, respectively, in the seventeenth invention. Hence, the
5 thirtieth invention is equivalent to the seventeenth invention and capable of providing the same advantages as those of the seventeenth invention.

According to a thirty-first invention of a gait generating device of a legged mobile robot in accordance
10 with the present invention, there is provided a gait generating device for generating a desired gait of a legged mobile robot that travels by moving a plurality of legs extended from its body, comprising:

permissible range setting means for setting a
15 permissible range of a restriction object amount, the restriction object amount being a vertical component of a floor reaction force moment or a component of the floor reaction force moment in floor surface normal line direction, or a vertical component of an angular momentum
20 changing rate of the robot or a component of the angular momentum changing rate in floor surface normal line direction, to be applied to the robot;

desired motion provisional instantaneous value determining means for sequentially determining a
25 provisional instantaneous value of a desired motion constituting the desired gait;

model calculating means for supplying the provisional

instantaneous value of the desired motion to a dynamic model representing a relationship between a motion of the robot and the restriction object amount so as to determine an instantaneous value of a model restriction object amount as an output of the dynamic model; and

desired instantaneous value determining means for determining an instantaneous value of a desired motion by correcting the provisional instantaneous value of the desired motion on the basis of a portion of the model restriction object amount instantaneous value that deviates from the permissible range and that has been passed through a low-pass filter.

According to the thirty-first invention, an instantaneous value of a desired motion is determined by correcting a provisional instantaneous value of the desired motion on the basis of a portion of the model restriction object amount instantaneous value as an output of the dynamic model, the portion deviating from the permissible range and having been passed through a low-pass filter. In other words, a provisional instantaneous value of a desired motion is corrected on the basis of a low-frequency component (including a DC component) of the aforementioned deviating portion. This makes it possible to generate a motion of a desired gait that permits prevention of a restriction object amount, such as a floor reaction force moment vertical component, from steadily deviating from a permissible range. More specifically, an

instantaneous value of a desired motion is determined,
taking into account the limitation of a vertical component
of a frictional force moment on the dynamic model. With
this arrangement, a desired gait can be generated that
5 makes it possible to prevent a robot from spinning and
falling from the spinning. In addition, it is not
required to always maintain a restriction object amount to
zero or substantially zero, so that it is possible to
generate a desired gait that prevents the motion of a
10 certain part of the robot from becoming unduly intense.

In the thirty-first invention, the desired
instantaneous value determining means preferably
determines a floor reaction force moment corresponding to
a difference between the model restriction object amount
15 instantaneous value and the deviating portion as the
instantaneous value of a desired floor reaction force
moment constituting the desired gait (a thirty-second
invention).

This arrangement makes it possible to determine an
20 instantaneous value of a desired floor reaction force
moment having high dynamic accuracy relative to an
instantaneous value of a desired motion.

According to a thirty-third invention, which is a
control device of a legged mobile robot in accordance with
25 the present invention, a control device for controlling an
operation of the robot to make the robot follow a desired
gait generated by the gait generating device of a legged

mobile robot according to the first to the thirty-second inventions comprises slippage determining means for determining the occurrence of a slippage of the robot in operation, following the desired gait, wherein the
5 permissible range setting means variably sets the permissible range according to a determination result of the slippage determining means.

According to the thirty-third invention, the permissible range of a restriction object amount is
10 variably set on the basis of a determination result of the occurrence of a slippage of an actual robot, so that the occurrence of a slippage of the robot can be securely restrained. If it is determined that a slippage has occurred, then the permissible range should be set to be
15 narrower.

According to the thirty-third invention, the occurrence of a slippage can be determined, for example, as described below.

Specifically, the slippage determining means
20 determines the occurrence of a slippage on the basis of at least a ground speed of a distal portion of a leg in contact with the ground (a thirty-fourth invention). In this case, it can be determined that a slippage has occurred if, for example, the absolute value of the ground
25 speed is larger than a predetermined value.

Alternatively, the slippage determining means comprises means for determining an apparent spring

constant of a leg on the basis of at least a temporal
changing rate of an actual floor reaction force acting on
the leg in contact with the ground and a ground speed of a
distal portion of the leg, wherein the occurrence of a
5 slippage is determined on the basis of at least the
apparent spring constant (a thirty-fifth invention). In
this case, it can be determined that a slippage has
occurred if, for example, the apparent spring constant is
smaller than a predetermined value.

10 Alternatively, the slippage determining means
determines the occurrence of a slippage on the basis of at
least an actual floor reaction force acting on a leg in
contact with the ground that has been passed through a
band-pass filter having a frequency pass characteristic in
15 a range near a predetermined frequency (a thirty-sixth
invention). In this case, the actual floor reaction force
passed through the band-pass filter will be equivalent to
a vibration component of the actual floor reaction force
when a so-called slippage vibration is taking place. And,
20 if, for example, the magnitude (absolute value) of the
vibration component is larger than a predetermined value,
then it can be determined that a slippage vibration exists.

The occurrence of a slippage can be determined by any
one of the thirty-fourth to the thirty-sixth inventions.
25 Alternatively, two or more of these thirty-fourth to the
thirty-sixth inventions may be combined to determine the
occurrence of a slippage.

Brief Description of the Drawings

Fig. 1 is a diagram schematically showing a general construction of a bipedal mobile robot as a legged mobile robot in an embodiment of the present invention and a reference example related thereto, Fig. 2 is a diagram showing a structure of a distal portion of a leg of the robot shown in Fig. 1, Fig. 3 is a block diagram showing a construction of a control unit provided on the robot shown in Fig. 1, and Fig. 4 is a block diagram showing a functional construction of the control unit in a first reference example. Fig. 5 is a diagram for explaining a walking gait generated in the embodiment and the reference example, Fig. 6 is a graph showing an example of a vertical component trajectory of a desired floor reaction force, Fig. 7 shows graphs illustrating examples of an X component and a Y component of a desired ZMP trajectory, Fig. 8 is a diagram for explaining a body translational mode of a robot, Fig. 9 is a diagram for explaining a body inclination mode of the robot, Fig. 10 is a diagram for explaining a body yaw rotation mode of the robot, Fig. 11(a) is a diagram for explaining an antiphase arm swing mode of the robot in a plan view and Fig. 11(b) is a diagram for explaining an antiphase arm swing mode of the robot in a side view, and Fig. 12 is a diagram for explaining a dynamic model used in the embodiment. Fig. 13 is a flowchart showing a main routine processing of a

gait generating device in a first reference example, Fig. 14 is a diagram for explaining a diversion state of the robot, Fig. 15 is a flowchart showing a subroutine processing of S022 of Fig. 13, Fig. 16 is a diagram for explaining a normal gait and a supporting leg coordinate system, Fig. 17 is a diagram illustrating a body trajectory of the normal gait and the supporting leg coordinate system, Fig. 18 is a graph showing an example of a reference antiphase arm swing angle, Fig. 19 is a graph showing a setting example of a desired floor reaction force vertical component trajectory in a normal gait, Fig. 20 is a graph showing a setting example of a floor reaction force horizontal component permissible range in a normal gait, Fig. 21 is a graph showing a setting example of a floor reaction force moment vertical component permissible range in the normal gait, and Fig. 22 is a graph showing a setting example of the desired ZMP trajectory in the normal gait. Fig. 23 is a flowchart showing subroutine processing of S024 in Fig. 13, Fig. 24 is a flowchart showing subroutine processing of S208 in Fig. 23, Fig. 25 is a flowchart showing subroutine processing of S306 in Fig. 24, Fig. 26 is a flowchart showing subroutine processing of S412 in Fig. 25, Fig. 27 is a graph showing an example of a floor reaction force horizontal component in which a permissible range is not considered, Fig. 28 is a graph showing an example of the floor reaction force horizontal component in which the

permissible range is considered, Fig. 29 is a graph showing an example of a body inclination angle acceleration, Fig. 30 is a graph showing an example of a body inclination restoring moment ZMP-converted value for restoring a body inclination angle of the robot, Fig. 31 is a graph showing an example of a body inclination angle acceleration in which the body inclination restoring moment ZMP-converted value is reflected, Fig. 32 is a graph showing an example of a floor reaction force moment vertical component in which a permissible range is not considered, Fig. 33 is a graph showing an example of a floor reaction force moment vertical component in which the permissible range is considered, Fig. 34 is a graph showing an example of an antiphase arm swing moment, Fig. 35 is a graph showing an antiphase arm swing angular acceleration corresponding to the antiphase arm swing moment shown in Fig. 34, Fig. 36 is a graph showing an example of an antiphase arm swing restoring angular acceleration for restoring an antiphase arm swing angle, Fig. 37 is a graph showing an antiphase arm swing restoring moment corresponding to an antiphase arm swing restoring angular acceleration shown in Fig. 36, and Fig. 38 is a graph showing a floor reaction force moment vertical component formed by combining the floor reaction force moment vertical component shown in Fig. 33 and the antiphase arm swing restoring moment shown in Fig. 37. Fig. 39 is a flowchart showing subroutine processing of

S026 in Fig. 13, Fig. 40 is a graph showing a setting example of a floor reaction force horizontal component permissible range of a present gait, Fig. 41 is a graph showing a setting example of a floor reaction force moment vertical component permissible range of the present gait, 5 Fig. 42 is a flowchart showing subroutine processing of S028 in Fig. 13, Fig. 43 is a flowchart showing subroutine processing of S702 in Fig. 42, Fig. 44 is a graph showing examples of a provisional desired ZMP of the present gait, 10 a ZMP correction amount, and a desired ZMP after correction, Fig. 45 is a flowchart showing subroutine processing of S030 in Fig. 13, and Fig. 46 is a flowchart showing subroutine processing of S1412 in Fig. 45. Fig. 47 is a graph showing a relationship between normal gaits and desired gaits relative to body position trajectories, 15 Fig. 48 is a diagram showing another example of a body inclination mode (body inclination about waist), Fig. 49 is a diagram for explaining another example of a dynamic model, Fig. 50 is a diagram showing a setting example of a 20 desired floor reaction force vertical component in a walking gait, Fig. 51 is a diagram showing a relationship between the position in the body vertical direction and a floor reaction force vertical component in running gaits of the robot, and Fig. 52 is a diagram showing a 25 relationship between the position in the body vertical direction and a floor reaction force vertical component in walking gaits of the robot. Fig. 53 is a block diagram

showing a functional construction of a control unit in a second reference example, Fig. 54 is a block diagram showing the processing of a compensating total floor reaction force moment horizontal component distributor shown in Fig. 53, Fig. 55 is a block diagram showing the processing of a model manipulation floor reaction force moment vertical component determiner shown in Fig. 53, Fig. 56 is a flowchart showing main routine processing of a gait generating device in the second reference example, Fig. 57 is a flowchart showing subroutine processing of S3032 in Fig. 56, and Fig. 58 is a flowchart showing a subroutine processing of S3414 in Fig. 57. Fig. 59 is a block diagram showing a functional construction of a control unit in a third reference example, Fig. 60 is a flowchart showing main routine processing of a gait generating device in the third reference example, Fig. 61 is a flowchart showing subroutine processing of S2034 in Fig. 60, and Fig. 62 is a flowchart showing subroutine processing of S2114 in Fig. 61. Fig. 63 is a block diagram showing a functional construction of a control unit in a first embodiment of the present invention, Fig. 64 is a block diagram showing a functional construction of a gait generating device in the first embodiment, Fig. 65 is a setting example of a ZMP permissible range in the first embodiment, Fig. 66 is a flowchart showing main routine processing of the gait generating device in the first embodiment, Fig. 67 is a block diagram illustrating

the processing of S3536 of Fig. 66, Fig. 68 is a diagram for explaining a horizontal body position perturbing model shown in Fig. 67, Fig. 69 is a diagram for explaining a perturbation model for correcting a body posture angle shown in Fig. 67, Fig. 70 is a diagram for explaining a perturbation model for correcting an antiphase arm swing angle shown in Fig. 67, and Fig. 71 is a block diagram showing processing of an antiphase arm swing angle correcting perturbation model moment determiner shown in Fig. 67. Fig. 72 is a block diagram showing the processing of S3536 in Fig. 66 in a second embodiment of the present invention and Fig. 73 is a block diagram showing the processing of the antiphase arm swing angle correcting perturbation model moment determiner shown in Fig. 72. Fig. 74 is a block diagram showing a functional construction of a gait generating device in a third embodiment of the present invention, and Fig. 75 is a block diagram showing the processing of a pseudo order full model shown in Fig. 74. Fig. 76 is a block diagram showing the processing of S3536 in Fig. 66 in a fourth embodiment of the present invention. Fig. 77 is a block diagram showing a functional construction of a control unit in a fourth reference example related to a fifth embodiment of the present invention, Fig. 78 is a flowchart showing main routine processing of a gait generating device in the fourth reference example, Fig. 79 is a flowchart showing the processing of S2334 of Fig. 78,

Fig. 80 is a flowchart showing the processing of a
slippage determiner shown in Fig. 77, Fig. 81 to Fig. 83
are flowcharts showing the subroutine processing of S5210,
S5212, and S5214, respectively, in Fig. 80, Fig. 84 is a
5 graph showing examples of determination results of the
slippage determiner, reducing rates of permissible ranges,
and floor reaction force permissible ranges, Fig. 85 is a
block diagram showing modification examples related to the
first to the fifth embodiments, and Fig. 86 is a block
10 diagram showing a modification example (a sixth
embodiment) of the processing of the antiphase arm swing
angle correcting perturbation model moment determiner
related to the first embodiment.

15 Best Mode for Carrying Out the Invention

Referring now to the accompanying drawings, control
devices of legged mobile robots according to embodiments
of the present invention will be explained. As the legged
mobile robots, bipedal mobile robots will be used as
20 examples.

First, with reference to Fig. 1 to Fig. 47, a first
reference example related to the control device of a
legged mobile robot in accordance with the present
invention will be explained. Further, a second reference
25 example will be explained, referring to Fig. 53 to Fig. 58,
and a third reference example will be explained, referring
to Fig. 59 to Fig. 62. The embodiments of the present

invention to be discussed hereinafter share the same mechanical constructions as that of the first reference example, while they only partly differ from any one of the first to the third reference examples in gait generation processing and control processing of a robot. For this reason, the explanation of the first to the third reference examples will be frequently used in the explanation of the embodiments to be discussed hereinafter. Supplementally, the same matters that will be explained with reference to Fig. 1 and Fig. 2, Fig. 3 and Fig. 5 to Fig. 12 to be discussed later will apply to the embodiments to be discussed later.

First, the first reference example will be explained. Fig. 1 is a schematic diagram generally showing a bipedal mobile robot representing a legged mobile robot according to the first reference example.

As shown in the figure, a bipedal mobile robot (hereinafter referred to as "the robot") 1 is equipped with a pair of right and left legs (leg links) 2, 2 provided such that they extend downward from a body (a base body of the robot 1) 3. The two legs 2, 2 share the same construction, each having six joints. The six joints of each leg are comprised of, in the following order from the body 3 side, joints 10R, 10L (symbols R and L meaning correspondence to the right leg and the left leg, respectively; the same will be applied hereinafter) for swinging (rotating) a hip (waist) (for rotating in a yaw

direction relative to the body 3), joints 12R, 12L for rotating the hip (waist) in a roll direction (about an X axis), joints 14R, 14L for rotating the hip (waist) in a pitch direction (about a Y axis), joints 16R, 16L for rotating knees in the pitch direction, joints 18R, 18L for rotating ankles in the pitch direction, and joints 20R, 20L for rotating the ankles in the roll direction.

A foot (foot portion) 22R (L) constituting a distal portion of each leg 2 is attached to the bottoms of the two joints 18R (L) and 20R (L) of the ankle of each leg 2. The body 3 is installed at the uppermost top of the two legs 2, 2 through the intermediary of the three joints 10R (L), 12R (L) and 14R (L) of the hip of each leg 2. A control unit 60 or the like, which will be discussed in detail hereinafter, is housed inside the body 3. For convenience of illustration, the control unit 60 is shown outside the body 3 in Fig. 1.

In each leg 2 having the aforesaid construction, a hip joint (or a waist joint) is formed of the joints 10R (L), 12R (L) and 14R (L), the knee joint is formed of the joint 16R (L), and the ankle joint is formed of the joints 18R (L) and 20R (L). The hip joint and the knee joint are connected by a thigh link 24R (L), and the knee joint and the ankle joint are connected by a crus link 26R (L).

A pair of right and left arms 5, 5 is attached to both sides of an upper portion of the body 3, and a head 4 is disposed at a top end of the body 3. Each arm 5 is

provided with a shoulder joint composed of three joints
30R (L), 32R (L), and 34R (L) an elbow joint composed of a
joint 36 R(L), a wrist joint composed of a joint 38R (L),
and a hand 40R (L) connected to the wrist joint. The head
5 4 is not directly connected to a topic of the present
invention, so that detailed explanation thereof will be
omitted.

According to the construction described above, the
foot 22R (L) of each leg 2 is given six degrees of freedom
10 relative to the body 3. During a travel, such as walking,
of the robot 1, desired motions of the two feet 22R and
22L can be accomplished by driving $6 \times 2 = 12$ joints of the
two legs 2, 2 together ("*" in the present description
will denote multiplication as scalar calculation, while it
15 will denote an outer product in vector calculation) at
appropriate angles. This arrangement enables the robot 1
to arbitrarily move in a three-dimensional space.
Furthermore, each arm 5 can perform a motion, such as arm
swinging, by rotating its shoulder joint, the elbow joint,
20 and the wrist joint.

As shown in Fig. 1, a publicly known six-axis force
sensor 50 is provided between the ankle joints 18R (L),
20R (L) and the foot 22R (L) of each leg 2. The six-axis
force sensor 50 detects primarily whether the foot 22R (L)
25 of each leg 2 is in contact with the ground, and a floor
reaction force (landing load) acting on each leg 2, and it
outputs detection signals of three-direction components F_x ,

Fy, and Fz of a translational force of the floor reaction force and three-direction components Mx, My, and Mz of a moment to the control unit 60. Furthermore, the body 3 is equipped with a posture sensor 54 for detecting an inclination angle of the body 3 relative to a Z-axis (vertical direction (gravitational direction)) and an angular velocity thereof, and a rotational angle (yaw angle) of the body 3 about the Z-axis and an angular velocity thereof, detection signals thereof being output from the posture sensor 54 to the control unit 60. The posture sensor 54 is provided with a three-axis direction accelerometer and a three-axis direction gyro sensor. These detection signals of these sensors are used to detect posture angles (an inclination angle and a yaw angle) of the body 3 and an angular velocity thereof, and also used to estimate a self position/posture of the robot 1. Although detailed structures are not shown, each joint of the robot 1 is provided with an electric motor 64 (refer to Fig. 3) for driving the joint, and an encoder (rotary encoder) 65 (refer to Fig. 3) for detecting a rotational amount of the electric motor 64 (a rotational angle of each joint). Detection signals of the encoder 65 are output from the encoder 65 to the control unit 60.

Furthermore, although not shown in Fig. 1, a joystick (operating device) 73 (refer to Fig. 3) is provided at an appropriate position of the robot 1. The joystick 73 is constructed in such a manner that a request regarding a

gait of the robot 1, such as a request for turning the robot 1 that is moving straight, is input to the control unit 60 as necessary by operating the joystick 73.

Fig. 2 is a diagram schematically showing a basic construction of a distal portion (including each foot 22R (L)) of each leg 2 in the present reference example. As shown in the diagram, a spring mechanism 70 is installed between each foot 22R (L) and the six-axis force sensor 50, and a foot sole elastic member 71 made of rubber or the like is bonded to a foot sole (the bottom surface of each foot 22R (L)). These spring mechanism 70 and the foot sole elastic member 71 constitute a compliance mechanism 72. The spring mechanism 70, which will be discussed in detail later, is constructed of a square guide member (not shown), which is installed on the upper surface of the foot 22R (L), and a piston-shaped member (not shown) installed adjacently to the ankle joint 18R (L) (the ankle joint 20R (L) being omitted in Fig. 2) and the six-axis force sensor 50, and housed in the guide member through the intermediary of an elastic member (rubber or spring) so that it may be jogged.

The foot 22R (L) indicated by a solid line shown in Fig. 2 is in a state where it is subjected to no floor reaction force. When each leg 2 is subjected to a floor reaction force, the spring mechanism 70 and the foot sole elastic member 71 of the compliance mechanism 72 flex, causing the foot 22R (L) to shift to the position/posture

illustrated by a dashed line in the figure. The structure of the compliance mechanism 72 is important not only to ease a landing impact but also to enhance controllability, as explained in detail in, for example, Japanese

5 Unexamined Patent Publication Application No. 5-305584 previously proposed by the present applicant.

Fig. 3 is a block diagram showing a construction of the control unit 60. The control unit 60 is comprised of a microcomputer, and includes a first calculator 90 and a
10 second calculator 92 formed of CPUs, an A/D converter 80, a counter 86, a D/A converter 96, a RAM 84, a ROM 94, and a bus line 82 for transferring data among them. In the control unit 60, output signals of the six-axis force sensor 50, the posture sensor 54 (an accelerometer and a
15 rate gyro sensor), the joystick 73, etc. of each leg 2 are converted into digital values by the A/D converter 80 and sent to the RAM 84 via the bus line 82. Outputs of the encoder 65 (rotary encoder) of each joint of the robot 1 are supplied to the RAM 84 via the counter 86.

20 As will be discussed hereinafter, the first calculator 90 generates desired gaits, calculates a joint angle displacement command (a displacement angle of each joint or a command value of a rotational angle of each electric motor 64), and sends the calculation result to
25 the RAM 84. The second calculator 92 reads the joint angle displacement command and an actual measurement value of a joint angle detected on the basis of an output signal

of the encoder 65 from the RAM 84 to calculate a manipulated variable required for driving each joint, and outputs the calculated variable to the electric motor 64 for driving each joint through the intermediary of the D/A converter 96 and a servo amplifier 64a.

Fig. 4 is a block diagram showing the entire functional construction of a control unit of the legged mobile robot in accordance with the first reference example. A portion except for the "actual robot" in Fig. 4 is constituted by processing functions implemented by the control unit 60 (primarily the functions of the first calculator 90 and the second calculator 92). In the following explanation, the symbols R and L will be omitted as long as it is not particularly necessary to discriminate right and left of the legs 2 and the arms 5.

The explanation will now be given. The control unit 60 is equipped with a gait generating device 100 for generating and outputting desired gaits of the robot 1 freely and in real time. The functions of the gait generating device 100 constitute individual means of the present invention. A desired gait output by the gait generating device 100 is constituted of a desired body position/posture trajectory (trajectory of a desired position and a desired posture of the body 3), a desired foot position/posture trajectory (trajectory of a desired position and a desired posture of each foot 22), a desired arm posture trajectory (trajectory of a desired posture of

each arm 5), a desired total floor reaction force central point (desired ZMP) trajectory, and a desired total floor reaction force trajectory. If a movable part relative to the body 3 is provided in addition to the legs 2 and the arms 5, then a desired position/posture trajectory of the movable part is added to the desired gait.

Here, the term "trajectory" in the above gait means a temporal change pattern (time series pattern), and may be referred to as "pattern" in place of "trajectory" in the following explanation. Furthermore, a "posture" of each part means a spatial orientation. For example, a posture of a body is represented by an inclination angle of the body 3 in the roll direction (about the X-axis) relative to the Z-axis (vertical axis), an inclination angle of the body 3 in the pitch direction (about the Y-axis), and a rotational angle (yaw angle) of the body 3 in the yaw direction (about the Z-axis). A foot posture is represented by means of a spatial azimuth of two axes fixedly set on each foot 22. In the present description, a body posture may be referred to as a body posture angle. Of body postures, a posture relative to a vertical direction may be referred to as a body posture inclination or a body posture inclination angle.

In the following explanation, the term "desired" will be frequently omitted when there is no danger of misunderstanding. Furthermore, among gaits, those gaits related to constituent elements other than those related

to a floor reaction force, that is, the gaits related to motions of the robot 1, such as a foot position/posture and a body position/posture, will be collectively referred to as "motion." A floor reaction force (floor reaction force comprised of a translational force and the moment) of each foot 22 is referred to as "each-foot floor reaction force", and a resultant force of the "each-foot floor reaction forces" of all (two) feet 22R and 22L of the robot 1 will be referred to as a "total floor reaction force" . In the following explanation, however, each-foot floor reaction force will hardly be referred to, so that "floor reaction force" will be handled as having the same meaning as "total floor reaction force" unless otherwise specified.

A desired floor reaction force is generally expressed by a point of action and a translational force and the moment acting on the point. The point of action may be set at any location, so that innumerable expressions are possible for the same desired floor reaction force. If, however, a desired floor reaction force is expressed using especially the aforesaid desired floor reaction force central point (a desired position of the floor reaction force central point) as the point of action, then the moment component of the desired floor reaction force will be zero except for a vertical component (the moment about the vertical axis (Z-axis)). In other words, the horizontal component of the moment of the desired floor

reaction force about the desired floor reaction force central point (the moment about the horizontal axis (the X-axis and the Y-axis)) will be zero.

5 In the case of a gait that satisfies dynamic balance conditions, a ZMP calculated from a desired motion trajectory of the robot 1 (a point at which the moment of a resultant force of an inertial force calculated from the desired motion trajectory and gravity acts about the point becomes zero except for a vertical component) agrees with
10 a desired floor reaction force central point. Therefore, providing a desired ZMP trajectory may be regarded as equivalent to providing a desired floor reaction force central point trajectory (refer to, for example, PCT Kokai publication WO/02/40224 by the present applicant for more
15 details).

From the background described above, in the description of PCT Kokai publication WO/02/40224, a desired gait has been defined as follows.

- 20 a) In a broad sense, a desired gait is a combination of a desired motion trajectory and a desired floor reaction force trajectory thereof in a period of one step or a plurality of steps.
- b) In a narrow sense, a desired gait is a combination of a desired motion trajectory and a ZMP trajectory thereof in
25 a period of one step.
- c) A series of gaits is formed of several gaits that are connected.

In walking, a vertical position of the body 3 of the robot 1 (a height of the body) is determined by a body height determining technique proposed previously in Japanese Unexamined Patent Application Publication No. 10-86080 by the present applicant. This subordinately determines a translational floor reaction force vertical component. Furthermore, a translational floor reaction force horizontal component is also determined by determining the horizontal body position trajectory of the robot 1 such that the horizontal component of the moment produced about a desired ZMP by a resultant force of the inertial force and the gravity generated by the motion of a desired gait becomes zero. For this reason, a desired ZMP alone has been adequate as a physical amount to be explicitly set for the floor reaction force of a desired gait in the description of PCT Kokai publication WO/02/40224. Thus, the definition in the above b) has been adequate as the definition of a desired gait in the narrow sense. However, in the running gait of the robot 1 explained in the first reference example (the details will be described hereinafter), a floor reaction force vertical component (a translational floor reaction force vertical component) is also important for control. In the present invention, therefore, a desired trajectory of the floor reaction force vertical component is explicitly set, and then a trajectory of a desired vertical body position or the like of the robot 1 is determined. Hence, in the

present description, the following b') will be adopted as the definition of a desired gait in a narrow sense.

b') A desired gait in a narrow sense is a combination of a desired motion trajectory and a desired floor reaction force trajectory including at least a ZMP trajectory of the desired motion trajectory and a desired translational floor reaction force vertical component trajectory in a period of one step.

In the present description, a desired gait used hereinafter will mean the desired gaits in the narrow sense of the above b') unless otherwise specified for the purpose of easy understand. In this case, "one step" of a desired gait will mean a period from the moment one leg 2 of the robot 1 touches the ground to the moment the other leg 2 touches the ground. Supplementally, in the reference example and embodiments in the present description, a desired gait is used to mean a gait for one-step period. This, however, does not have to be necessarily the one-step period; it may alternatively be a period for a plurality of steps or a period that is shorter than one step (e.g., a half step). In the following explanation, "floor reaction force vertical component" will mean "translational floor reaction force vertical component," and the term "moment" will be used for the vertical component (the component about the vertical axis) of a moment of a floor reaction force so as to distinguish it from the "floor reaction force vertical

component." Similarly, "floor reaction force horizontal component" will mean "translational floor reaction force horizontal component."

Needless to say, a double stance period in a gait
5 will refer to a period during which the robot 1 supports
its own weight by the two legs 2, 2. A single stance
period will refer to a period during which the robot 1
supports its own weight only by one leg 2, and a floating
period will refer to a period during which both legs 2, 2
10 are apart from a floor (floating in the air). In the
single stance period, the leg 2 not supporting the self-
weight of the robot 1 will be referred to as a "free leg."
The running gait explained in the first reference example
does not have the double stance period, but alternately
15 repeats the single stance period (landing period) and the
floating period. In this case, during the floating period
of running, both legs 2, 2 do not support the self-weight
of the robot 1; however, the leg 2 that was a free leg and
the leg 2 that was a supporting leg during a single stance
20 period immediately before the floating period will be
referred to as a "free leg" and a "supporting leg,"
respectively, even in the floating period.

Taking the running gait shown in Fig. 5 as an example,
an outline of a desired gait generated by the gait
25 generating device 100 will be explained. More definitions
and details related to gaits have been given also in
Japanese Unexamined Patent Application Publication No. 10-

86081 previously proposed by the present applicant, so that the following will mainly give a description not covered by the Japanese Unexamined Patent Application Publication No. 10-86081.

5 First, the running gait shown in Fig. 5 will be explained. This running gait is a gait similar to a typical human running gait. In this running gait, the single stance period in which the foot 22 of only either the right or left leg 2 (supporting leg) of the robot 1
10 lands (contacts the ground) and a floating period in which both the legs 2, 2 float in the air are alternately repeated. In Fig. 5, the first state illustrates a state wherein a single stance period has begun (initial stage), the second state illustrates a state of a midpoint of the
15 single stance period, the third state illustrates a state wherein a floating period following the single stance period has begun (an end of the single stance period), the fourth state illustrates a state of a midpoint of the floating period, and the fifth state illustrates an end of
20 the floating period (a start of the next single stance period).

 In this running gait, the robot 1 lands at the heel of the foot 22 of the supporting leg (the leg 2 on the front side in the advancing direction of the robot 1) at
25 the beginning of the single stance period, as shown in the first state of Fig. 5. Subsequently, the robot 1 brings substantially the entire surface of the sole of the landed

foot 22 (the foot 22 of the supporting leg) into contact with the ground as shown in the second state of Fig. 5, and then kicks the floor with the tiptoe of the foot 22 (the foot 22 of the leg 2 on the rear side with respect to the advancing direction of the robot 1 in the third state of Fig. 5) of the supporting leg to jump into the air as shown in the third state of Fig. 5. This ends the single stance period and starts the floating period at the same time. The free leg in the single stance period exists behind the supporting leg at the beginning of the single stance period as shown in the first state of Fig. 5, but swung out to the front of the supporting leg toward the next predetermined landing position, as shown in the second and the third states of Fig. 5. Next, following the floating period shown in the fourth state of Fig. 5, the robot 1 lands at the heel of the foot 22 of the free leg (the leg 2 that was the free leg in the single stance period immediately before the floating period started), and the next single stance period is begun.

Considering the running gait shown in Fig. 5, a basic outline of a desired gait generated by the gait generating device 100 will be explained. Although more details will be discussed later, when the gait generating device 100 generates a desired gait, basic required values (required parameters) for generating the desired gait, such as a landing position/posture (expected landing position/posture) of the foot 22 of a free leg and a

landing time (expected landing time), are supplied to the gait generating device 100 according to a required operation or the like of the joystick 73. The gait generating device 100 then generates the desired gait using the required parameters. More detailedly, the gait generating device 100 determines parameters (referred to as gait parameters) that specify some constituent elements of the desired gait, such as a desired foot position/posture trajectory and a desired floor reaction force vertical component trajectory, on the basis of the above required parameters, and then sequentially determines instantaneous values of the desired gait by using the gait parameters so as to generate a time series pattern of the desired gait.

In this case, a desired foot position/posture trajectory (to be more specific, a desired trajectory of each spatial component (X-axis component or the like) of the position and the posture of a foot) is generated for each foot 22 by using a finite-duration setting filter proposed in Patent No. 3233450 by the present applicant. This finite-duration setting filter includes a plurality of stages (3 stages or more in the first reference example) of first-order lag filters of variable time constants, that is, filters represented in terms of a transfer function of $1/(1+\tau s)$ (τ is a variable time constant. Hereinafter, the filter will be referred to as a unit filter), the plurality of stages of the filters

being connected in series. This arrangement makes it possible to generate and output a trajectory that reaches a specified value at desired specified time. In this case, every time constant τ of the unit filter of each stage is

5 variably set in sequence according to remaining time until the above specified time after starting the generation of an output of the finite-duration setting filter. More specifically, the setting is made such that, the value of τ is decreased from a predetermined initial value (>0) as

10 the remaining time reduces, and the value of τ finally reaches zero at the specified time at which the remaining time reaches zero. A step input of a height based on the specified value (more specifically, a change amount from an initial value to the specified value of an output of

15 the finite-duration setting filter) is supplied to the finite-duration setting filter. The finite-duration setting filter not only generates an output that reaches a specified value at specified time but also makes it possible to set a changing rate of an output of the

20 finite-duration setting filter at specified time to zero or substantially zero. Especially when three stages or more (three stages will do) of the unit filters are connected, the changing acceleration (a differential value of a changing rate) of an output of the finite-duration

25 setting filter can be reduced to zero or substantially zero.

The desired foot position/posture trajectory

generated by the finite-duration setting filter as described above is the desired position/posture trajectory of each foot 22 on a supporting leg coordinate system, which is fixed on a floor surface and which is to be discussed later.

The desired foot position/posture trajectory generated as described above is generated such that the position of each foot 22 begins moving, while gradually accelerating from the initial in-contact-with-the-ground state (the state at the initial time of a desired gait) toward an expected landing position. The desired foot position/posture trajectory is generated such that the changing rate of the position is gradually decelerated to zero or substantially zero until the expected landing time is finally reached, and the expected landing position is reached at the expected landing time, stopping the movement. Hence, the ground speed at the moment each foot 22 lands becomes zero or substantially zero (the changing rate of the position of each foot 22 on the supporting leg coordinate system secured to a floor). Accordingly, a landing impact will be low even when the robot 1 lands from the state wherein all legs 2, 2 are simultaneously present in the air (the state in the floating period) in a running gait.

In the aforesaid running gait, the vertical velocity of the body 3 switches downward from the latter half of the floating period due to the gravity acting on the robot

1, and remains downward at the time of landing. Therefore,
the relative velocity of the foot 22 of a free leg with
respect to the body 3 switches upward immediately before
landing if the desired foot position/posture trajectory is
5 generated such that the ground speed at the moment each
foot 22 lands reaches zero or substantially zero, as
described above, and if the desired position/posture
trajectory of the body 3 is generated to satisfy a dynamic
balance condition, as will be discussed later. This means
10 that the desired gait of the robot 1 is such that the
robot 1 lands, withdrawing the leg 22 that is a free leg
toward the body 3. In other words, according to the
desired gait in the first reference example, the robot 1
lands while pulling the foot 22 up, as observed from the
15 body 3, so that the ground speed of the foot 22 of the
free leg reaches zero or substantially zero. This
restrains a landing impact to prevent the landing impact
from becoming excessive.

Furthermore, in the first reference example, the
20 finite-duration setting filter is composed of three stages
of more (e.g., three stages) of the unit filters connected
in series, so that the velocity of each foot 22 (the
changing rate of a foot position) reaches zero or
substantially zero by expected landing time and the
25 acceleration of each foot 22 also reaches zero or
substantially zero at the expected landing time when the
movement stops. This means that the ground acceleration

also becomes zero or substantially zero at the landing instant. Hence, the landing impact will be further restrained. Especially, even if actual landing time of the robot 1 deviates from desired landing time, the impact
5 no longer increases much. Supplementally, the number of stages of the unit filters of the finite-duration setting filter may be two to make setting so that the ground speed of each foot 22 reaches zero or substantially zero at expected landing time. In this case, however, the
10 acceleration of each foot 22 at expected landing time does not usually become zero.

Regarding a foot posture, after each foot 22 lands at its heel at expected landing time, the foot continues to move until substantially the entire sole of the foot 22
15 comes in contact with a floor. For this reason, the time at which substantially the entire sole of the foot 22 comes in contact with the floor is set to the above specified time, and the foot posture trajectory is generated by the finite-duration setting filter.

20 In the first reference example, the foot position trajectory has been generated using the finite-duration setting filter. Alternatively, however, a desired foot position trajectory may be generated using a function, such as a polynomial, that is set such that the changing
25 rate of a foot position at the expected landing time (a time differential value of a foot position) reaches zero or substantially zero and further the changing

acceleration of the foot position at the expected landing time (a time differential value of the changing rate) reaches zero or substantially zero. This applies also to the generation of a desired foot posture trajectory.

5 However, regarding the generation of the desired foot posture trajectory, a function, such as a polynomial, is set such that the changing rate of the posture of each foot 22 and the changing acceleration thereof reaches zero or substantially zero at the time when substantially the
10 entire sole of each foot 22 comes in contact with a floor, as described above.

A desired floor reaction force vertical component trajectory is set as shown in, for example, Fig. 6. In the first reference example, the shape of a desired floor
15 reaction force vertical component trajectory in a running gait (strictly speaking, the shape in a single stance period) is specified to be trapezoidal (a shape projecting to an increasing side of a floor reaction force vertical component). The height of the trapezoid and the time of a
20 bending point are regarded as gait parameters defining a desired floor reaction force vertical component trajectory, and the gait parameters (floor reaction force vertical component trajectory parameters) are determined. In a floating period of a running gait, the desired floor
25 reaction force vertical component is steadily set to zero. A desired floor reaction force vertical component trajectory is desirably set so that it is virtually

continuous (so that values are not discontinuous), as in the case of the present example. This is for ensuring smooth operations of joints of the robot 1 when controlling a floor reaction force. The term "virtually continuous" means that a skipped value that inevitably takes place when a trajectory that is continuous in an analog fashion (a continuous trajectory in a true meaning) is digitally expressed by a discrete-time system does not cause the continuity of the trajectory to be lost.

10 A desired ZMP trajectory is set as follows. In the running gait shown in Fig. 5, the robot 1 lands at the heel of the foot 22 of a supporting leg, and then kicks at the tiptoe of the foot 22 of the supporting leg to jump into the air. Lastly, the robot 1 lands at the heel of
15 the foot 22 of a free leg, as described above. Therefore, as shown in the upper diagram of Fig. 7, the desired ZMP trajectory in the single stance period is set such that it takes the heel of the foot 22 of the supporting leg as its initial position, and then extends to the center in the
20 longitudinal direction of the foot 22 in the period in which substantially the entire sole of the foot 22 of the supporting leg comes on contact with the ground, and thereafter, reaches the tiptoe of the foot 22 of the supporting leg by floor leaving time. Here, the upper
25 diagram of Fig. 7 shows a desired ZMP trajectory in an X-axis direction (longitudinal direction), while a lower diagram of Fig. 7 shows a desired ZMP trajectory in a Y-

axis direction (lateral direction). The desired ZMP trajectory in the Y-axis direction in a single stance period is set at the same position as the central position of an ankle joint of a supporting leg 2 in the Y-axis direction, as shown in the lower diagram of Fig. 7.

In a running gait, after a single stance period ends, both legs 2, 2 leave a floor, and the floor reaction force vertical component becomes zero. When the floor reaction force vertical component is zero, that is, during a floating period, the total center of gravity of the robot 1 is subject to free fall motion, and an angular momentum change about the total center of gravity is zero. At this time, the moment of a resultant force of gravity and an inertial force that acts on the robot 1 is zero at an arbitrary point of a floor, so that a desired ZMP is indefinite. This means that any point of the floor satisfies a condition of ZMP represented by "a point of action at which the horizontal component of the moment, in which a resultant force of gravity and an inertial force acts, is zero." In other words, setting the desired ZMP at an arbitrary point satisfies a dynamic balance condition in that the horizontal component of the moment in which the above resultant force acts about the desired ZMP is zero. Hence, the desired ZMP may be set discontinuously. For example, the desired ZMP may be set so that it does not move from a desired ZMP position when leaving a floor (when a single stance period ends) in a

floating period, and it moves discontinuously (in steps) to a desired ZMP position for landing at the end of the floating period. In the first reference example, however, the position of the desired ZMP trajectory in the X-axis direction in a floating period has been set so as to continuously move to the landing position of the heel of the foot 22 of a free leg from the tiptoe of the foot 22 of a supporting leg by the time the next free leg 2 lands, as shown in the upper diagram of Fig. 7. Further, as shown in the lower diagram of Fig. 7, the position of the desired ZMP trajectory in the Y-axis direction in a floating period has been set so as to continuously move to the Y-axis directional position of the center of the ankle joint of a free leg from the Y-axis directional position of the center of the ankle joint of a supporting leg 2 by the time the next free leg 2 lands. In other words, the desired ZMP trajectory has been set so that it is continuous (virtually continuous) in all periods of a gait. As it will be discussed hereinafter, a desired gait has been generated so that a moment of the resultant force of gravity and an inertial force (excluding a vertical component) about the desired ZMP becomes zero (to be more specific, a desired body position/posture trajectory has been adjusted). Taking an approximation error into account, the desired ZMP trajectory is desirably set to be continuous (virtually continuous) also in a floating period in order to ensure a smooth generated gait.

However, a dynamic model, which is used in the first reference example and which will be discussed later, makes it possible to uniquely generate a desired gait that sets the horizontal component of a moment about a desired ZMP at a certain value (the value is zero in the first reference example, whereas it is not necessarily zero in embodiments, which will be described hereinafter) independently of the position of a desired ZMP. Therefore, the desired ZMP does not have to be always continuous.

In the first reference example, the positions and time of the bending points of the desired ZMP trajectory as shown in Fig. 7 are set as ZMP trajectory parameters (parameters defining the desired ZMP trajectory). The meaning of "virtually continuous" of the aforementioned ZMP trajectory is the same as that in the case of the above floor reaction force vertical component trajectory.

The ZMP trajectory parameters are determined such that a high stability margin is secured and no sudden change takes place. Here, a state in which a desired ZMP exists near the center of a least convex polygon (so-called supporting polygon) that includes a ground contact surface of the robot 1 indicates a high safety margin (refer to Japanese Unexamined Patent Application Publication No. 10-86081 for more detail). The desired ZMP trajectory shown in Fig. 7 has been set to meet such a condition.

A desired body position/posture, a desired foot

position/posture, and a reference body posture, which will be discussed hereinafter, are described in terms of a global coordinate system. The global coordinate system is a coordinate system fixed to a floor. More specifically,
5 a supporting leg coordinate system to be discussed hereinafter is used as the global coordinate system.

In the first reference example, the gait generating device 100 generates a reference body posture in addition to a desired body posture. The reference body posture is
10 a body posture generated directly on the basis of requests regarding a gait (requests from a unit, such as an action scheduler, or from an external source (the joystick 73 or the like) sent to the gait generating device 100).

A desired body posture (representing hereinafter a
15 desired body posture unless "reference" is added) is generated such that it follows or agrees with a reference body posture in a long term.

In walking, generally, a desired body posture may be always set to agree with a reference body posture as in
20 the case of an embodiment disclosed in the description of PCT Kokai publication WO/02/40224. Although the PCT Kokai publication WO/02/40224 does not refer to the concept of the reference body posture, it explicitly and preferentially gives desired body posture patterns, which
25 is equivalent to steady agreement of desired body postures with a reference body posture.

However, in a gait including a floating period, as in

running, or walking on a low-friction floor surface,
simply adjusting a body horizontal acceleration or the
like is not enough to satisfy a dynamic balance condition
while maintaining a floor reaction force horizontal
5 component and a floor reaction force vertical component of
a desired gait within a permissible range (or within a
friction limit) at the same time.

In the first reference example, therefore, a desired
body posture is deliberately deviated from a reference
10 body posture, as necessary. To be more specific, motion
modes explained below are generated in a combined manner
so as to satisfy the dynamic balance condition while
having a floor reaction force horizontal component and a
floor reaction force moment vertical component of a
15 desired gait falling within a permissible range (or within
a friction limit).

As shown in Fig. 8, when the robot 1 is in a certain
motion state, if only a body horizontal acceleration is
perturbated (slightly changed), a total center-of-gravity
20 horizontal acceleration and an angular momentum about the
total center-of-gravity of the robot 1 are perturbated.
More specifically, perturbating the body horizontal
acceleration perturbates the floor reaction force moment
horizontal component about a desired ZMP (a component
25 about the horizontal axis) and the floor reaction force
horizontal component without perturbating the floor
reaction force vertical component that dynamically

balances with a resultant force of an inertial force and gravity of the robot 1 produced by the perturbation of the body horizontal acceleration (without perturbing a total center-of-gravity vertical acceleration of the robot 1).

5 The motion mode that perturbs the body horizontal acceleration of the robot 1 as described above is referred to as a body translational mode.

In other words, a motion in which the floor reaction force moment horizontal component about the desired ZMP
10 and the floor reaction force horizontal component are changed without changing the floor reaction force vertical component is referred to as the body translational mode. In the body translational mode, the floor reaction force moment vertical component (the component about the
15 vertical axis) is also perturbed; however, no attention will be paid to this aspect in this case.

A change in the floor reaction force moment horizontal component per unit acceleration at this time is denoted by ΔM_p and a change in the floor reaction force
20 horizontal component per unit acceleration is denoted by ΔF_p . If the body 3 is horizontally accelerated forward in the situation illustrated in Fig. 8, then ΔM_p and ΔF_p act in the directions of the arrows shown in Fig. 8.

To facilitate perceptual understanding, the floor
25 reaction force that balances with the resultant force of an inertial force and gravity generated by a motion has been used for expression. However, it is theoretically

more accurate to express using the resultant force of an inertial force and gravity. The above resultant force and the floor reaction force have the same magnitude but opposite directions.

5 In comparison with the above, if the body inclination angular acceleration (the angular acceleration of the inclination angle of the body 3) is perturbed about a certain point P_r from a certain motion state of the robot 1, as shown in Fig. 9, then the angular momentum
10 (excluding the component about the vertical axis) about the total center-of-gravity is perturbed, while the total center-of-gravity of the robot 1 is not perturbed. This means that perturbing the body inclination angle acceleration about the point P_r perturbs the floor
15 reaction force moment horizontal component about a desired ZMP without perturbing the floor reaction force vertical component and the floor reaction force horizontal component. The motion mode in which the body inclination angle acceleration of the robot 1 is perturbed as
20 described above is referred to as the body inclination mode.

 In other words, the motion in which the floor reaction force moment horizontal component about a desired ZMP is changed without changing a floor reaction force
25 vertical component and a floor reaction force horizontal component is called the body inclination mode.

 A change in the floor reaction force moment

horizontal component per unit angular acceleration at this time is denoted by ΔM_r and a change in the floor reaction force horizontal component per unit angular acceleration is denoted by ΔF_r . ΔF_r is zero. If an angular acceleration of a body inclination angle is generated to cause the body 3 to lean forward in the situation shown in Fig. 9, then ΔM_r acts in the direction of the arrow shown in Fig. 9.

Further, if a body yaw angle acceleration (the rotational angular acceleration about the vertical axis of the body 3) is perturbed about a certain point P_q from a certain motion state of the robot 1, as shown in Fig. 10, then the angular momentum vertical component about the total center-of-gravity is perturbed, while the total center-of-gravity of the robot 1 is not perturbed.

Incidentally, if the total center-of-gravity of the robot 1 is not perturbed, then the perturbation of the angular momentum vertical component does not depend on a point of action. Hence, perturbing the body yaw angular

acceleration about the point P_q perturbs the floor reaction force moment vertical component about a desired ZMP without perturbing the floor reaction force vertical component, the floor reaction force horizontal component, and the floor reaction force moment horizontal component.

The motion mode in which the body yaw angular acceleration of the robot 1 is perturbed as described above is referred to as the body yaw rotation mode.

In other words, the body motion in which the floor reaction force moment vertical component about a desired ZMP is changed without changing a floor reaction force vertical component, a floor reaction force horizontal component, and a floor reaction force moment horizontal component is called the body yaw rotation mode.

A change in the floor reaction force moment vertical component per unit angular acceleration at this time is denoted by ΔM_{bz} , and a change in the floor reaction force horizontal component per unit angular acceleration is denoted by ΔF_b . ΔF_b is zero. If the body 3 is rotated in the direction of the arrow at the unit angular acceleration (rotated at an angular acceleration $\beta_b=1$) in the situation shown in Fig. 10, then ΔM_{bz} acts in the direction of the arrow shown in Fig. 10.

In the motion shown in Fig. 10, the body 3 has been rotated so that the positions of the distal ends of both arms 5, 5 remain unchanged as observed from the supporting leg coordinate system (the coordinate system fixed to a floor). However, a motion in which an arm 5 is rotated together with the body 3 without changing the relative position/posture of the arm 5 in relation to the body 3 may be defined as the body yaw rotation mode. In this case, however, a motion equation to be discussed hereinafter has to be slightly changed.

Further, if the distal ends of both arms 5, 5 are perturbed longitudinally in opposite directions from

each other from a motion state of the robot 1, as illustrated in Figs. 11 (a) and (b), then the angular momentum vertical component about the total center-of-gravity is perturbed, while the total center-of-gravity of the robot 1 is not perturbed. Hereinafter, this motion mode will be referred to as an antiphase arm swing mode. In other words, the arm swing motion mode in which the floor reaction force moment vertical component about a desired ZMP is perturbed without perturbing a floor reaction force vertical component, a floor reaction force horizontal component, and a floor reaction force moment horizontal component is referred to as the antiphase arm swing mode.

A motion in which a right arm 5R is moved forward by a unit amount and a left arm 5L is moved backward by a unit amount is referred to as an antiphase arm swing of a unit angle. Figs. 11 (a) and (b) illustrate a state wherein an antiphase arm swing angle is θ_{az} .

A change in the floor reaction force moment vertical component per unit angular acceleration in the antiphase arm swing mode is denoted by ΔM_{az} , and a change in the floor reaction force horizontal component per unit angular acceleration is denoted by ΔF_a . ΔF_a is zero. In the situation shown in Figs. 11 (a) and (b), if the right arm 5R is accelerated forward, while the left arm 5L is accelerated backward (swinging at an angular acceleration $\beta_a > 0$), then a floor reaction force moment vertical

component M_{az} acts in the direction of the arrow (a positive direction of the vertical axis) shown in Fig. 11 (a).

A description will now be given of a dynamic model of the robot 1 used in the first reference example. In the first reference example, a simplified (approximated) dynamic model shown below is used. However, regarding the dynamic model shown below, a kinematics model (a model representing the structures and dimensions of joints and links, i.e., a model representing a relationship between joint displacements and the positions/postures of links) will be also necessary.

Fig. 12 shows a dynamic model of the robot 1 used in the first reference example. As illustrated, the dynamic model is a model composed of a total of three mass points, namely, two mass points $2m$, $2m$ corresponding to the legs 2 of the robot 1 and a mass point $3m$ corresponding to the body 3, and four flywheels FH_x , FH_y , FH_{bz} , and FH_{az} having inertias but no mass. The flywheels FH_x , FH_y , FH_{bz} , and FH_{az} can be rotated about an X-axis (longitudinal axis), a Y-axis (lateral axis), a Z-axis (vertical axis), and a Z-axis (vertical axis), respectively. This dynamic model is decoupled, that is, the dynamic model is constructed such that the dynamics (the dynamics of the mass points $2m$, $2m$) of the legs 2, 2, the dynamics of the body 3 (the dynamics of the mass point $3m$ and the flywheels FH_x , FH_y and FH_{bz}), and the dynamics of the arms 5, 5 (the dynamics of the

flywheel FHaz) do not interfere with each other, and the dynamics of the entire robot 1 is represented by their linear connection. In addition, a relationship between a motion of the body 3 and a floor reaction force is

5 separated into a relationship between a translational motion of the body 3 (body translation mode) and a floor reaction force, a relationship between an inclination motion of the body 3 (body inclination mode) and a floor reaction force, a relationship between a yaw rotational

10 motion of the body 3 (body yaw rotation mode) and a floor reaction force, and a relationship between an antiphase arm swing motion of both arms 5, 5 (antiphase arm swing mode) and a floor reaction force. To be more specific, a floor reaction force generated by a horizontal motion of

15 the body mass point 3m corresponds to a floor reaction force generated by a horizontal translational motion of the body 3 (body translation mode), and a floor reaction force generated by a rotational motion of the flywheels FHx and FHy corresponds to a floor reaction force

20 generated by a rotational motion of an inclination angle of the body 3 (body inclination mode). The rotational motion of the flywheel FHx corresponds to the rotational motion of an inclination angle of the body 3 in the roll direction (about the X-axis), and the rotational motion of

25 the flywheel FHy corresponds to the rotational motion of an inclination angle of the body 3 in the pitch direction (about the y-axis). A floor reaction force generated by

the rotational motion of the flywheel FHbz corresponds to a floor reaction force generated by a yaw rotational motion of the body 3 (the body yaw rotation mode). A floor reaction force generated by the rotational motion of the flywheel FHaz corresponds to a floor reaction force generated by an antiphase arm swing motion (the antiphase arm swing mode).

The mass of the arms of the robot 1 is assumed to be included in the body 3, and the body mass point 3m has a mass that includes the mass of the arms 5, 5.

For the convenience of explanation, variables and parameters related to the dynamic model will be defined as follows. Each of the mass points 2m, 2m and 3m corresponds to a representative point of a part with which it is associated or a point uniquely decided geometrically from the position/posture of the part. For instance, the position of the mass point 2m of a supporting leg 2 is defined as the point above the aforesaid representative point of the sole of the foot 22 of the leg 2 by a predetermined distance.

Zsup: Supporting leg mass point vertical position

Zswg: Free leg mass point vertical position

Zb: Body mass point vertical position (usually different from a vertical body position)

ZGtotal: Overall gravitational center vertical position

Xsup: Supporting leg mass point X position

Ysup: Supporting leg mass point Y position

Xswg: Free leg mass point X position

Yswg: Free leg mass point Y position

Xb: Body mass point X position (The body mass point position is the position offset by a predetermined

5 distance in the longitudinal direction of the body from the aforesaid point Pr. The offset is determined such that the gravitational center position of an exact model and the gravitational center position of the present dynamic model agree with each other as much as possible in
10 an upright stance or the like. This is usually different from a horizontal body position.)

Yb: Body mass point Y position

XGtotal: Overall gravitational center horizontal X position

15 YGtotal: Overall gravitational center horizontal Y position

θ_{bx} : Body inclination angle about X-axis relative to vertical direction

θ_{by} : Body inclination angle about Y-axis relative to
20 vertical direction

θ_{bz} : Body yaw rotational angle

θ_{az} : Antiphase arm swing angle

m_b : Body mass point mass

m_{sup} : Supporting leg mass point mass

25 m_{swg} : Free leg mass point mass

m_{total} : Total mass of robot (= m_{total} + m_{sup} + m_{swg})

J: Body inertial moment (Equivalent inertial moment in the

body inclination mode. In other words, this is an inertial moment of FH_x and FH_y . Usually, it does not agree with the inertial moment of the body 3 part of the actual robot 1.)

5 J_{bz} : Body inertial moment about a vertical axis
(Equivalent inertial moment in the body yaw rotation mode. Usually, this does not agree with the inertial moment of the body 3 part of the actual robot 1.)

J_{az} : Arm swing inertial moment about a vertical axis
10 (Equivalent inertial moment in antiphase arm swing to cancel a spin. In other words, it is an inertial moment of FH_z .)

F_x : Floor reaction force X component (More specifically, a longitudinal (X-axis) component of a translational floor
15 reaction force)

F_y : Floor reaction force Y component (More specifically, a lateral (Y-axis) component of a translational floor reaction force)

F_z : Floor reaction force vertical component (More
20 specifically, a vertical (Z-axis) component of a translational floor reaction force. This is equivalent to a desired translational floor reaction force vertical component in the first reference example.)

M_x : X component of a floor reaction force moment about a
25 desired ZMP (More specifically, a component about a longitudinal axis (X-axis) of a floor reaction force moment)

My: Y component of a floor reaction force moment about a desired ZMP (More specifically, a component about a lateral axis (Y-axis) of a floor reaction force moment)

Mz: Z component of a floor reaction force moment about a desired ZMP (More specifically, a component about a vertical axis (Z-axis) of a floor reaction force moment)

An X position and a Y position of each of the mass points 2m and 3m mean a position in the longitudinal direction (X-axis direction) and a position in the lateral direction (Y-axis direction), respectively. In the first reference example, a positional relationship between a position of the mass point 2m of each leg 2 and a position of the foot 22 of the leg 2 (a position of a predetermined representative point of the foot 22) is determined in advance, so that one of the positions is decided, then the other position is uniquely decided. Further, a positional relationship between the body mass point 3m and the position of the body 3 (a position of a predetermined representative point of the body 3) is determined in advance on the basis of a posture angle of the body 3 (hereinafter, regarding the body, a posture angle will mean an inclination angle and a yaw angle), and if a position and a posture angle of one of them are determined, then a position of the other is uniquely determined.

For an arbitrary variable X, dX/dt denotes first order differentiation of X, and d^2X/dt^2 denotes second order differentiation. Therefore, if the variable X

denotes displacement, then dx/dt means velocity and d^2x/dt^2 means acceleration. g denotes a gravity acceleration constant. Here, g takes a positive value.

A motional equation of the above dynamic model (an equation expressing a dynamic balance condition) is represented by equation 01, equation 02x, equation 02y, equation 03x, equation 03y, and equation 03z.

$$F_z = m_b \cdot (g + d^2Z_b/dt^2) + m_{sup} \cdot (g + d^2Z_{sup}/dt^2) + m_{swg} \cdot (g + d^2Z_{swg}/dt^2) \quad \text{..... Equation 01}$$

$$F_x = m_b \cdot d^2X_b/dt^2 + m_{sup} \cdot d^2X_{sup}/dt^2 + m_{swg} \cdot d^2X_{swg}/dt^2 \quad \text{..... Equation 02x}$$

$$F_y = m_b \cdot d^2Y_b/dt^2 + m_{sup} \cdot d^2Y_{sup}/dt^2 + m_{swg} \cdot d^2Y_{swg}/dt^2 \quad \text{..... Equation 02y}$$

$$\begin{aligned} M_x = & m_b \cdot (Y_b - Y_{zmp}) \cdot (g + d^2Z_b/dt^2) \\ & - m_b \cdot (Z_b - Z_{zmp}) \cdot (d^2Y_b/dt^2) \\ & + m_{sup} \cdot (Y_{sup} - Y_{zmp}) \cdot (g + d^2Z_{sup}/dt^2) \\ & - m_{sup} \cdot (Z_{sup} - Z_{zmp}) \cdot (d^2Y_{sup}/dt^2) \\ & + m_{swg} \cdot (Y_{swg} - Y_{zmp}) \cdot (g + d^2Z_{swg}/dt^2) \\ & - m_{swg} \cdot (Z_{swg} - Z_{zmp}) \cdot (d^2Y_{swg}/dt^2) + J \cdot d^2\theta_{bx}/dt^2 \end{aligned} \quad \text{..... Equation 03x}$$

$$\begin{aligned} M_y = & -m_b \cdot (X_b - X_{zmp}) \cdot (g + d^2Z_b/dt^2) \\ & + m_b \cdot (Z_b - Z_{zmp}) \cdot (d^2X_b/dt^2) \\ & - m_{sup} \cdot (X_{sup} - X_{zmp}) \cdot (g + d^2Z_{sup}/dt^2) \end{aligned}$$

$$\begin{aligned} &+m_{sup}*(Z_{sup}-Z_{zmp})*(d^2X_{sup}/dt^2) \\ &-m_{swg}*(X_{swg}-X_{zmp})*(g+d^2Z_{swg}/dt^2) \\ &+m_{swg}*(Z_{swg}-Z_{zmp})*(d^2X_{swg}/dt^2)+J*d^2\theta_{by}/dt^2 \end{aligned}$$

..... Equation 03y

5

$$\begin{aligned} M_z = & m_b*(X_b-X_{zmp})*(d^2Y_b/dt^2)-m_b*(Y_b-Y_{zmp})*(d^2X_b/dt^2) \\ & +m_{sup}*(X_{sup}-X_{zmp})*(d^2Y_{sup}/dt^2) \\ & -m_{sup}*(Y_{sup}-Y_{zmp})*(d^2X_{sup}/dt^2) \\ & +m_{swg}*(X_{swg}-X_{zmp})*(d^2Y_{swg}/dt^2) \\ 10 \quad & -m_{swg}*(Y_{swg}-Y_{zmp})*(d^2X_{swg}/dt^2) \\ & +J_{bz}*d^2\theta_{bz}/dt^2+J_{az}*d^2\theta_{az}/dt^2 \end{aligned}$$

..... Equation 03z

Furthermore, for a total center-of-gravity position
15 of the robot, the following relational expressions hold:

$$Z_{Gtotal}=(m_b*Z_b+m_{sup}*Z_{sup}+m_{swg}*Z_{swg})/m_{total}$$

..... Equation 04

$$X_{Gtotal}=(m_b*X_b+m_{sup}*X_{sup}+m_{swg}*X_{swg})/m_{total}$$

..... Equation 05x

$$20 \quad Y_{Gtotal}=(m_b*Y_b+m_{sup}*Y_{sup}+m_{swg}*Y_{swg})/m_{total}$$

..... Equation 05y

The following will show a relationship between the
above dynamic model and the above ΔF_p , ΔM_p , ΔF_r , and ΔM_r .

25 The above ΔF_p is a perturbation amount of F_x or F_y
when d^2X_b/dt^2 or d^2Y_b/dt^2 is perturbed by a unit amount
in equation 02x or equation 02y, so that it is determined

according to the following equation:

$$\Delta F_p = m_b \quad \dots \text{Equation 06}$$

This means that the change ΔF_p of a floor reaction force horizontal component per unit acceleration in the direction of each horizontal axis (X-axis, Y-axis) in the body translation mode corresponds to the mass of the body mass point $3m$ of the dynamic model.

The above ΔM_p is a perturbation amount of M_y or M_x when d^2X_b/dt^2 or d^2Y_b/dt^2 is perturbed by a unit amount in equation 03y or equation 03x, so that it is determined according to the following equation:

$$\Delta M_p = m_b \cdot (Z_b - Z_{zmp}) \quad \dots \text{Equation 07}$$

This means that the change ΔM_p of a floor reaction force moment horizontal component per unit acceleration in the direction of each horizontal axis (X-axis, Y-axis) in the body translation mode is obtained by multiplying a body mass point mass of the dynamic model by a height (vertical position) of the body mass point $3m$ from a desired ZMP.

The relationship between the positions of the body mass point $3m$ and the desired ZMP and the motion of the body mass point $3m$ corresponds to the behavior of an inverted pendulum obtained when the body mass point $3m$ is associated with an inverted pendulum mass point and when the desired ZMP is associated with an inverted pendulum supporting point. To be more accurate, ΔM_p in the Y-axis direction is obtained by reversing the sign of the right side of equation 07.

The above ΔFr is a perturbation amount of F_x or F_y when $d^2\theta_{by}/dt^2$ is perturbed by a unit amount in equation 02x or equation 02y, so that it is determined according to the following equation:

5 $\Delta Fr = 0$... Equation 08

This means that the change ΔFr of a floor reaction force horizontal component per unit acceleration in the direction of each horizontal axis (X-axis, Y-axis) in the body inclination mode is zero.

10 The above ΔMr is a perturbation amount of M_x or M_y when $d^2\theta_{bx}/dt^2$ or $d^2\theta_{by}/dt^2$ is perturbed by a unit amount in equation 03x or equation 03y, so that it is determined according to the following equation:

$\Delta Mr = J$... Equation 09

15 This means that the change ΔMr of a floor reaction force moment horizontal component per unit acceleration in the direction of each horizontal axis (X-axis, Y-axis) in the body inclination mode corresponds to the inertial moments of horizontal axis flywheels (FH_x and FH_y).

20 The above ΔMb_z is a perturbation amount of M_z when $d^2\theta_{bz}/dt^2$ is perturbed by a unit amount in equation 03z, so that it is determined according to the following equation:

$\Delta Mb_z = Jb_z$... Equation 09b

25 This means that the change ΔMb_z of a floor reaction force moment component per unit acceleration in the body yaw rotation mode corresponds to the inertial moment of a

flywheel FHBz corresponding to body yaw rotation.

The above ΔM_{az} is a perturbation amount of M_z when $d^2\theta_{az}/dt^2$ is perturbed by a unit amount in equation 03z, so that it is determined according to the following
5 equation:

$$\Delta M_{az} = J_{az} \dots \text{Equation 09a}$$

This means that the change ΔM_{az} of a floor reaction force moment component per unit angular acceleration of an antiphase arm swing corresponds to the inertial moment of
10 a flywheel FHBz corresponding to an arm swing.

The gait generating device 100 in the first reference example generates a desired gait for one step in order, the desired gait (the desired gait in the narrow sense described above) for one step from the moment one leg 2 of
15 the robot 1 lands to the moment the other leg 2 lands. Hence, for the running gait shown in Fig. 5 to be generated in the first reference example, a desired gait from the beginning of a single stance period to the end of the following floating period (the beginning of the next
20 single stance period) is generated in sequence. Here, a desired gait that is being newly generated will be referred to as a "current time gait," the next desired gait will be referred to as a "next gait," and a desired gait after next will be referred to as a "next but one
25 time gait." Furthermore, a desired gait generated one step before the "current time gait" will be referred to as a "last time's gait."

When the gait generating device 100 newly generates a current time gait, expected positions/postures of landing of the foot 22 of a free leg and required values (requests) of expected landing time for the next two steps of the robot 1 are input as required parameters to the gait generating device 100 (or the gait generating device 100 reads the required parameters from a memory). Then, the gait generating device 100 uses these required parameters to generate a desired body position/posture trajectory, a desired foot position/posture trajectory, a desired ZMP trajectory, a desired floor reaction force vertical component trajectory, a desired arm posture trajectory, etc. At this time, some of the gait parameters specifying these trajectories are corrected, as necessary, to secure continuity of walking.

Taking the generation of the running gait shown in Fig. 5 as an example, gait generation processing of the gait generating device 100 in the first reference example will be explained in detail with reference to Fig. 13 to Fig. 46. Fig. 13 is a flowchart (structured flowchart) illustrating a main routine of the gait generation processing carried out by the gait generating device 100.

First, various initializing operations, including initialization of time t to zero, are performed in S010. This processing is implemented primarily when starting up the gait generating device 100. Next, the processing proceeds to S014 via S012 and waits for a timer interrupt

for each control cycle (the calculation processing cycle of the flowchart shown in Fig. 13). The control cycle is denoted by Δt .

5 Then, the processing proceeds to S016 and determines whether a shift in a gait is taking place. If a shift in the gait is taking place, then the processing proceeds to S018, or if a shift in a gait is not taking place, then it proceeds to S030. Here, "the shift in a gait" means a timing at which the generation of the last time's gait has
10 been completed and the generation of the current time gait is about to start. For instance, a control cycle following the control cycle in which the generation of a last time's gait has been completed refers to the shift in a gait.

15 When proceeding to S018, time t is initialized to zero. The gait generating device 100 then proceeds to S020 and reads a next time gait's supporting leg coordinate system, a next but one time gait's supporting leg coordinate system, a current time gait cycle, and a
20 next time gait cycle. These supporting leg coordinate systems and the gait cycles are determined by the above required parameters. More specifically, in the first reference example, the required parameters supplied to the gait generating device 100 from the joystick 73 or the
25 like include required values of expected landing positions/postures (foot positions/postures in a state wherein the foot 22 has been rotated without slippage such

that its sole is substantially in full contact with a floor surface after landing) and expected landing time of the foot 22 of a free leg for up to two steps ahead. The required value for the first step and the required value
5 for the second step are supplied to the gait generating device 100 as the values associated with a current time gait and a next gait, respectively, before the generation of the current time gait is begun (the shift in a gait in S016 mentioned above). These required values can be
10 changed in the middle of generating the current time gait.

Then, the next time gait's supporting leg coordinate system is determined on the basis of the required value of the expected landing position/posture of the free leg foot 22 of the first step (the free leg foot 22 in the current
15 time gait) in the above required parameters.

Referring to, for example, Fig. 16, it is assumed that the required value for an expected landing position/posture of the free leg foot 22 (22L in the figure) related to the current time gait (first step)
20 specifies a position/posture obtained by moving by x_{next} and y_{next} in the X-axis direction (in the longitudinal direction of a supporting leg foot 22R of the current time gait) and in the Y-axis direction (in the lateral direction of the supporting leg foot 22R of the current
25 time gait), respectively, of a current time's gait supporting leg coordinate system, and by rotating about the Z-axis (about the vertical axis) by θ_{znext} with

respect to a landing position/posture of the supporting leg foot 22 (22R in the figure) of the current time gait.

Here, the supporting leg coordinate system is a global coordinate system (a coordinate system fixed to a floor)

5 in which a point, at which a perpendicular line extended

onto a floor surface from the center of the ankle of a

supporting leg foot 2 intersects with the floor surface

(this point agreeing with a representative point of the

foot 22 in a state, wherein substantially the entire

10 surface of the sole of the supporting leg foot 22 is in

contact with the floor surface in the first reference

example), in a state wherein the supporting leg foot 22 is

set in a horizontal posture (more generally, a posture

parallel to the floor surface) and substantially the

15 entire surface of the sole of the supporting leg foot 22

is in contact (in close contact) with the floor surface,

is defined as an origin thereof, and a horizontal plane

passing the origin is defined as an XY plane. In this

case, the X-axis direction and the Y-axis direction

20 correspond to the longitudinal direction and the lateral

direction, respectively, of the supporting leg foot 22.

The origin of the supporting leg coordinate system does

not have to agree with the representative point of the

foot 22 (a point representing the position of the foot 22)

25 in the state wherein substantially the entire surface of

the sole of the supporting leg foot 22 is in contact with

the floor surface. Alternatively, the origin may be set

at a point on the floor surface that is different from the representative point.

At this time, the next time gait's supporting leg coordinate system is a coordinate system that takes, as
5 its origin, the representative point (more specifically, a point on a floor that agrees with the representative point) of the foot 22L in a case where the foot 22 is landed according to a required value of the expected landing position/posture of the free leg foot 22L of the
10 current time gait as illustrated (in a case where the representative point of the foot 22 is made to agree with the required value of an expected landing position and the posture (orientation) of the foot 22 is made to agree with the required value of an expected landing posture), the
15 longitudinal direction and the lateral direction of the foot 22L in the horizontal plane passing the origin corresponding to an X'-axis direction and Y'-axis direction, respectively.

In the same manner described above, a next but one
20 time gait's supporting leg coordinate system (refer to the X'' Y'' coordinates shown in Fig. 16) is determined on the basis of the required values for the expected landing position/posture of the free leg foot 22 of the second step. A current time gait cycle is determined as the
25 duration from the expected landing time (required value) of the supporting leg foot 22 of the current time gait to the expected landing time (required value) of the free leg

foot 22 of the first step (current time gait). The next time gait cycle is determined as the duration from the expected landing time (required value) of the free leg foot 22 of the first step to the expected landing time (required value) of the free leg foot 22 of the second step.

The required parameters are input to the gait generating device 100 by necessary manipulation of the joystick 73 in the first reference example. Alternatively, however, the required parameters or the positions/postures and gait cycles of the aforesaid supporting leg coordinate systems associated with the required parameters may be stored in advance as a travel schedule of the robot 1. Alternatively, the aforesaid next time and the next but one time gait's supporting leg coordinate systems and the current time and the next time gait cycles may be determined on the basis of commands (requests) from a control device, such as the joystick 73, and a travel history of the robot 1 up to that moment.

Subsequently, the processing proceeds to S022 and determines gait parameters of a normal turning gait as a virtual cyclic gait that follows the current time gait. The gait parameters include a foot trajectory parameter defining a desired foot position/posture trajectory, a reference body posture trajectory parameter defining a body posture trajectory to be based on, a reference arm posture trajectory parameter defining an arm posture

trajectory to be based on, a ZMP trajectory parameter defining a desired ZMP trajectory, and a floor reaction force vertical component trajectory parameter defining a desired floor reaction force vertical component trajectory in the normal turning gait. Furthermore, parameters that define a floor reaction force horizontal component permissible range and a floor reaction force moment vertical component permissible range are also included in gait parameters.

In the present description, "the normal turning gait" is used to mean a cyclic gait that does not cause discontinuity in motional states (states of foot position/posture, body position/posture, etc.) of the robot 1 in a boundary of gait when the gait is repeated (the boundary of a gait for each step in the first reference example). Hereinafter, "the normal turning gait" may be abbreviated as "the normal gait."

According to the first reference example, the normal turning gait, which is a cyclic gait, may be defined as follows. A gait for two steps of the robot 1, i.e., a gait composed of a first turning gait following a current time gait and a second turning gait following the first turning gait, as the gait for one cycle. The normal turning gait consists of a repetition of the gait for one cycle. The term "turning" is used here, because it would mean straight advancement when the turning rate is set to zero, and straight advancement can be also included in

turning in a broad sense. If a desired gait to be generated is the running gait shown in Fig. 5, then a current time gait of the desired gait is a running gait that has a single stance period and a floating period.

5 Hence, the first turning gait and the second turning gait of the normal turning gait are both gaits that also have a single stance period and a floating period, as in the current time gait. In other words, a basic gait form of the first turning gait and the second turning gait is the
10 same as the current time gait.

Supplemental explanation of the normal turning gait will be added. In a bipedal mobile robot, the normal turning gait for one cycle requires the gaits in the aforesaid narrow sense for at least two steps. It is
15 further possible to set a complicated normal turning gait using a gait for three steps or more as the gait for one cycle. The normal turning gait, however, is used only to determine a divergent component (to be discussed in detail hereinafter) at the end (finish time) of the current time
20 gait. For this reason, using the normal turning gait composed of a gait for three or more steps for one cycle will provide low effect despite the complicated processing for generating the gait. Therefore, the gait for one cycle in the normal turning gait in the first reference
25 example is composed of a gait for two steps (the first and the second turning gaits). For a legged mobile robot having three or more feet, the number of gaits for

defining the normal turning gait will increase accordingly.
In the following description, for the convenience of
explanation, the normal turning gait composed of a
plurality of gaits in the narrow sense (the gait for two
5 steps in the first reference example) will be regarded as
the gait for one step.

A normal turning gait is prepared, by the gait
generating device 100, for provisional use to determine
motional states of the robot 1, including a divergent
10 component or a vertical body position velocity at the end
of a current time gait, a body posture angle, and an
angular velocity thereof, and it is not directly output
from the gait generating device 100.

The term "divergent" means that the position of the
15 body 3 of the bipedal mobile robot 1 is undesirably
shifted to a position away from the positions of both feet
22 and 22, as shown in Fig. 14. The value of a divergent
component is a numeral value indicating how far the
position of the body 3 of the bipedal mobile robot 1 is
20 away from the positions of both feet 22 and 22 (to be more
specific, the origin of a global coordinate system (a
supporting leg coordinate system) set on the surface with
which a supporting leg foot 22 is in contact).

In the first reference example, gaits are generated
25 using a divergent component as an indicator so that a
desired gait can be continuously generated without causing
the divergence. However, even if it is an initial

divergent component (divergent component at initial time of the normal turning gait) of the normal gait, which is a typical example of a continuous gait (a cyclic gait that permits repetition of a gait of the same pattern without causing discontinuity of a gait trajectory, and that does not theoretically diverge after an infinite number of repetitions), the initial divergent component is not simply zero. The initial divergent component changes if a parameter of a normal gait changes. In other words, a proper divergent component changes according to a gait form, such as the manner of walking or the manner of running, or the like. In the first reference example, therefore, a normal gait following a current time gait to be generated is set on the basis of required parameters involved in the current time gait, and the initial divergent component of the normal gait is determined, and then a current time gait is generated such that the divergent component at the end of the current time gait agrees with the initial divergent component of the normal gait (more generally, the current time gait is made to continue or approximate to the normal gait). The basic guideline for generating such gaits is the same as that disclosed in PCT Kokai publication WO/02/40224 previously proposed by the present applicant.

The first reference example of the present invention does not use a linear dynamic model with three mass points used in the first embodiment of PCT Kokai publication

WO/02/40224. Nevertheless, the concept of the divergent component and a convergent component defined by the equation given below can be applied with adequate approximate accuracy to a perturbation of a behavior of a nonlinear dynamic model such as the one shown in Fig. 12.

Divergent component = Body mass point horizontal position + Body mass point horizontal velocity / ω_0

... Equation 10

Convergent component = Body mass point horizontal position - Body mass point horizontal velocity / ω_0'

... Equation 11

where the body mass point horizontal position in this case indicates a body mass point horizontal position X_b in the dynamic model shown in Fig. 12.

ω_0 and ω_0' take predetermined values. The values of these ω_0 and ω_0' are substantially the same, although they do not exactly coincide. Further, the values for generating walking gaits in PCT Kokai publication WO/02/40224 must be slightly changed for running.

More details of the divergent component and the convergent component have been given in PCT Kokai publication WO/02/40224, so that no more description will be given here.

In the first reference example, in addition to the method disclosed in PCT Kokai publication WO/02/40224, a gait parameter defining a desired floor reaction force vertical component trajectory is set, and a total center-

of-gravity vertical position of the robot 1 is determined so as to dynamically satisfy the desired floor reaction force vertical component, as will be discussed hereinafter. In this case, a second order integrated value of the floor reaction force vertical component will define the total center-of-gravity vertical position of the robot 1. Hence, if the desired floor reaction force vertical component is improperly set, then the total center-of-gravity vertical position or the vertical body position of the robot 1 will be too high or too low. Therefore, the method for setting a desired floor reaction force vertical component is also an important issue. However, the relationship between a floor reaction force vertical component and a vertical body position is similar to the relationship between ZMP and a horizontal body position, so that a part of a technique for determining a desired ZMP for setting a proper horizontal body position velocity can be applied to a technique for determining a desired floor reaction force vertical component for setting a proper vertical body position velocity simply by slightly changing a part thereof, as shown in the following first reference example.

Returning to the main subject, in S022, the processing below is carried out according to the flowchart shown in Fig. 15.

First, in S100, a foot trajectory parameter among the gait parameters of a normal gait is determined to provide a foot position/posture trajectory composed of a current

time gait, a first turning gait, and a second turning gait in succession in this order. The following will explain a specific setting method with reference to Fig. 16. In the following explanation, the foot 22 of a supporting leg 2 will be referred to as the supporting leg foot and the foot 22 of a free leg 2 will be referred to as the free leg foot. Further, "start" and "end" will mean start time and end time of a gait or instantaneous gaits at the start time and the end time.

The foot trajectory parameter is constructed primarily of the positions/postures of the supporting leg foot and the free leg foot, respectively, at the start and the end, respectively, of a first turning gait and a second turning gait, and a gait cycle of each turning gait. In the foot trajectory parameter, the free leg foot position/posture at the start of the first turning gait is defined as the supporting leg foot position/posture at the end of a current time gait observed from a next time gait's supporting leg coordinate system. In this case, the supporting leg foot 22 at the end of the current time gait is moving in the air in a running gait. And the supporting leg foot position/posture at the end of the current time gait is determined by generating a required value of an expected landing position/posture of the free leg foot 22 of a second step in the required parameter (a required value of an expected landing position/posture in a next time gait of the supporting leg foot 22 of the

current time gait) or a foot position/posture trajectory for reaching a free leg position/posture at the end of the next time gait determined on the basis of a next but time one gait's supporting leg coordinate system that

5 corresponds to the above required value (more specifically, the trajectory observed from a next time gait's supporting leg coordinate system) from the supporting leg foot position/posture at the start of the current time gait (= the free leg foot position/posture at the end of the last
10 time's gait) by using the finite-duration setting filter until the end of the current time gait.

The free leg foot position/posture at the end of the next time gait is determined such that the position/posture of the foot obtained when the foot 22 is
15 turned from that position/posture by a predetermined angle in the pitch direction until it reaches a horizontal posture by lowering its tiptoe while holding the foot 22 in contact with the ground agrees with the position/posture in the next but one time's gait

20 supporting leg coordinate system. In other words, the free leg foot position/posture at the end of the next time gait is the position/posture of the foot 22 in a state wherein the foot 22 has been turned, from a required value of the landing position/posture of the free leg foot 22 of
25 the second step in the required parameter, by a predetermined angle in the pitch direction by lifting its tiptoe while holding the foot 22 in contact with the

ground so that it does not slip (a state wherein the heel has been landed with the tiptoe lifted).

Further, the supporting leg foot position/posture at the start of the first turning gait is defined as the free
5 leg foot position/posture at the end of the current time gait observed from the next time gait's supporting leg coordinate system. In this case, the free leg foot position/posture at the end of the current time gait is determined on the basis of the above next time's gait
10 supporting leg coordinate system or a required value of an expected landing position/posture of the free leg of the first step (the current time gait) of the required parameter corresponding thereto, as in the case of the free leg foot position/posture at the end of the next time
15 gait. In other words, the free leg foot position/posture at the end of the current time gait is determined such that a representative point of the foot obtained when substantially entire surface of the sole of the foot 22 is brought into contact with a floor surface by turning the
20 foot 22 from the position/posture so as to lower its tiptoe while holding the foot 22 in contact with the ground agrees with the origin of the next time gait's supporting leg coordinate system.

The free leg foot position/posture at the end of the
25 first turning gait is determined on the basis of a position/posture on the next but one time gait's supporting leg coordinate system observed from the next

time's gait supporting leg coordinate system, as in the case of the technique for determining the free leg foot position/posture at the end of the current time gait or the free leg foot position/posture at the end of the next time gait. To be more specific, the free leg foot position/posture at the end of the first turning gait is determined such that the position/posture of the foot obtained when the foot 22 is turned from that position/posture by a predetermined angle until it reaches a horizontal posture while avoiding a slippage and while holding the foot 22 in contact with the ground agrees with the position/posture in the next but one time's gait supporting leg coordinate system as observed from the next time gait's supporting leg coordinate system.

At the end of the first turning gait, the supporting leg foot 22 is in the air, being off the floor. To determine the trajectory after the supporting leg foot 22 leaves the floor, an expected landing position/posture of the supporting leg foot of the first turning gait is set.

The expected landing position/posture of the supporting leg foot of the first turning gait is set on the basis of a position/posture on a next but two time gait's supporting leg coordinate system observed from the next time gait's supporting leg coordinate system. To be more specific, the expected landing position/posture of the supporting leg foot of the first turning gait is the position/posture on the next but two time gait's

supporting leg coordinate system observed from the next
time gait's supporting leg coordinate system. The next
but two time gait's supporting leg coordinate system is
set such that the relative position/posture relationship
5 between the next but one time gait's supporting leg
coordinate system and the next but two time gait's
supporting leg coordinate system agrees with the relative
position/posture relationship between the current time
gait's supporting leg coordinate system and the next time
10 gait's supporting leg coordinate system.

The supporting leg foot position/posture at the end
of the first turning gait is determined by generating a
foot position/posture trajectory for reaching the expected
landing position/posture of the supporting leg foot of the
15 first turning gait from the supporting leg foot
position/posture at the start of the first turning gait
(more specifically, the trajectory observed from a next
time gait's supporting leg coordinate system) by using the
finite-duration setting filter until the end of the first
20 turning gait, as in the case where the supporting leg foot
position/posture at the start of the first turning gait is
determined.

The free leg foot position/posture at the start of
the second turning gait is regarded as the supporting leg
25 foot position/posture at the end of the first turning gait
observed from the next but one time gait's supporting leg
coordinate system. The supporting leg foot

position/posture at the start of the second turning gait is regarded as the free leg foot position/posture at the end of the first turning gait observed from the next but one time gait's supporting leg coordinate system.

5 The free leg foot position/posture at the end of the second turning gait is regarded as the free leg foot position/posture at the end of the current time gait observed from the current time's gait supporting leg coordinate system. The supporting leg foot
10 position/posture at the end of the second turning gait is regarded as the supporting leg foot position/posture at the end of the current time gait observed from the current time's gait supporting leg coordinate system.

 The gait cycles of the first turning gait and the
15 second turning gait are set to be identical to a next time gait cycle. These gait cycles of the first turning gait and the second turning gait do not have to be the same with each other; however, both cycles are preferably determined on the basis of at least a next time gait cycle.
20 Motion parameters (including a time parameter, such as double stance period duration) of the current time gait, the first turning gait, and the second turning gait other than the above described parameters are determined, as necessary, to satisfy gait conditions (such as an actuator
25 velocity falling within a permissible range, a movable angle being not exceeded, and no interference with a floor) on the basis of the parameters determined above.

Next, the processing proceeds to S102 and determines a reference body posture trajectory parameter that defines the reference body posture trajectory to be followed by a desired body posture. The reference body posture does not have to be constant as long as it is set to ensure connection at the start (the start of the first turning gait) and the end (the end of the second turning gait) of a normal gait (to ensure that the posture angle of the reference body posture and the angular velocity thereof at the start of a normal gait agrees with those at the end of the normal gait). In the first reference example, however, for the purpose of easy understanding, a posture related to an inclination angle (an inclination angle relative to the vertical direction) in the reference body posture is set to an upright posture (vertical posture). This means that, in the first reference example, the reference body posture related to an inclination angle of the body 3 is set to the upright posture in all periods of the normal gait. Accordingly, in the first reference example, the angular velocity and angular acceleration of an inclination angle of the reference body posture is zero. A yaw angle trajectory (hereinafter referred to also as a reference yaw angle trajectory) θ_{bz} of the reference body posture may be, for example, a motion at a constant angular velocity (an average turning velocity of a normal gait), or may take a sinusoidal wave shape, as in the example (Fig. 18) of a reference antiphase arm swing

trajectory, which will be discussed hereinafter. However, the yaw angle trajectory is to be set such that a reference yaw angle and its angular velocity are in succession when the normal gait is repeated.

5 In the first reference example, the yaw angle trajectory (hereinafter referred to also as a desired yaw angle trajectory) of a desired body posture is set to agree with a reference yaw angle trajectory.

10 Subsequently, the processing proceeds to S104 to determine reference arm posture trajectory parameters. To be more specific, parameters related to a total center-of-gravity position of both arms 5, 5 (a relative center-of-gravity position with respect to the body 3), a lateral interval between right and left hands (the distal ends of both arms 5, 5), and an antiphase arm swing angle are
15 determined. For turning, for example, to the left as shown in Fig. 17, the reference antiphase arm swing angle may be set as shown in Fig. 18. As illustrated in Fig. 18, a reference antiphase arm swing angle θ_{azref} is set such
20 that, when a normal gait is repeated, an antiphase arm swing angle and an angular velocity will be both continuous at a boundary of gaits (the boundary between the end of a second turning gait and the next first turning gait) and the relative relationship between the
25 supporting leg at the start of the first turning gait and an antiphase arm swing angle agrees with the relative relationship between the supporting leg at the start of

the next first turning gait and an antiphase arm swing angle. In other words, the antiphase arm swing angular velocity at the start of the first turning gait and the antiphase arm swing angular velocity at the end of the second turning gait agree with each other, and the antiphase arm swing angle at the end of the second turning gait is set to a value obtained by adding the antiphase arm swing angle at the start of the first turning gait to the turning angle of the normal gait (the sum of the turning angles of the first turning gait and the second turning gait). In Fig. 18, the reference antiphase arm swing angle θ_{azref} has the sinusoidal waveform; however, it may alternatively be set to a constant angular velocity, or it may take an average value of a supporting leg yaw angle and a free leg yaw angle.

In the first reference example, the total center-of-gravity position of both arms 5, 5 of the desired arm posture (the relative position with respect to the body 3) is set to be maintained constant with respect to the body 3.

Next, the processing proceeds to S106 and sets a floor reaction force vertical component trajectory parameter. In this case, the floor reaction force vertical component trajectory parameter is set such that the floor reaction force vertical component trajectory defined by the parameter is virtually continuous (values do not jump in steps), as shown in Fig. 6, in both the

first turning gait and the second turning gait. In other words, a desired floor reaction force vertical component trajectory of the normal turning gait is set to have the pattern shown in Fig. 19. According to the pattern, for
5 both the first turning gait and the second turning gait, the floor reaction force vertical component exhibits a trapezoidal change in a single stance period, and the floor reaction force vertical component is maintained at zero in a floating period. The time of break points of
10 the pattern and the height of a trapezoid (peak value) are set as the floor reaction force vertical component trajectory parameters.

When setting the floor reaction force vertical component trajectory parameters, an average value
15 throughout a gait period of the floor reaction force vertical component (the period equivalent to the sum of the periods of the first turning gait and the second turning gait, or the period equivalent to one cycle of a normal gait) is made to agree with the self weight of the
20 robot 1. This means that the average value of the floor reaction force vertical component is set so that it provides the same magnitude as that of the gravity acting on the robot 1 but in an opposite direction.

Setting the floor reaction force vertical component
25 trajectory as described above is necessary to satisfy a normal gait condition. The normal gait conditions is such that a beginning state (a beginning state of a first

turning gait) of any state variables (a position, a posture, a velocity or the like of each part of the robot 1) of a gait observed from a supporting leg coordinate system (a coordinate system set on a plane with which the supporting leg foot 22 is in contact) and a terminal state (a terminal state of a second turning gait) of a gait observed from the next supporting leg coordinate system (the supporting leg coordinate system of the next first turning gait) agree with each other (hereinafter, this condition may be referred to as a boundary condition of a normal gait). Therefore, the difference between a total center-of-gravity vertical velocity of the robot 1 at the end of the normal gait and a total center-of-gravity vertical velocity at the start of the normal gait (more specifically, the difference between the total center-of-gravity vertical velocity at the end of a second turning gait and the total center-of-gravity vertical velocity at the start of the first turning gait) must be also zero. The difference is an integrated value of the difference between the floor reaction force vertical component and gravity (first order integrated value); therefore, the floor reaction force vertical component trajectory must be set as described above in order to set the difference to zero.

In the first reference example, the average value of the floor reaction force vertical component in the period of each of the first turning gait and the second turning

gait has been made to agree with the self weight of the robot 1. More specifically, based on, for example, the gait cycle of the first turning gait and the second turning gait, the time of the break points of the trapezoidal portions of the floor reaction force vertical component trajectory in each turning gait has been set, and then the heights of the trapezoidal portions have been determined such that the average value of the floor reaction force vertical component in the period of each of the first turning gait and the second turning gait agrees with the self weight of the robot 1 (the heights of the trapezoids are determined by solving an equation representing the condition under which the average value and the self weight coincide, taking the heights of the trapezoids as unknown numbers).

Thus, the difference between the total center-of-gravity vertical velocity at the end of the first turning gait and the total center-of-gravity vertical velocity at the start of the first turning gait will be zero, and the difference between the total center-of-gravity vertical velocity at the end of the second turning gait and the total center-of-gravity vertical velocity at the start of the second turning gait will be also zero. This, however, is not a must. If, for instance, a vertical body position becomes excessively high or low at about a boundary of the first turning gait and the second turning gait, leading to a likelihood of an unreasonable posture, then the heights

or the like of trapezoids of the floor reaction force vertical component trajectory of each turning gait may be corrected in the state in which the average value and the self weight agree in each turning gait.

5 Next, the processing proceeds to S108 to set a permissible range of a floor reaction force horizontal component $[F_{xmin}, F_{xmax}]$ (more specifically, a parameter defining it), as shown in Fig. 20, on the basis of the floor reaction force vertical component trajectory set as
10 shown in Fig. 19, as described above. The polygonal line on the negative side in Fig. 20 indicates the permissible lower limit value F_{xmin} of the floor reaction force horizontal component, while the polygonal line on the positive side indicates the permissible upper limit value
15 F_{xmax} of the floor reaction force horizontal component. A supplemental description will be given of a method for setting them. The following will explain a case where a floor surface is horizontal.

20 The floor reaction force horizontal component is generated from friction between a floor and a foot 22. The friction cannot be generated limitlessly; it has a limit. Hence, the floor reaction force horizontal component of a desired gait has to be always within a friction limit in order to prevent the robot 1 from
25 slipping when the actual robot 1 moves according to a generated desired gait. To meet this condition, a permissible range of the floor reaction force horizontal

component will be set, and a desired gait will be generated such that the floor reaction force horizontal component of the desired gait falls within the permissible range, as it will be discussed hereinafter.

5 When the coefficient of friction between the floor
and the foot 22 is denoted by μ , F_{xmin} must be always set
to be not less than $-\mu * \text{floor reaction force vertical}$
component, and F_{xmax} must be set to be not more than $\mu *$
floor reaction force vertical component. A simplest
10 setting method is to set according to the following
expression, in which k_a is a positive constant that is
smaller than 1.

$$F_{xmin} = -k_a * \mu * \text{Floor reaction force vertical component}$$

$$F_{x\max} = k_a * \mu * \text{Floor reaction force vertical component}$$

15 ... Equation 12

The permissible range of the floor reaction force horizontal component shown in Fig. 20 is an example set according to Equation 12. The values and time at the break points of the trapezoidal waveforms or the like in Fig. 20 may be set as the parameters for defining the permissible range of the floor reaction force horizontal component. Alternatively, however, if the permissible range of the floor reaction force horizontal component is determined according to Equation 12, then the value of $(ka \cdot \mu)$ in Equation 12 may be simply set as a parameter.

As long as the above condition (the condition in that the floor reaction force horizontal component of a desired

gait always falls within a frictional limit) is satisfied, a different setting method may be used to set the permissible range of the floor reaction force horizontal component.

5 The gait generating device 100 then proceeds to S109 and sets the permissible range of a floor reaction force moment vertical component [M_{zmin} , M_{zmax}] (more specifically, a parameter defining it), as shown in Fig. 21, on the basis of the floor reaction force vertical component trajectory or the like set as shown in Fig. 19,
10 as described above. The polygonal line on the negative side in Fig. 21 indicates the permissible lower limit value M_{zmin} of the floor reaction force moment vertical component, while the polygonal line on the positive side
15 indicates the permissible upper limit value M_{zmax} of the floor reaction force moment vertical component. A supplemental description will be given of a method for setting them. The following will explain a case where a floor surface is horizontal.

20 The floor reaction force moment vertical component is generated from friction between a floor and a foot 22. The friction cannot be generated limitlessly; it has a limit. Hence, the floor reaction force moment vertical component of a desired gait has to be always within a
25 friction limit in order to prevent the robot 1 from slipping when the actual robot 1 moves according to a generated desired gait. To meet this condition, a

permissible range of the floor reaction force moment
vertical component will be set, and a desired gait will be
generated such that the floor reaction force moment
vertical component of the desired gait falls within the
5 permissible range, as it will be discussed hereinafter.

If the coefficient of friction between the floor and
the foot 22 is denoted by μ , and an effective radius of
the surface of contact between the floor and the foot 22
to generate a moment vertical component (or a square root
10 of a sectional secondary moment about a desired ZMP of the
surface of contact between the floor and the foot 22) is
denote by r , then M_{zmin} must be always set to be not less
than $-\mu * r * \text{floor reaction force vertical component}$, and
 M_{zmax} must be set to be not more than $\mu * r * \text{floor}$
15 $\text{reaction force vertical component}$. A simplest setting
method is to set according to the following expression, in
which k_a is a positive constant that is smaller than 1.
 $M_{zxmin} = -k_a * \mu * r * \text{Floor reaction force vertical}$
 component
20 $M_{zmax} = k_a * \mu * r * \text{Floor reaction force vertical}$
 component

... Equation 1012

The permissible range of the floor reaction force
moment vertical component shown in Fig. 21 is an example
25 set according to Equation 1012. The values and time at
the break points of the trapezoidal waveforms or the like
in Fig. 21 may be set as the parameters for defining the

permissible range of the floor reaction force moment vertical component. Alternatively, however, if the permissible range of the floor reaction force moment vertical component is determined according to Equation 1012, then the value of $(k_a \mu)$ in Equation 1012 may be simply set as a parameter. r is desirably calculated from a desired ZMP and a contact surface at each instant; alternately, however, r may be a constant.

As long as the above condition (the condition in that the floor reaction force moment vertical component of a desired gait always falls within a frictional limit) is satisfied, a different setting method may be used to set the permissible range of the floor reaction force moment vertical component.

Further alternatively, a permissible range may be set by combining a floor reaction force horizontal component and a floor reaction force vertical component moment rather than independently setting the permissible range of a floor reaction force horizontal component and the permissible range of a floor reaction force moment vertical component. This is because the permissible range of a floor reaction force moment vertical component becomes narrower as a floor reaction force horizontal component increases, while the permissible range of the floor reaction force horizontal component becomes narrower as the floor reaction force moment vertical component increases.

Next, the processing proceeds to S110 and sets ZMP trajectory parameters defining the ZMP trajectory of the normal gait that combines the first turning gait and the second turning gait. In this case, a desired ZMP trajectory is set so as to exhibit a high stability margin and no sudden changes, as described above.

To be more specific, according to the running gait shown in Fig. 5, a few moments after the heel of the supporting leg foot 22 lands, substantially the entire surface of the sole of the supporting leg foot 22 comes in contact with the ground, and then, following a few moments, only the tiptoe of the supporting leg foot 22 comes in contact with the ground. Thereafter, the robot 1 kicks the ground with the tiptoe of the supporting leg foot 22 to jump into the air. Lastly, the robot 1 lands at the heel of the free leg foot 22. The desired ZMP has to be in a ground contact surface. In the first reference example, therefore, the position of the desired ZMP in the X-axis direction for the first turning gait and the second turning gait of the normal gait is set so that it takes the heel of the supporting leg foot 22 as its initial position and stays at this position until substantially the entire sole of the foot 22 comes in contact with the ground, as illustrated in the upper diagram of Fig. 7 described above. Subsequently, the desired ZMP is set to move to the center of the supporting leg foot 22, and then move to the tiptoe by the time the tiptoe of the foot 22

comes in contact with the ground and remain at the tiptoe of the supporting leg foot 22 until the foot 22 leaves the floor. Thereafter, the desired ZMP is set such that the desired ZMP continuously moves from the tiptoe of the supporting leg foot 22 to the landing position of the heel of the free leg foot 22 by the time the next free leg foot 22 lands, as previously described. Thus, the desired ZMP trajectory (the trajectory in the X-axis direction) of the normal gait composed of the first turning gait and the second turning gait will be as illustrated in Fig. 22. The time and positions of the break points of the desired ZMP trajectory are set as the ZMP trajectory parameters. In this case, the time of the break points is set on the basis of gait cycles of the first turning gait and the second turning gait determined based on the required parameters. The positions of the break points are set on the basis of the positions/postures on the next time gait's supporting leg coordinate system and the next but one time gait's supporting leg coordinate system or on the basis of the required values of the expected free leg foot landing positions/postures of the first step and the second step of the required parameters that define these coordinate systems. The position of the ZMP trajectory in the Y-axis direction is set in the same manner as that illustrated in the lower diagram of Fig. 7. More specifically, the trajectory of the positions of the desired ZMP in the Y-axis direction in the first turning

gait is set according to the same pattern as that shown in the lower diagram of Fig. 7. The trajectory of the positions of the desired ZMP in the Y-axis direction in the second turning gait is set to have the same shape as that for the first turning gait and continues from the end of the trajectory.

Subsequently, the processing proceeds to S112 and redefines the start time, the end time, and duration of one step (one cycle) of the normal gait as follows.

A normal gait must be a gait in which state variables continuously connect at the start and the end thereof. To easily determine such a gait, in the first reference example, the start, the end, and the duration of one step of a normal gait are determined as illustrated in Fig. 19 for convenience sake, which is different from the definition of a gait in the narrow sense described above. Specifically, in the latter half of a single stance period of the first turning gait, the time at which the floor reaction force vertical component has reduced to a certain degree is set as start time T_s of the normal gait. The start time T_s is preferably set to the time of the moment at which the state wherein substantially the entire surface of the sole of the supporting leg foot 22 is in contact with the ground is switched to tiptoe contact with the ground or at the time immediately preceding it, as shown in Fig. 7 (the time when the period of the entire sole surface in contact with the ground ends or the time

immediately preceding it, as shown in Fig. 7). A description will now be given of the relationship between the desired ZMP and time T_s shown in Fig. 22 (or Fig. 7) set in S110. After substantially the entire surface of the sole of the supporting leg foot 22 comes in contact with the ground in the first turning gait, the desired ZMP moves to the center of the supporting leg foot 22. The instant the movement to the tiptoe is completed by the tiptoe contact with the ground is established is preferably time T_s . The start time T_s is set on the basis of, for example, the desired ZMP trajectory parameters previously set. The reason for setting the start time T_s as described above will be discussed hereinafter.

As shown in Fig. 19, a cycle T_{cyc} of the normal gait is a sum of the gait cycles of the first turning gait and the second turning gait. The end time of the normal gait is denoted by T_e . T_e is set to the time obtained by adding T_{cyc} to T_s .

The definition of the start, the end, or the like of a gait will be returned to the definition of the gait in the aforesaid narrow sense again from the moment the normal gait is determined (the moment the program leaves the loop of S204 shown in Fig. 23). In the following explanation, the start time (the time at which the supporting leg foot 22 lands first) according to the definition of a gait based on the aforesaid narrow sense will be set to 0, and the above start time T_s used until

the normal gait is determined will be distinguished from the original start time 0 by using the reference mark T_s (abbreviated to " T_s " in some cases).

5 Lastly, the processing proceeds to S114 and sets a body posture angle and antiphase arm swing angle restoring period $[T_m, T_{s2}]$ and $[T_{m2}, T_e]$ of the normal gait. Supplementally, when the normal gait is repeated, the body posture angle and the antiphase arm swing angle should be continuous in a boundary of gaits. For this purpose, the
10 beginning body posture angular velocity and the ending body posture angular velocity of the normal gait must agree with each other, and the beginning antiphase arm swing angular velocity and the ending antiphase arm swing angular velocity must agree with each other. The
15 aforesaid period is the period for adjusting a body posture angle trajectory and an antiphase arm swing angle trajectory to implement the agreement.

 To be more specific, the gait goes through the floating period of the first turning gait from the start
20 time T_s and reaches the second turning gait. The time at which the floor reaction force vertical component has increased to a predetermined magnitude is set as time T_m . Further, in the latter half of a single stance period of the second turning gait, the time at which the floor
25 reaction force vertical component has reduced to a certain degree is set as time T_{s2} . Further, the gait goes through the floating period of the second turning gait and reaches

the first turning gait. The time at which the floor reaction force vertical component has increased to a predetermined magnitude is set as time T_{m2} .

Fig. 19 shows these times. The time T_m is preferably set to be the moment substantially the entire surface of the sole of the supporting leg foot 22 comes in contact with the ground or immediately after that. The same applies to time T_{m2} . The time T_{s2} is preferably set to the time of the moment at which the state wherein substantially the entire surface of the sole of the supporting leg foot 22 is in contact with the ground is switched to tiptoe contact with the ground or at the time immediately preceding it, as in the case of the start time T_s .

A description will now be given of the relationship between the desired ZMP of Fig. 22 and these times T_m , T_{s2} and T_{m2} set in the afore-mentioned S110 of Fig. 15. In the second turning gait, the desired ZMP takes the heel of the supporting leg foot 22 as the beginning position and remains at this position until substantially the entire surface of the sole of the supporting leg foot 22 comes in contact with the ground, and then the desired ZMP begins to move to the center of the supporting leg foot 22. It is desired to set this moment the desired ZMP begins to move the center as time T_m . Thereafter, the instant the movement of the desired ZMP to the tiptoe is completed by the time only the tiptoe of the supporting leg foot 22

comes in contact with the ground is preferably set as time
Ts2. Furthermore, in the next first turning gait, the
desired ZMP takes the heel of the supporting leg foot 22
as the beginning position and remains at this position
5 until substantially the entire surface of the sole of the
supporting leg foot 22 comes in contact with the ground,
and then the desired ZMP begins to move to the center of
the supporting leg foot 22. It is desired to set this
moment the desired ZMP begins to move to the center as
10 time Tm2.

The reason for setting as described above will be
discussed hereinafter. The period for restoring
(adjusting) the body posture angle and the period for
restoring (adjusting) the antiphase arm swing angle may be
15 separately set.

After the processing from S010 to S022 shown in Fig.
13 is carried out, the processing proceeds to S024 and
calculates an initial state of the normal gait. The
initial state calculated here includes an initial
20 horizontal body position/velocity (an initial body
position and initial body velocity in the horizontal
direction), an initial vertical body position/velocity (an
initial body position and an initial body velocity in the
vertical direction), an initial divergent component, an
25 initial body posture angle, and an angular velocity, and
an initial antiphase arm swing angle and an angular
velocity of the normal gait. The initial state is

exploratorily calculated according to the flowchart of Fig. 23.

In the flowchart of Fig. 23, first, in S200, an initial state (a state at the start time T_s) of a desired foot position/posture, a desired arm posture, and a
5 desired body posture angle (an inclination angle and a yaw angle) are determined on the basis of the gait parameters of the normal gait (the parameters set in S022 of Fig. 13 described above). The state here represents positions and
10 posture angles and their changing rates (time derivative).

In this case, the initial state of a desired foot position/posture of a supporting leg is determined by generating, using a finite-duration setting filter, a foot position/posture trajectory (a trajectory observed from a
15 next time gait's supporting leg coordinate system) from the supporting leg foot position/posture at the start of the first turning gait of the foot trajectory parameter determined in S100 of Fig. 15 to the free leg foot position/posture at the end of the second turning gait
20 until time T_s is reached. The initial state of a desired foot position/posture of the free leg is determined by generating, using a finite-duration setting filter, a foot position/posture trajectory from the supporting leg foot position/posture at the start of the current time gait
25 observed from a next time gait's supporting leg coordinate system to the free leg foot position/posture at the end of the first turning gait until time T_s is reached. The

initial state of a desired arm posture is determined to be a reference arm posture at time T_s that is determined on the basis of the reference arm posture trajectory

parameters determined in S104 of Fig. 15. To be more specific, a total center-of-gravity position of both arms 5, 5 (a relative position with respect to the body 3) of a desired arm posture, a lateral interval between right and left hands (the distal ends of both arms 5, 5), and an antiphase arm swing angle and an angular velocity are determined. However, the antiphase arm swing angle and the angular velocity are corrected so that they are continuous in a boundary of gaits when a normal gait is repeated, as it will be discussed hereinafter; therefore, they have been just temporarily determined.

For an initial state of a desired body posture angle, a reference body posture (an inclination angle and a yaw angle) and an angular velocity thereof at time T_s determined by the reference body posture trajectory parameter determined in S102 of Fig. 15 are determined as an initial state of the desired body posture angle. In the first reference example, the reference body posture related to the inclination angle of the body 3 is a vertical posture, so that the initial state (the inclination angle and the angular velocity thereof) of the inclination angle in the desired body posture is zero.

Further, in the first reference example, a desired foot position/posture trajectory, a floor reaction force

vertical component trajectory, and a desired ZMP trajectory of a normal gait are determined independently from each other on the basis of a foot trajectory parameter, a floor reaction force vertical component trajectory parameter, and a ZMP trajectory parameter, respectively, which have been determined in the flowchart of Fig. 15. For example, a desired foot position/posture at each instant of a normal gait is determined on the basis of a foot trajectory parameter without depending on an instantaneous value of a floor reaction force vertical component.

Subsequently, in S202, (X_s, V_{xs}) (X_s : horizontal position; V_{xs} : horizontal velocity), which is a candidate of an initial horizontal body position velocity (that is, a candidate of the horizontal body position velocity at the start time T_s), is provisionally determined. The candidate (X_s, V_{xs}) to be provisionally determined may be arbitrary. For example, the horizontal body position velocity in the initial state of the normal gait determined when the last time's gait was generated may be used as a provisionally determined candidate (X_s, V_{xs}) .

To simplify the explanation, a case where the initial state of a normal gait in the X-direction (longitudinal direction) on a sagittal plane is searched for will be taken as an example. However, for the initial state of a normal gait (the initial state that meets the aforesaid boundary condition of a normal gait), it is actually

required to search for the position and the velocity in the X direction (longitudinal direction) and the Y direction (lateral direction) separately or simultaneously.

Supplementally, there is no concept related to a yaw rotation or a moment vertical component or others about a vertical axis on the sagittal plane. For this reason, at least the yaw rotation and a moment vertical component are calculated in a three-dimensional space.

As an exploratory determining technique, a method in which a pseudo-Jacobian (sensitivity matrix) is determined and then a next candidate is determined by the steepest descent method or the like, or the simplex method or the like may be used. In the present embodiment, the steepest descent method will be used.

Next, the processing proceeds to S206 via S204 and determines the initial (time T_s) vertical body position velocity (Z_s , V_zs) (Z_s : vertical position; V_zs : vertical velocity) so that the vertical body position velocity is continuous and angles of joints, such as knees, will not be excessively large or small when the normal gait is repeated. More details regarding this have been described in, for example, PCT/JP02/13592 previously applied by the present applicant, and will be therefore omitted here.

After the processing of S206, the processing proceeds to S208 to provisionally generate a normal turning gait (the normal turning gait provisionally generated may be hereinafter referred to as the provisional gait). To be

more specific, based on the gait parameters of the normal gait determined in S022 of Fig. 13 described above, a desired ZMP, a desired floor reaction force vertical component, a desired foot position/posture, a reference body posture, a desired arm posture, a floor reaction force horizontal component permissible range, and a floor reaction force moment vertical component permissible range at each instant from the start time T_s to the end time T_e are sequentially determined. Then, gaits from time T_s to the end time T_e are generated by sequentially determining the body position/posture, taking the horizontal body position velocity (X_s , V_{xs}) and the vertical body position velocity (Z_s , V_{zs}) mentioned above as the initial (time T_s) state of the body 3, and by using the aforesaid dynamic model (the model in Fig. 12) so as to satisfy the dynamic balance condition related to the determined desired ZMP and the desired floor reaction force vertical component and the condition of the floor reaction force horizontal component permissible range. At this time, the gaits are generated so that the body posture agrees with the reference body posture as much as possible.

Moreover, an antiphase arm swing motion is determined such that the condition related to the floor reaction force moment vertical component, i.e., the floor reaction force moment vertical component permissible range, is satisfied.

Incidentally, the gait generation of the normal gait

is performed merely inside the gait generating device 100,
and the generated gaits are not output to a composite-
compliance operation determiner 104, which will be
discussed later, as desired values for driving the actual
5 robot 1.

The following will explain in detail the processing
for generating a normal gait by sequential calculation,
which is the processing in S208.

Fig. 24 is a subroutine flowchart illustrating the
10 processing.

The explanation will now be given. In S300, various
elements are initialized. Specifically, the start time T_s
is substituted into time k for generating a provisional
gait. Furthermore, a currently determined (X_s, V_xs)
15 (determined in S202, or S216 or S218 of Fig. 23 to be
discussed hereinafter) is substituted into the horizontal
body position velocity, and the latest (Z_s, V_zs)
determined in the aforesaid S206 is substituted into the
vertical body position velocity. In addition, an initial
20 value of a reference body posture angle (angle at the
start time T_s) is substituted into the body posture angle,
and an initial value of a reference body posture angular
velocity (an angular velocity at the start time T_s) is
substituted into the body posture angular velocity.

25 A reference initial antiphase arm swing angle (angle
at the start time T_s) is substituted into the antiphase
arm swing angle, and a reference initial antiphase arm

swing angular velocity (angular velocity at the start time T_s) is substituted into the antiphase arm swing angular velocity.

Subsequently, the processing proceeds to S304 via
5 S302 and determines whether time k for generating a
provisional gait is before gait end time (whether $k \leq T_s + T_{cyc}$). If the determination result is YES, then the
processing proceeds to a gait instantaneous value
determining subroutine of S306 to determine a gait
10 instantaneous value. Subsequently, the processing of the
gait generating device 100 proceeds to S308 to increment
time k for generating a provisional gait by Δk , and then
returns to S304.

Here, Δk is an interval of the generation of
15 provisional gaits and normally set to agree with a control
cycle Δt . If the dynamic accuracy of provisional gaits is
not demanding, then Δk may be set to be longer than Δt in
order to reduce the volume of calculation.

If the determination result of S304 is NO, then the
20 processing proceeds to S310. The processing described
above generates a normal gait (provisional gait) from its
start to end before proceeding to S310.

A gait instantaneous value determining subroutine of
S306 will now be explained in detail with reference to Fig.
25 25.

First, in S400 of Fig. 25, based on a normal gait
parameter (the floor reaction force vertical component

trajectory parameter), a value (current time value) of the
desired floor reaction force vertical component shown in
Fig. 19 at time k is determined. Further, in S402, a
value (current time value) of the desired ZMP trajectory
shown in Fig. 22 at time k is determined on the basis of a
normal gait parameter (the ZMP trajectory parameter).

Then, the processing proceeds to S404 and determines
the values (current time values) of desired
positions/postures of both feet (desired foot
positions/postures of both supporting leg and free leg),
the reference body posture, and the reference arm posture
at time k on the basis of the normal gait parameters (the
foot trajectory parameter, the reference body posture
trajectory parameter, and the arm posture trajectory
parameter). To be more specific about the reference arm
posture, the values (current time values) of the total
center-of-gravity position of both arms 5, 5 (the relative
position with respect to the body 3), the lateral interval
between right and left hands (the distal ends of both arms
5, 5), and the antiphase arm swing angle are determined.

The current time value (the value at time k) of the
desired foot position/posture is determined in the same
manner as in the case where the foot position/posture at
the start time T_s was determined in S200 of Fig. 23.

Then, the processing proceeds to S406 and calculates
a value (current time value) of the total center-of-
gravity vertical position velocity at time k that

satisfies the desired floor reaction force vertical component (balances the sum of the inertial force in the vertical direction and gravity of the robot 1 with the desired floor reaction force vertical component). To be more specific, the total center-of-gravity vertical position velocity is calculated on the basis of, for example, the above Equation 01 and Equation 04 related to the dynamic model shown in Fig. 12. In other words, Equation 01 and Equation 04 provides a relational expression (a dynamic equation related to the vertical direction of the total center of gravity of the robot 1) indicating that the result obtained by multiplying the sum of the total center-of-gravity vertical acceleration and the gravity acceleration from a motion of the robot 1 by the total mass of the robot 1 is equal to a floor reaction force vertical component. Thus, the total center-of-gravity vertical acceleration is determined from the relational expression and the desired floor reaction force vertical component.

The relational expression itself generally holds without depending on a model of the robot 1. The total center-of-gravity vertical velocity is calculated by integrating the determined total center-of-gravity vertical acceleration, and further, the total center-of-gravity vertical velocity is integrated to calculate the total center-of-gravity vertical position. More generally, these calculations are carried out using the dynamic

leg mass point $2m$ and the current time value of the total center-of-gravity vertical position determined in S407 are applied to Equation 04 so as to determine the vertical position of the body mass point $3m$. Furthermore, the
5 vertical body position is determined from the determined vertical position of the body mass point $3m$ and the current time value of the desired body posture angle (the reference body posture angle set in S404 or the last time's (time $k-\Delta k$) desired body posture angle determined
10 in S414 to be discussed hereinafter).

The processing then proceeds to S410 wherein the values (current time value), at time k , of the floor reaction force horizontal component permissible range [F_{xmin} , F_{xmax}] shown in Fig. 20 are determined on the
15 basis of the gait parameter (the parameter defining the floor reaction force horizontal component permissible range) determined in S108 of Fig. 15 described above.

Subsequently, the processing proceeds to S411 wherein the values (current time value), at time k , of the floor
20 reaction force moment vertical component permissible range [M_{zmin} , M_{zmax}] shown in Fig. 21 are determined on the basis of the gait parameter (the parameter defining the floor reaction force moment vertical component permissible range) determined in S109 of Fig. 15 described above.

25 Then, the processing proceeds to S412 wherein the current time values of the desired body horizontal acceleration and the desired body posture acceleration are

determined such that the dynamic balance condition related to the desired ZMP (the condition in that the horizontal component of a moment generated about the desired ZMP by a resultant force of an inertial force and the gravity of the robot 1 is zero) is satisfied. The body horizontal acceleration and the body posture angular acceleration (more specifically, the body inclination angular acceleration) are determined such that the floor reaction force horizontal component F_x does not exceed $[F_{xmin}, F_{xmax}]$. Further, the current time value of the desired antiphase arm swing angular acceleration is determined such that the floor reaction force moment vertical component M_z does not exceed $[M_{zmin}, M_{zmax}]$.

Of the body posture angle, the yaw angle is determined so as to agree with the yaw angle of the reference body posture angle. Regarding the desired arm posture, components other than the antiphase arm swing angle are determined to agree with the reference arm posture. At this time, the desired body inclination angle and the desired antiphase arm swing angle are determined to follow the reference body inclination angle and the reference antiphase arm swing angle, respectively, as much as possible, while satisfying the aforesaid condition. This will be explained in detail below.

At this point, the instantaneous values (current time values) of the foot position/posture and the vertical body position have been determined as described above.

Regarding the arm posture, the components other than the antiphase arm swing angle have been determined to agree with those of the reference arm posture. Therefore, once the remaining horizontal body position, body posture angle and antiphase arm swing angle are determined, then the desired motion of the robot 1 will be uniquely determined. Hence, all floor reaction forces will be also uniquely determined. In the first reference example, the desired floor reaction force vertical component and the desired ZMP of a normal gait are defined by the floor reaction force vertical component trajectory parameter and the desired ZMP trajectory parameter, respectively, determined in S022 of Fig. 13 described above.

When generating a gait, if the body inclination mode is primarily used to satisfy a desired ZMP (to set the horizontal component of a floor reaction force moment about a desired ZMP to zero) without using the aforesaid body translational mode, then the body posture angle may become excessively large. To prevent this, therefore, the body translational mode should be used as much as possible. However, the body translational mode involves floor reaction force horizontal component changes, so that slippage may occur if the body translational mode is intensely effected when the floor reaction force horizontal component permissible range is narrow. In this case, depending upon the body inclination mode is an inevitable choice. Especially during a period in which

the floor reaction force horizontal component permissible range is zero, as in the aforesaid running gait, it is impossible to generate a gait for generating a floor reaction force horizontal component. Hence, depending upon the body inclination mode is an inevitable choice.

Meanwhile, an antiphase arm swing motion allows only the floor reaction force moment vertical component to be changed without changing any of the horizontal component of a floor reaction force moment about a desired ZMP and the floor reaction force horizontal component, so that it can be used to prevent the floor reaction force moment vertical component from exceeding the aforesaid floor reaction force moment vertical component permissible range.

Considering the above, in the first reference example, the body horizontal acceleration, the body posture angular acceleration, and the antiphase arm swing acceleration are determined according to the flowchart shown in Fig. 26.

For the convenience of understanding, regarding the determination of the body horizontal acceleration and the

body posture angular acceleration (the angular acceleration of an inclination angle of the body 3), a case where the body horizontal acceleration and the body posture angular acceleration in the X direction (longitudinal direction) are determined on a sagittal plane will be taken as an example. Actually, however, the body horizontal acceleration and the body posture angular acceleration in the Y direction (lateral direction) are

also determined in the same manner as that for the X direction.

First, in S500, the value of the reference body yaw angle at time k is substituted into the desired body yaw angle. Further, the value of a reference arm posture at
5 time k is substituted into the desired arm posture, excluding the antiphase arm swing angle and the angular velocity component of an arm posture.

Then, in S502, it is determined whether the current
10 time (the value of a timer for generating a normal gait) k is in the period of restoring a body posture angle and an antiphase arm swing angle (the period of restoring a body posture angle and an antiphase arm swing angle being the period from time T_m to time T_{s2} and the period from time
15 T_{m2} to T_e in the case of a normal gait). The processing proceeds to S504 if the determination result of S502 is NO, or to S530 if the determination result is YES.

In S504, a body horizontal acceleration α_{tmp} necessary to satisfy the current (time k) desired ZMP is
20 determined, assuming that the robot 1 is made to perform a motion of the body translational mode, the angular acceleration of the body inclination mode being set to zero, from a last time's instantaneous gait state (the gait state at time $k-1$) of the robot 1. The α_{tmp} is
25 determined using, for example, the above Equation 03y related to the dynamic model of Fig. 12 described above. To be more specific, for example, time series values of

desired foot positions/postures determined by the current time k are used to determine the vertical accelerations of the supporting leg mass point $2m$ and the free leg mass point $2m$ at the current time k , and a desired foot position/posture at the current time k (current time) is used to determine the vertical positions of the supporting leg mass point $2m$ and the free leg mass point $2m$. Furthermore, the floor reaction force vertical position at the current time k (current time) is used to determine the vertical position of the body mass point $3m$, and the vertical acceleration of the body mass point $3m$ at the current time k is determined by using time series values of the desired vertical body positions determined by the current time k . Then, these determined values are substituted into the above Equation 03y, and an equation obtained by setting M_y and $d^2\theta_{by}/dt^2$ of the Equation 03y to zero is solved on d^2X_b/dt^2 so as to determine the body mass point horizontal acceleration as the body horizontal acceleration α_{tmp} . A more precise dynamic model may be used to exploratorily determine the body horizontal acceleration α_{tmp} that sets the horizontal component of the floor reaction force moment about the desired ZMP to zero. Further, in the first reference example, the reference body posture related to the inclination angle of the body 3 is the vertical posture and the body posture angular acceleration (the angular acceleration of the inclination angle of the body 3) in the reference body

posture is zero, so that the angular acceleration in the body inclination mode was set to zero to determine the body horizontal acceleration α_{tmp} . If, however, the reference body posture trajectory parameter is set so that the inclination angle of the reference body posture changes and if the reference body posture angular acceleration (the reference angular acceleration of the inclination angle of the body 3) at the current time k determined thereby is not zero, then the angular acceleration in the body inclination mode may be set to the value of that reference body posture angular acceleration, which is not zero, to determine the body horizontal acceleration α_{tmp} by using a dynamic model (for example, $d^2\theta_{by}/dt^2$ of Equation 03y may be set to a reference body posture angular acceleration that is not zero to determine the body horizontal acceleration α_{tmp} in the same manner as described above).

Next, the processing proceeds to S506 wherein a floor reaction force horizontal component F_{xtmp} at time k when the body horizontal acceleration is α_{tmp} is determined using a dynamic model. In the first reference example, F_{xtmp} is determined using Equation 02x of the dynamic model. In other words, F_{xtmp} is determined according to the following Equation 17, where d^2X_{sup}/dt^2 and d^2X_{swg}/dt^2 denote the supporting leg foot mass point horizontal acceleration and the free leg foot mass point horizontal acceleration.

$$\begin{aligned} F_{xtmp} = m_b * \alpha_{tmp} + m_{sup} * d^2X_{sup}/dt^2 \\ + m_{swg} * d^2X_{swg}/dt^2 \quad \dots \text{Equation 17} \end{aligned}$$

5 An example of F_{xtmp} determined as described above is shown in Fig. 27. In Fig. 27, a portion wherein F_{xtmp} exceeds the floor reaction force horizontal component permissible range $[F_{xmin}, F_{xmax}]$ is hatched.

10 Subsequently, the processing proceeds to S508 wherein a body horizontal acceleration α in the body translational mode and a floor reaction force horizontal component F_x generated thereby, and a body angular acceleration β in the body inclination mode are determined as shown below (S508 to S516).

15 Specifically,

 If $F_{xtmp} > F_{xmax}$, then the processing proceeds to S510 wherein F_x is determined according to the following equation.

20 $F_x = F_{xmax} \quad \dots \text{Equation 18}$

 If $F_{xtmp} < F_{xmin}$, then the processing proceeds to S512 wherein F_x is determined according to the following equation.

25

$F_x = F_{xmin} \quad \dots \text{Equation 19}$

In other cases, that is, if F_{xtmp} lies within the floor reaction force horizontal component permissible range $[F_{xmin}, F_{xmax}]$, then the processing proceeds to S514 wherein F_x is determined according to the following equation.

$$F_x = F_{xtmp} \quad \dots \text{Equation 20}$$

In any case, the processing proceeds to S516 wherein the body horizontal acceleration α and the body posture angular acceleration (body inclination angular acceleration) β are determined according to the following equations.

$$\alpha = \alpha_{tmp} + (F_x - F_{xtmp}) / \Delta F_p \quad \dots \text{Equation 21}$$

$$\beta = (\alpha_{tmp} - \alpha) * \Delta M_p / \Delta M_r \quad \dots \text{Equation 22}$$

where ΔF_p , ΔM_p , and ΔM_r are determined according to the above Equations 06, 07, and Equation 09, respectively.

Supplementally, if higher accuracy of the dynamic calculation is required, then, after determining the body angular acceleration β as described above, the body horizontal acceleration α in the body translational mode should be analytically or exploratorily determined by using a more precise dynamic model so that a motion obtained by combining the body translational mode and the body inclination mode of the above determined body angular acceleration β satisfies the desired ZMP. As an

exploratory determining method, a method in which a pseudo-Jacobian (sensitivity matrix) is determined and then a next candidate is determined by the pseudo-Newton method or the like, or the simplex method or the like may be used.

Further, in order to strictly prevent the floor reaction force horizontal component F_x from exceeding the floor reaction force horizontal component permissible range $[F_{xmin}, F_{xmax}]$, a set of the body horizontal acceleration α and the body angular acceleration β may be exploratorily searched for such that $F_x = F_{xmax}$ and the horizontal component of the floor reaction force moment about the desired ZMP is zero in S510 and also $F_x = F_{xmin}$ and the horizontal component of the floor reaction force moment about the desired ZMP is zero in S512.

Fig. 28 shows F_x determined as described above. F_x has been limited (saturated) so that a value of F_{xtmp} does not exceed the floor reaction force horizontal component permissible range $[F_{xmin}, F_{xmax}]$. More specifically, F_{xtmp} is directly used as F_x if F_{xtmp} based on the body horizontal acceleration α_{tmp} only by the body translational mode lies within the permissible range $[F_{xmin}, F_{xmax}]$. If F_{xtmp} based on the body horizontal acceleration α_{tmp} only by the body translational mode exceeds an upper limit of the permissible range $[F_{xmin}, F_{xmax}]$ or reduces below a lower limit thereof, then F_x is forcibly limited to F_{xmax} and F_{xmin} , respectively.

Especially in a floating period of a running gait,
 $F_{x\max}=F_{x\min}=0$ applies all the times, so that $F_x=0$.

Fig. 29 shows the body posture angular acceleration β determined as described above. Thus, an insufficient
5 portion of the floor reaction force moment caused by limiting the acceleration in the body translational mode so as to prevent F_x generated by the body translational mode from exceeding the permissible range $[F_{x\min}, F_{x\max}]$ (more specifically, the moment obtained by subtracting a
10 moment component produced by a limited body horizontal motion and the motions of both legs 2, 2 from an inertial force moment required for reducing the horizontal component of a floor reaction force moment about the desired ZMP to zero) has been compensated for by the body inclination mode. During a floating period of a running
15 gate, the body horizontal acceleration α by the body translational mode is always limited to zero, so that the insufficient portion of the floor reaction force moment is compensated for only by the body posture angular
20 acceleration β by the body inclination mode.

Subsequently, the processing proceeds to S518 to determine a floor reaction force moment vertical component M_{ztmp} when a motion in which, for example, a body
horizontal acceleration in the body translational mode is
25 α , a body angular acceleration (body inclination angular acceleration) in the body inclination mode is β , a body acceleration in the body yaw rotation mode (body yaw

angular acceleration) is a reference yaw angular acceleration $d^2\theta_{bzref}/dt^2$, and an antiphase arm swing angular acceleration β_a is a reference antiphase arm swing angular acceleration $d^2\theta_{azref}/dt^2$, is performed.

5 Hereinafter, $d^2\theta_{bzref}/dt^2$ will be β_{bref} , and $d^2\theta_{azref}/dt^2$ will be β_{aref} .

To be more specific, M_z obtained by substituting Equation 1001 through Equation 1004 into Equation 03z is M_{ztmp} .

10

$d^2X_b/dt^2 = \alpha_x$... Equation 1001

$d^2Y_b/dt^2 = \alpha_y$... Equation 1002

$d^2\theta_{bz}/dt^2 = \beta_{bref}$... Equation 1003

$d^2\theta_{az}/dt^2 = \beta_{aref}$... Equation 1004

15

where α_x denotes an X component of the body horizontal acceleration α ; α_y denotes a Y component of the body horizontal acceleration α . Furthermore, A horizontal body position at time $k-1$ is substituted into X_b and Y_b , and a value of time k is substituted into X_{zmp} , Y_{zmp} , X_{sup} , d^2Y_{sup}/dt^2 , X_{swg} , and d^2Y_{swg}/dt^2 .

20

Fig. 32 shows an example M_{ztmp} determined as described above. In Fig. 32, the portions of M_{ztmp} that exceeds the floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$ are shown by hatching.

25

Next, the processing proceeds to S520 wherein an antiphase arm swing angular acceleration β_a is determined

as shown below (S520 ~ S528).

Specifically,

If $M_{ztmp} > M_{zmax}$, then the processing proceeds to
S522 wherein M_z is determined according to the following
5 equation.

$$M_z = M_{zmax} \quad \dots \text{Equation 1018}$$

If $M_{ztmp} < M_{zmin}$, then the processing proceeds to
10 S524 wherein M_z is determined according to the following
equation.

$$M_z = M_{zmin} \quad \dots \text{Equation 1019}$$

15 In other cases, that is, if M_{ztmp} lies within the
floor reaction force horizontal component permissible
range $[M_{zmin}, M_{zmax}]$, then the processing proceeds to S526
wherein M_z is determined according to the following
equation.

20

$$M_z = M_{ztmp} \quad \dots \text{Equation 1020}$$

In any case, the processing proceeds to S528 wherein
the antiphase arm swing angular acceleration β_a is
25 determined according to the following equation.

$$\beta_a = \beta_{aref} + (M_{ztmp} - M_z) / \Delta M_{az} \quad \dots \text{Equation 1021}$$

where ΔM_z is determined according to Equation 09a.

The following will explain the processing from S518 to S528.

5 M_z determined as described above denotes a floor reaction force moment vertical component from a motion of the entire robot, including an antiphase arm swing.

 In the above processing, the antiphase arm swing angular acceleration β_a has been determined such that the
10 M_z does not exceed the floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$. To be more specific, M_z has been determined to be limited (saturated) so that a value of M_{ztmp} does not exceed the floor reaction force horizontal component permissible
15 range $[M_{zmin}, M_{zmax}]$. More detailedly, M_{ztmp} is directly used as M_z if M_{ztmp} lies within the permissible range $[M_{zmin}, M_{zmax}]$. If M_{ztmp} exceeds an upper limit of the permissible range $[M_{zmin}, M_{zmax}]$ or reduces below a lower limit thereof, then M_z is forcibly limited to M_{zmax} and
20 M_{zmin} , respectively. Especially in a floating period of a running gait, $M_{zmax}=M_{zmin}=0$ applies all the times, so that $M_z=0$.

 A moment vertical component M_{az} to be generated by an antiphase arm swing in order to prevent M_z from exceeding
25 the floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$ is $(M_z - M_{ztmp})$. $M_{az}(= M_z - M_{ztmp})$ is shown in Fig. 34.

The antiphase arm swing angular acceleration β_a can be obtained by adding the result obtained by dividing M_{az} by an equivalent inertial moment ΔM_{az} of an antiphase arm swing to a reference antiphase arm swing angular acceleration β_{aref} (a value obtained by subjecting a reference antiphase arm swing angle to second order differentiation). Specifically, β_a is determined according to the above Equation 1021. The antiphase arm swing angular acceleration β_a is shown in Fig. 35.

As described above, in the processing from S504 to S528, the antiphase arm swing angular acceleration β_a is determined such that the floor reaction force moment vertical component M_z generated by a motion of the entire robot, including an antiphase arm swing, does not exceed the permissible range $[M_{zmin}, M_{zmax}]$ (such that the floor reaction force moment vertical component M_{ztmp} offsets (cancels) the portion of the floor reaction force moment vertical component M_{ztmp} that exceeds the permissible range, the floor reaction force moment vertical component M_{ztmp} being generated when an antiphase arm swing angular acceleration is set to agree with the reference antiphase arm swing angular acceleration β_{aref}).

Supplementally, to strictly prevent the floor reaction force moment vertical component M_z from exceeding the floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$, the antiphase arm swing angular acceleration β_a should be analytically or

exploratorily searched for by using a more precise dynamic model in place of the processing from S504 to S528. As an exploratory determining method, a method in which a pseudo-Jacobian (sensitivity matrix) is determined and then a next candidate is determined by the pseudo-Newton method or the like, or the simplex method or the like may be used.

The above processing is performed if time k is not found during the period of restoring a body posture angle and an antiphase arm swing angle.

If a determination result of S502 is YES, then the following processing will be carried out. First, the processing proceeds to S530 wherein the body horizontal acceleration α required to satisfy the desired ZMP of current time (time k) when the angular acceleration in the body inclination mode is set to zero from the last time's instantaneous gait state (the gait state at time $k-1$) of the robot 1 so as to make the robot 1 perform a motion of the body translational mode is determined, and this is determined as a final body horizontal acceleration.

Next, the processing proceeds to S532 wherein the floor reaction force horizontal component F_x in the aforesaid case is determined.

Next, the processing proceeds to S534 wherein the body posture angular acceleration (the body inclination angular acceleration) β is determined to be zero. The body yaw angular acceleration is determined to be the

reference body yaw angular acceleration β_{bref} (the value obtained by subjecting the reference body yaw angle to second order differentiation).

5 Lastly, the processing proceeds to S536 wherein the reference antiphase arm swing angular acceleration β_{aref} (the value obtained by subjecting the reference antiphase arm swing angle to second order differentiation) is substituted into the antiphase arm swing angular acceleration β_a .

10 The above is the processing carried out if the determination result of S502 is YES. More specifically, in this case, the body posture angular acceleration (the body inclination angular acceleration and the body yaw angular acceleration) is set to agree with the reference
15 body posture angular acceleration, and the antiphase arm swing angular acceleration is set to agree with a reference antiphase arm swing angular acceleration. It is expected that this setting will not cause a floor reaction force generated by a motion to exceed the floor reaction
20 force horizontal component permissible range and the floor reaction force moment vertical component permissible range; therefore, determining as described above will present no problem.

25 After the processing of S528 or S536, the processing proceeds to S414 of Fig. 25 wherein the body horizontal acceleration determined in S412 is sequentially integrated (cumulative addition from time T_s to current time k) so as

to determine a horizontal body velocity, and further, the horizontal body velocity is sequentially integrated (cumulative addition from time T_s to current time k) so as to determine a horizontal body position (current time value). Further, the body posture angular acceleration determined in S412 is sequentially integrated (cumulative addition from time T_s to the current time k) so as to determine a body posture angular velocity, and further, the body posture angular velocity is sequentially integrated (cumulative addition from time T_s to the current time k) so as to determine a body posture angle (current time value).

The processing then proceeds to S416 wherein the antiphase arm swing acceleration β_a is sequentially integrated (cumulative addition from time T_s to the current time k) so as to determine an antiphase arm swing velocity, and further, the determined antiphase arm swing velocity is sequentially integrated (cumulative addition from time T_s to the current time k) so as to determine an antiphase arm swing angle θ_{az} (current time value).

After the normal gait instantaneous value determining subroutine of S306 in Fig. 24 is carried out, the processing proceeds to S308 wherein the value of time k for generating a gait is incremented by a gait generation interval Δk . Then, the processing returns to S304 to repeat the processing of S306 and S308 as long as the condition shown in S304 is satisfied. When the condition

shown in S304 is no longer satisfied, that is, when the generation of provisional gaits up to the end (time $T_e = T_s + T_{cyc}$) is completed, the processing proceeds to S310.

5 For a normal gait, an initial body posture angle and its angular velocity must be determined such that motional states of the robot 1 are not discontinuous at boundaries when the normal gait is repeated.

Hence, in S310, a pattern of a ZMP-converted value (hereinafter referred to as the body posture restoring moment ZMP-converted value and abbreviated to ZMPrec) of a
10 floor reaction force moment for generating a body posture angular acceleration for setting a body posture angular velocity back to an initial value (the value at time T_s) by time T_e is set.

15 This will be explained in detail below.

The following will discuss the procedure for setting a body posture angular velocity back to an initial value (the value at time T_s) by generating a body posture angular acceleration by using the body inclination mode
20 during the period of restoring a body posture angle and an antiphase arm swing angle (the period from time T_m to time T_{s2} and from time T_{m2} to T_e). A body posture angular acceleration pattern for this purpose is denoted by $\beta(k)$. In periods other than the above-mentioned period, $\beta(k)=0$
25 will apply.

In the body inclination mode, generating the body posture angular acceleration $\beta(k)$ will generate a floor

reaction force moment $\beta(k) \cdot \Delta Mr$. As a result, if the floor
reaction force vertical component at that instant is
denoted by $F_z(k)$, then $ZMP(k)$ calculated from a motion
(rather than a desired ZMP) will be shifted by ΔZMP
5 determined according to the following equation.

$$\Delta ZMP(k) = -\beta(k) \cdot \Delta Mr / F_z(k) \quad \dots \text{Equation 23}$$

Therefore, if the pattern of ΔMr and the pattern of
10 $F_z(k)$ have been determined (known), then the body posture
angular velocity can be set back to the initial value (the
value at time T_s), that is, the body posture angular
velocity in an initial (time T_s) state of the reference
body posture trajectory by appropriately setting a pattern
15 of $\Delta ZMP(k)$ to generate a body posture angular acceleration
pattern that satisfies Equation 23.

The aforesaid body posture restoring moment ZMP-
converted value (ZMP_{prec}) means $\Delta ZMP(k)$ that has been
appropriately set as described above. Strictly speaking,
20 ΔMr varies when setting the body posture restoring moment
ZMP-converted value by using the above Equation 23, but it
may be approximately set at a constant value. This is
because the normal gait is merely generated for temporary
use and not used to make an actual robot follow the gait,
25 so that the dynamic accuracy of a normal gait does not
have to be very high.

Fig. 30 illustrates an example of ZMP_{prec} . In Fig. 30,

as a pattern of ZMPrec, trapezoidal patterns are formed for the period from time Tm to time Ts2 and for the period from time Tm2 to time Te. The times of break points of the trapezoidal portions are set to agree with the times of break points of a desired ZMP pattern in the period between time Tm and time Ts2 and the period from Tm2 to Te (refer to Fig. 22). This is because correction of the desired ZMP pattern of a current time gait will be easier, as it will be discussed hereinafter.

Substituting ZMPrec(k) into $\Delta ZMP(k)$ of Equation 23 provides the following equation.

$$\beta(k) = -ZMPrec(k) * Fz(k) / \Delta Mr \quad \dots \text{Equation 24}$$

Therefore, $\beta(k)$ determined in this Equation 24 will be as indicated by the solid lines in Fig. 31. The dashed lines in Fig. 31 indicate the body posture angular acceleration during the period from time Ts to time Tm and the period from time Tm2 to Te (indicated by the solid lines in Fig. 29). (Hereinafter, (k) may be omitted if a value is obviously the value at time k.)

The initial (time Ts) body posture angle is set to agree with the initial (time Ts) reference body posture angle.

Further, the initial body posture angular velocity is determined to satisfy Equations 37a and 37b.

Terminal body posture angle - Initial body posture angle
= Second order integration of a body posture angular
acceleration that has been determined to satisfy a floor
reaction force horizontal component permissible range
5 + Second order integration of a body posture angular
acceleration generated by ZMPrec
+ Initial body posture angular velocity * Cycle of
normal gait

..... Equation 37a

10

Terminal body posture angular velocity - Initial body
posture angular velocity
= First order integration of a body posture angular
acceleration that has been determined to satisfy a floor
15 reaction force horizontal component permissible range
+ First order integration of a body posture angular
acceleration generated by ZMPrec

..... Equation 37b

20

The integration period of the first term of the right
side of each of Equations 37a and 37b is the period
combining the period from time T_s to T_m and the period
from T_{s2} to T_{m2} , while the integration period of the
second term of the right side is the period combining the
25 period from time T_m to T_{s2} and the period from T_{m2} to T_e .

To explain more specifically, in a normal gait, an
initial state posture angle and an angular velocity

observed from a supporting leg coordinate system of a first turning gait (a next time's gait supporting leg coordinate system) must agree with a terminal body posture angle and angular velocity, respectively, observed from a supporting leg coordinate system of the next first turning gait (the next but two time gait's supporting leg coordinate system). Therefore, in the first reference example, the initial (time T_s) body posture angle is determined to be the value of the initial (time T_s) reference body posture angle, and this value and the value obtained by subjecting this value to coordinate conversion into a value observed from the next time gait's supporting leg coordinate system by a matrix (matrix of rotational coordinate conversion) based on a total turning angle (turning angle about a vertical axis) of the robot 1 in a normal gait are substituted into the initial body posture angle and the terminal body posture angle, respectively, in the left side of Equation 37a. The body posture angular acceleration determined in S518 of Fig. 26 described above is used as the body posture angular acceleration related to the integration of the first term of the right side of Equations 37a and 37b.

Then, the initial body posture angular velocities of Equations 37a and 37b and the heights of the trapezoids of ZMPrec (the trapezoidal patterns shown in Fig. 30) related to the integration of the second terms of the right sides of Equations 37a and 37b are taken as unknown numbers

(However, the times of the break points of the trapezoidal patterns of ZMPrec are determined beforehand. Further, a trapezoidal height acycl of ZMPrec of a first turning gait and a trapezoidal height acyc2 of ZMPrec of a second
5 turning gait are set to have the same value.) An initial body posture angular velocity determined by solving the simultaneous equation of Equations 37a and 37b including the unknown numbers is decided as a new initial body posture angular velocity. In this case, the terminal body
10 posture angular velocity in Equation 37b is obtained by coordinate-converting the initial body posture angular velocity, which is an unknown number, into a value observed from a next time's supporting leg coordinate system by a matrix based on the above total turning angle
15 of a normal gait.

Subsequently, the processing proceeds to S312 wherein an amount of influence exerted by a body inclination restoring moment ZMP-converted value (ZMPrec) pattern on a horizontal body position and a velocity is determined on
20 the basis thereof, and the determined amount is added to the horizontal body position and velocity at an end.

This processing will be explained. The details have been explained in PCT/JP02/13592 by the present applicant, so that only a brief explanation will be given here.

25 During the period from time T_s to T_m and the period from time T_{s2} to T_e , if the body posture angular acceleration β is changed to generate the body inclination

restoring moment ZMP-converted value (ZMPrec) pattern, as described above, then the body posture angular acceleration β is determined according to the following equation.

5

$$\beta = -\text{ZMPrec} * F_z / \Delta M_r \quad \dots \text{Equation 1025}$$

The body horizontal acceleration that satisfies the desired ZMP when no body inclination restoring moment is generated is α_{tmp} as determined in S532. When the body posture angular acceleration β is changed as described above, the body horizontal acceleration α required to satisfy the desired ZMP is determined according to the following equation.

15

$$\alpha = \alpha_{tmp} - (\Delta M_r / \Delta M_p) * \beta \quad \dots \text{Equation 1026}$$

From Equations 1025 and 1026,

20

$$\alpha = \alpha_{tmp} + \text{ZMPrec} * F_z / \Delta M_p \quad \dots \text{Equation 1027}$$

In other words, the acceleration is increased by an equivalent to the second term of the right side of Equation 1027 by the body inclination restoring moment ZMP-converted value (ZMPrec).

25

Using the linearity of the equations, the body horizontal velocity at an end obtained when the body

posture angular acceleration β is changed to generate the body inclination restoring moment ZMP-converted value (ZMPrec) pattern as described above will be determined by adding the first order integration of $(ZMPrec * Fz / \Delta Mp)$ from time T_s to T_e to the body horizontal velocity at an end obtained when the body inclination restoring moment ZMP-converted value (ZMPrec) pattern is not generated, i.e., the end value of the body horizontal velocity determined in S414. Further, the horizontal body position at an end obtained when the body posture angular acceleration β is changed to generate the body inclination restoring moment ZMP-converted value (ZMPrec) pattern as described above will be determined by adding the second order integration of $(ZMPrec * Fz / \Delta Mp)$ from time T_s to T_e to the horizontal body position at an end obtained when the body inclination restoring moment ZMP-converted value (ZMPrec) pattern is not generated, i.e., the end value of the horizontal body position determined in S414.

After completing the processing of S312, the processing proceeds to S314 wherein an antiphase arm swing restoring angular acceleration (β_{arec}) pattern is determined such that the antiphase arm swing angular velocities at a start and an end agree.

To be more specific, the antiphase arm swing restoring angular acceleration patterns are set to be trapezoidal, as shown in Fig. 36, and a trapezoidal height $azcyc2$ in the period from time T_m to T_{s2} and a trapezoidal

height $azcyc1$ in the period from time $Tm2$ to Te are set to be the same. The trapezoidal heights $azcyc1$ and $azcyc2$ are determined such that the sum of the integrated value of β_{arec} from time Ts to Te and the integrated value of the above determined antiphase arm swing acceleration β_a for preventing the floor reaction force moment vertical component M_z from exceeding a permissible range becomes zero. The trapezoidal heights in the two periods do not have to be the same.

Supplementally, a floor reaction force moment vertical component (M_{zrec}) generated by the antiphase arm swing restoring angular acceleration pattern determined as described above is as shown in Fig. 37. Accordingly, as shown in Fig. 38, the floor reaction force moment vertical component M_z generated by a motion of the robot, including an antiphase arm swing, will be eventually the sum of M_{ztmp} of Fig. 32, M_z of Fig. 34, and M_{zrec} of Fig. 37, i.e., the sum of M_z of Fig. 33 and M_{zrec} of Fig. 37. In the period from time Tm to $Ts2$ and the period from time $Tm2$ to Te , trapezoidal restoring moments are added. These periods are set so as to provide a sufficiently wide permissible range; therefore, the floor reaction force moment vertical components generated by motions of the robot, including antiphase arm swings, do not exceed the permissible range.

The processing then proceeds to S316 wherein an initial (time Ts) antiphase arm swing angle and an angular

velocity of a normal gait are determined.

To be more specific, the initial antiphase arm swing angular velocity is determined according to the following equation.

5

Initial antiphase arm swing angular velocity

$$\begin{aligned} &= \text{Reference initial antiphase arm swing angular velocity} \\ &\quad - (\text{Antiphase arm swing angle when } \beta_{\text{arec}} \text{ is } 0 \\ &\quad + \text{Second order integration of } \beta_{\text{arec}} \text{ pattern}) / T_{\text{cyc}} \end{aligned}$$

10

... Equation 1030

where in the above equation, the antiphase arm swing angle when β_{arec} is zero is the antiphase arm swing angle (the antiphase arm swing angle at time T_e) determined in S416. The second order integration of β_{arec} refers to a second order integrated value of the antiphase arm swing restoring angular acceleration from time T_s to T_e set as shown in Fig. 36. The reference initial antiphase arm swing angular velocity refers to the value of the aforesaid reference antiphase arm swing angular velocity (the first order differential value of the reference antiphase arm swing angle θ_{aref}) at time T_s .

15

20

The initial antiphase arm swing angle is set to agree with the reference initial antiphase arm swing angle. Alternatively, based on a finally determined antiphase arm swing angular acceleration (that is, the above determined sum of antiphase arm swing acceleration β_a and the restoring angular acceleration β_{arec} for preventing the

25

floor reaction force moment vertical component M_z from exceeding a permissible range) and the above determined initial antiphase arm swing angular velocity, the average value of the difference between an arm swing angle
5 calculated when an initial antiphase arm swing angle is set to agree with a reference initial antiphase arm swing angle and a reference antiphase arm swing angle, or an average value of the maximum value and the minimum value of the difference may be determined, and then the value
10 obtained by subtracting a half of the determined average value from the reference initial antiphase arm swing angle may be determined as the final initial antiphase arm swing angle. This arrangement makes it possible to prevent the absolute value of the difference between a calculated arm
15 swing angle and the reference antiphase arm swing angle from becoming excessively large.

One of the reasons that times T_s , T_m , T_{s2} , and T_{m2} have been set as described above is to prevent the floor reaction force horizontal component F_x from exceeding the
20 permissible range $[F_{xmin}, F_{xmax}]$ even if the body posture angular acceleration β is generated to set the body posture angular velocity back to the initial angular velocity of a reference body posture trajectory during the period from time T_m to T_{s2} and the period from time T_{m2} to
25 T_e . In other words, the floor reaction force horizontal component permissible range is sufficiently wide in the period from time T_m to T_{s2} and the period from time T_{m2} to

Te, so that the floor reaction force horizontal component F_x does not exceed the permissible range even if the body posture angular acceleration β is generated to restore the body posture angular velocity, while satisfying the
5 desired ZMP.

Another reason that the times T_s , T_m , T_{s2} , and T_{m2} have been set as described above is to prevent the floor reaction force moment vertical component M_z from exceeding the permissible range $[M_{zmin}, M_{zmax}]$ even if the antiphase
10 arm swing angular acceleration β_a is generated to set the antiphase arm swing angular velocity back to the initial angular velocity of a reference antiphase arm swing angle trajectory during the period from time T_m to T_{s2} and the period from time T_{m2} to T_e . In other words, the floor
15 reaction force moment vertical component permissible range is sufficiently wide in the period from time T_m to T_{s2} and the period from time T_{m2} to T_e , so that the floor reaction force moment vertical component M_z does not exceed the permissible range even if the antiphase arm swing angular
20 acceleration β_a is generated to restore the antiphase arm swing angular velocity.

After the processing of S316 of Fig. 24 is completed as described above, the processing proceeds to S210 of Fig. 23 wherein the horizontal body position and velocity at
25 the end of a generated gait (provisional normal gait) are converted into values observed from a supporting leg coordinate system (the coordinate system of X''' , Y''' , and

z''' shown in Fig. 17) associated with the supporting leg of that particular instant, and the values are defined as (X_e, V_xe) (X_e : Body horizontal position at the end; and V_xe : Body horizontal velocity at the end).

5 Subsequently, the processing proceeds to S212 wherein the difference between the initial horizontal body position and velocity (X_s, V_{xs}) and the horizontal position and velocity at the end (X_e, V_{xe}) is calculated, as illustrated. This difference $(X_s - X_e, V_{xs} - V_{xe})$ is
10 referred to as a horizontal body position and velocity boundary condition error (err_x, err_vx) . In a normal gait, the boundary condition must be satisfied, so that (X_s, V_{xs}) and (X_e, V_{xe}) must agree. Hence, the horizontal body position and velocity boundary condition error (err_x, err_vx) must be zero or substantially zero. In the first
15 reference example, (X_s, V_{xs}) that sets the horizontal body position and velocity boundary condition error (err_x, err_vx) to substantially zero is exploratorily determined.

 Subsequently, the processing proceeds to S214 wherein
20 it is determined whether the calculated horizontal body position and velocity boundary condition error (err_x, err_vx) falls within the permissible range appropriately set beforehand. Instead of setting the permissible range of a horizontal body position and velocity boundary
25 condition error as described above, it may be determined whether the difference between an initial divergent component $(X_s + V_{xs}/\omega_0)$ and a divergent component at an end

($X_e + V_{xe}/\omega_0$) and the difference between an initial convergent component ($X_s - V_{xs}/\omega_0'$) and a convergent component at an end ($X_e - V_{xe}/\omega_0'$) respectively fall within certain permissible ranges. As previously mentioned, ω_0 and ω_0' denote certain predetermined values.

If the determination result of S214 is NO, then the processing proceeds to S216. In this S216, a plurality of (two in the first reference example) initial value candidates ($X_s + \Delta X_s, V_{xs}$) and ($X_s, V_{xs} + \Delta V_{xs}$) is determined in the vicinity of (X_s, V_{xs}). Here, ΔX_s and ΔV_{xs} mean predetermined minute variation associated with X_s and V_{xs} , respectively. Then, taking each of these initial value candidates as an initial state of the horizontal body position and velocity, a normal gait is generated using a gait parameter by the same processing as that of the above S208. Further, the body position and velocity at the end of the generated normal gait are converted to obtain values ($X_e + \Delta X_{e1}, V_{xe} + \Delta V_{xe1}$) and ($X_e + \Delta X_{e2}, V_{xe} + \Delta V_{xe2}$) observed from a supporting leg coordinate system (the coordinate system of X''' , Y''' , and Z''' shown in Fig. 17) associated with the supporting leg at that particular instant. Here, ($X_e + \Delta X_{e1}, V_{xe} + \Delta V_{xe1}$) means the body position and velocity at an end that corresponds to ($X_s + \Delta X_s, V_{xs}$), and ($X_e + \Delta X_{e2}, V_{xe} + \Delta V_{xe2}$) corresponds to the body position and velocity at an end that corresponds to ($X_s, V_{xs} + \Delta V_{xs}$). In the processing for generating a normal gait (provisional gait) in this case,

the initial state (the state at time T_s) of a variable other than the horizontal body position and velocity may be set to the same value as that in a case where, for example, the initial value candidate of the horizontal
5 body position and velocity is set to (X_s, V_{xs}) . In S216, the same processing as that of the above S210 is carried out to determine the difference between each initial value candidate and the body position and velocity at an end corresponding thereto, i.e., the horizontal body position
10 and velocity boundary condition error corresponding to each initial value candidate $(X_s + \Delta X_s, V_{xs})$, $(X_s, V_{xs} + \Delta V_{xs})$.

Next, the processing proceeds to S218 wherein, based on the horizontal body position and velocity boundary condition error corresponding to each of (X_s, V_{xs}) and the
15 initial value candidates in the vicinity thereof $(X_s + \Delta X_s, V_{xs})$, $(X_s, V_{xs} + \Delta V_{xs})$, an initial value candidate following (X_s, V_{xs}) is determined by a searching method (a method in which a pseudo-Jacobian (sensitivity matrix) is determined and then a next candidate is determined by the steepest
20 descent method or the like, or the simplex method or the like). More specifically, a sensitivity matrix indicating a changing degree of a horizontal body position and velocity boundary condition error observed when a horizontal body position and a body horizontal velocity
25 are respectively changed minutely from the initial value candidate (X_s, V_{xs}) on the basis of the horizontal body position and velocity boundary condition errors associated

with each of (X_s, V_{xs}) and the initial value candidates in the vicinity thereof $(X_s + \Delta X_s, V_{xs})$, $(X_s, V_{xs} + \Delta V_{xs})$ is determined, and then, based on the determined sensitivity matrix, an initial value candidate (X_s, V_{xs}) that will
5 further reduces the horizontal body position and velocity boundary condition error is newly determined. After the new initial value candidate (X_s, V_{xs}) of the horizontal body position and velocity is determined as described above, the processing returns to S206.

10 The aforesaid processing (the processing from S206 to S218) is repeated as long as the determination result of S214 is NO. In this case, in S300 (refer to Fig. 24) of the processing for generating a normal gait corresponding to a new initial value candidate (X_s, V_{xs}) of the
15 horizontal body position and velocity (S208), the initial value of the body posture angular velocity is set to the value determined in S310 (refer to Fig. 24) in the processing of S208 that corresponds to the last time's initial value candidate (X_s, V_{xs}) of the horizontal body
20 position and velocity rather than being set to the initial value of the reference body posture angular velocity. And if the determination result of S214 is YES, then the processing leaves the repetition loop (S204) and proceeds to S220. The provisional normal gait generated
25 immediately before leaving the repetition loop of S204 will be obtained as the normal gait that satisfies the boundary condition.

In S220, an initial horizontal body position and velocity (X_0 , V_0) at an original initial time 0 (the end time of the current time gait), an initial vertical body position and velocity (Z_0 , V_{z0}) at the original initial
5 time 0, and initial body posture angle and angular velocity at the initial time 0 are determined.

Specifically, (X_0 , V_0) and (Z_0 , V_{z0}) are determined to be the values obtained by converting the horizontal body position/velocity and the vertical body position/
10 velocity, which are determined at the time of instant when a second turning gait is switched to a first turning gait, i.e., at time $k=T_{cyc}$ (time T_e-T_s), into the values observed from the supporting leg coordinate system (the X''' , Y''' , and Z''' coordinate system of Fig. 17) associated
15 with the supporting leg of the first step starting from time T_{cyc} (i.e., a second 1st turning gait) in a case where a gait is generated to satisfy a gait condition on the basis of a body inclination restoring moment ZMP-converted value pattern and the initial body posture angle
20 and angular velocity of a normal gait at time T_s that have been determined in S310 and the horizontal body position and velocity (X_s , V_{xs}) at time T_s after leaving the loop of S204. Similarly, the initial state posture angle and angular velocity are determined to be the values obtained
25 by converting the body posture angle and angular acceleration determined when time $k=T_{cyc}$ (time T_e-T_s) into values observed from the supporting leg coordinate system

(the X''' , Y''' , and Z''' coordinate system of Fig. 17) associated with the supporting leg of one step starting from time T_{cyc} (i.e., a second first turning gait).

Subsequently, the processing proceeds to S222 wherein
5 a normal gait initial divergent component $q[0]$ is determined according to the following equation.

$$q[0] = X_0 + V_0/\omega_0 \quad \dots \text{Equation 40}$$

where ω_0 takes a certain predetermined value, as
10 explained above in relation to the divergence.

Subsequently, the processing proceeds to S224 wherein the normal gait initial divergent component $q[0]$ is converted into a value observed from a current time gait's supporting leg coordinate system, and this is determined
15 as $q''[0]$. Further, the initial vertical body position and velocity (Z_0 , V_{z0}) is converted into a value observed from the current time gait's supporting leg coordinate system, and this is determined as (Z_0'' , V_{z0}'').

Supplementally, (Z_0'' , V_{z0}'') agrees with the vertical
20 body position and velocity at the end of a second turning gait observed from the supporting leg coordinate system of the second turning gait (the X'' , Y'' , and Z'' coordinate system of Fig. 17). In addition, $q''[0]$ also agrees with the divergent component at the end of the second turning
25 gait observed from the supporting leg coordinate system of the second turning gait (the X'' , Y'' , and Z'' coordinate system of Fig. 17). Alternatively, therefore, (Z_0'' , V_{z0}'')

and $q''[0]$ may be calculated by utilizing these properties.

The processing further proceeds to S226 wherein initial antiphase arm swing angle and angular velocity (θ_{az0} , ω_{az0}) at the original initial time 0 (the end time of the current time gait) are determined, and further, (5 θ_{az0}'' , ω_{az0}''), which is the value observed from the current time's gait supporting leg coordinate system is determined. To be more specific, (θ_{az0} , ω_{az0}) is determined to be the value obtained by converting the antiphase arm swing angle and angular velocity, which are (10 determined at the time of instant when a second turning gait is switched to a first turning gait, i.e., at time $k=T_{cyc}$ (time T_e-T_s), in a case where a gait is generated to satisfy a gait condition on the basis of an antiphase arm swing restoring angular acceleration pattern, and (15 initial (time T_s) antiphase arm swing angle and angular velocity of a normal gait that have been determined in S314 and S316 (more specifically, in a case where an antiphase arm swing angle trajectory is determined such that a floor reaction force moment vertical component does (20 not exceed a permissible range in a period other than the body posture angle and antiphase arm swing angle restoring period, and the antiphase arm swing angle trajectory is determined such that the sum of the reference antiphase arm swing angular acceleration β_{aref} and the antiphase arm swing restoring angular acceleration β_{arec} is generated in (25 the body posture angle and antiphase arm swing angle

restoring period), into a value observed from the supporting leg coordinate system (the X''' , Y''' , and Z''' coordinate system of Fig. 17) associated with the supporting leg of one step starting from time T_{cyc} (i.e.,
5 a second 1st turning gait).

Thus, the processing of S024 of Fig. 13, that is, the subroutine processing for determining an initial state of a normal gait is finished.

Subsequently, the processing proceeds to S026 of Fig.
10 13 wherein the gait parameters of the current time gait are determined (some are provisionally determined). To be more specific, in S026, the following processing is carried out according to the flowchart shown in Fig. 39.

First, in S600, the foot trajectory parameters of the
15 current time gait are set such that the foot position/posture trajectory of the current time gait continues to the foot position/posture trajectory of a normal gait.

Specifically, the free leg foot position/posture at
20 the start of the current time gait (the initial value of the free leg foot position/posture of the current time gait) is set to current free leg position/posture observed from the current time gait's supporting leg coordinate system (the free leg position/posture at the end of the
25 last time's gait). The supporting leg foot position/posture at the start of the current time gait (the initial value of the current time gait's supporting

leg foot position/posture) are set to current supporting
leg foot position/posture observed from the current time
gait's supporting leg coordinate system (the supporting
leg foot position/posture at the end of the last time's
5 gait). The free leg foot position/posture at the end of
the current time gait is determined on the basis of a next
time gait's supporting leg coordinate system observed from
the current time gait's supporting leg coordinate system
(a required value of the free leg landing position/posture
10 of the first step related to the current time gait). More
specifically, the free leg foot position/posture at the
end of the current time gait are determined such that a
representative point of a free leg foot 22 agrees with the
origin of the next time gait's supporting leg coordinate
15 system observed from the current time's gait supporting
leg coordinate system when the free leg foot 22 is turned,
from the free leg foot position/posture at the end of the
current time gait, until substantially the entire surface
of the sole of the foot 22 comes in contact with the
20 ground without slippage, while maintaining the free leg
foot 22 in contact with a floor.

At the end of the current time gait, the supporting
leg foot 22 is off the floor and floating. To determine
the trajectory after the supporting leg foot 22 leaves the
25 floor, an expected supporting leg foot landing
position/posture is set. The expected supporting leg foot
landing position/posture is set on the basis of the next

but one time gait's supporting leg coordinate system
observed from the current time gait's supporting leg
coordinate system (a required value of the free leg foot
position/posture of the second step related to the current
5 time gait). To be more specific, the expected supporting
leg foot landing position/posture is determined such that
a representative point of the foot 22 obtained when the
foot 22 is turned from that position/posture without
slippage until substantially entire surface of the sole of
10 the foot 22 is brought into contact with the floor while
holding the foot 22 in contact with the floor agrees with
the origin of the next but one time gait's supporting leg
coordinate system observed from the current time gait's
supporting leg coordinate system.

15 The supporting leg foot position/posture at the end
of the current time gait is determined by generating a
foot position/posture trajectory from a current supporting
leg position/posture (the supporting leg foot
position/posture at the start of the current time gait) to
20 the expected foot landing position/posture corresponding
to the next time gait's supporting leg coordinate system
(the required value of the free leg foot landing
position/posture of the second step in the aforesaid
required parameter) by using the finite-duration setting
25 filter until the end of the current time gait.

Subsequently, the processing proceeds to S602 wherein
the reference body posture trajectory parameter of the

current time gait is determined in the same manner as that for the first turning gait and the second turning gait of a normal gait. The aforesaid parameter, however, is set such that the reference body posture trajectory of the current time gait continuously connects to the reference body posture trajectory of the above normal gait (such that the reference body posture angle and the angular velocity at the end of the current time gait agree with the reference body posture angle and the angular velocity, respectively, at the start of a normal gait). In the first reference example, the reference body posture related to an inclination angle refers to a steady vertical posture in both a current time gait and a normal gait.

Next, the processing proceeds to S604 wherein the reference arm posture trajectory parameters of the current time gait are determined in the same manner as that for the first turning gait and the second turning gait of the normal gait. The above parameters, however, are set such that the reference arm posture at the start of the current time gait and the changing rate thereof agree with the current instantaneous values of a reference arm posture and the changing rate thereof, and the arm posture trajectory of the current time gait continuously connects with the arm posture trajectory of the normal gait. For the arm posture trajectory parameters determined here, the parameters related to, for example, a total center-of-

gravity position of both arms 5, 5 (a relative position with respect to the body 3), a lateral interval between right and left hands (the distal ends of both arms 5, 5), and an antiphase arm swing angle are determined, as in the case where the normal gait parameters are determined (S104 in Fig. 15). In the first reference example, the total center-of-gravity position of both arms 5, 5 is set so as to be maintained at a constant level with respect to the body 3.

The processing then proceeds to S606 wherein the floor reaction force vertical component trajectory parameters of the current time gait are determined such that the floor reaction force vertical component trajectory defined by the parameters will be a substantially continuous (values are not jumping in steps) trajectory as illustrated in Fig. 6 mentioned above, as in the case of the first turning gait and the second turning gait of a normal gait.

The floor reaction force vertical component trajectory parameters, however, are determined such that both the total center-of-gravity vertical position and velocity and the floor reaction force vertical component trajectory of the current time gait continuously connect with the normal gait.

To be specific, first, the value (Z_0'' , V_{z0}'') obtained by converting the vertical body position and velocity at the start of the normal gait that has been finally

determined by the processing of S024 of Fig. 13 mentioned above (the processing for determining the initial state of the normal gait) into the value observed from a current time's gait supporting leg coordinate system, i.e., the
5 total center-of-gravity vertical position and velocity at the start of the normal gait observed from the current time's gait supporting leg coordinate system are determined using, for example, the above Equation 04 (or a kinematics model of the robot 1) on the basis of ($Z0''$,
10 $Vz0''$) or the like determined in S224 of Fig. 23. To be more specific, the total center-of-gravity vertical position at the start of the normal gait observed from the current time's gait supporting leg coordinate system is determined by substituting the body mass point vertical
15 position of the model shown in Fig. 12, which corresponds to the vertical body position $Z0''$ of the normal gait determined in S224, and the leg mass point vertical positions of a supporting leg and a free leg, which correspond to the values obtained by converting individual
20 foot positions at the start of the normal gait into the values observed from the current time's gait supporting leg coordinate system, into Equation 04. Further, the total center-of-gravity vertical velocity at the start of the normal gait observed from the current time's gait
25 supporting leg coordinate system is determined by substituting the body mass point vertical velocity of the model shown in Fig. 12, which corresponds to the body

vertical velocity V_{z0} of the normal gait determined in S224, and the leg mass point vertical velocities of a supporting leg and a free leg, which correspond to the values obtained by converting individual foot vertical velocities at the start of the normal gait into the values
5 observed from the current time's gait supporting leg coordinate system, into an equation derived from differentiating both sides of Equation 04. Alternatively, the initial total center-of-gravity vertical position and
10 velocity may be calculated by using a more precise model.

Then, the initial total center-of-gravity vertical position and velocity of the normal gait determined as described above is substituted into the terminal total center-of-gravity vertical positions and velocities of the
15 following equations 41a and 41b, and the total center-of-gravity vertical position and velocity of the last time's desired gait instantaneous value (to be more precise, the value obtained by converting the terminal state of the last time's desired gait into the current time's
20 supporting leg coordinate system) into the initial total center-of-gravity vertical positions and velocities of Equations 41a and 41b. A floor reaction force vertical component pattern (to be more specific, a parameter value) of the current time gait is determined such that the
25 relationship between Equations 41a and 41b is satisfied. The integrated values in Equations 41a and 41b are to be the integrated values in the period from the start to the

end of the current time gait.

Terminal total center-of-gravity vertical position -
Initial total center-of-gravity vertical position
5 = Second order integration of (Floor reaction force
vertical component / Total mass of the robot)
+ Second order integration of acceleration of gravity
+ Initial total center-of-gravity vertical velocity *
Duration of one step

10 ... Equation 41a

Terminal total center-of-gravity vertical velocity -
Initial total center-of-gravity vertical velocity
= First order integration of (Floor reaction force
15 vertical component / Total mass of the robot)
+ First order integration of acceleration of gravity

... Equation 41b

20 where the acceleration of gravity takes a negative
value.

To be more specific, first, at least two parameters
out of the floor reaction force vertical component
parameters (e.g., times of break points) that define the
floor reaction force vertical component pattern as shown
25 in Fig. 6 are taken as independent unknown variables. The
values of the unknown variables are determined by solving
a simultaneous equation composed of Equations 41a and 41b.

The floor reaction force vertical component parameters to be selected as the unknown variables may be, for example, the height (the peak value of the floor reaction force vertical component) and the width (duration of single stance period) of the trapezoid shown in Fig. 6. In this case, the slopes of both sides of the trapezoid shown in Fig. 6 take values determined beforehand on the basis of a current time gait cycle or the like, or the values of times of the break points of the floor reaction force vertical component pattern, excluding the time at which a single stance period is switched to a floating period, that has been determined beforehand on the basis of a current time gait cycle or the like. Supplementally, if only one unknown variable is given, then no solution generally exists that satisfies the simultaneous equation of Equations 41a and 41b.

Subsequently, the processing proceeds to S608 wherein a floor reaction force horizontal component permissible range [F_{xmin} , F_{xmax}] (to be more specific, the parameters defining the pattern of the floor reaction force horizontal component permissible range) is set in the same manner as that for the first turning gait and the second turning gait of a normal gait. For instance, the floor reaction force horizontal component permissible range is set according to the pattern shown in Fig. 40. In the first reference example, the floor reaction force horizontal component permissible range is set according to

the aforesaid Equation 12 on the basis of the floor reaction force vertical component pattern determined previously in S606.

Then, the processing proceeds to S610 wherein a floor
5 reaction force moment vertical component permissible range
[Mzmin, Mzmax] (to be more specific, the parameters
defining the pattern of the floor reaction force moment
vertical component permissible range) is set in the same
manner as that for the first turning gait and the second
10 turning gait of a normal gait. For instance, the floor
reaction force moment vertical component permissible range
is set according to the pattern shown in Fig. 41. In the
first reference example, the floor reaction force moment
vertical component permissible range is set according to
15 the aforesaid Equation 1012 on the basis of the floor
reaction force vertical component pattern determined
previously in S606.

Subsequently, the processing proceeds to S612 wherein
the ZMP trajectory of the current time gait (specifically,
20 the parameters defining the ZMP trajectory, such as times
and positions of break points of the trajectory) is set,
as shown in Fig. 7, such that it exhibits a high stability
margin and no sudden changes, as in the first turning gait
and the second turning gait of a normal gait. The
25 parameters are set such that the ZMP trajectory of the
current time gait continuously connects with the ZMP
trajectory of the aforesaid normal gait. In other words,

the ZMP trajectory parameters are determined so that the ZMP position at the end of the current time gait agrees with the ZMP position at the start of the normal gait. In this case, in a running gait, the times and positions of break points of the ZMP trajectory in a single stance period may be set in the same manner as that for setting the ZMP trajectory parameters of the normal gait described above. And the ZMP trajectory parameters may be set so that a desired ZMP trajectory in a floating period linearly changes in succession from the start of the floating period to the ZMP position at the start of a normal gait.

It should be noted that the ZMP trajectory parameters of the current time gait determined in S612 are merely temporary, and will be corrected, as it will be discussed hereinafter. For this reason, the ZMP trajectory of the current time gait set as described above will be hereinafter referred to as a provisional desired ZMP trajectory of a current time gait.

Lastly, the processing proceeds to S614 wherein a body posture angle and antiphase arm swing angle restoring period $[T_a, T_b]$ is set. The body posture angle and antiphase arm swing angle restoring start time T_a corresponds to T_m in the second turning gait of a normal gait, while body posture angle and antiphase arm swing angle restoring end time T_b corresponds to T_{s2} in the second turning gait of the normal gait. These times T_a

and Tb are set in the same manner as that for setting Tm and Ts2.

Returning to the explanation of Fig. 13, after carrying out the processing shown in S026 (the processing for determining the gait parameters of the current time gait) as described above, the program proceeds to S028 wherein the gait parameters (ZMP trajectory parameters) of the current time gait are corrected, and the parameter of the antiphase arm swing angle is determined. In this processing, the ZMP trajectory parameters are corrected so as to make the body position/posture trajectory continue or approximate to a normal gait, and a parameter related to the antiphase arm swing angle of the current time gait is determined to make the antiphase arm swing angle converge to the antiphase arm swing angle trajectory of the normal gait.

Fig. 42 shows the subroutine flowchart illustrating the processing.

First, the processing proceeds to S702 via S700 and temporarily generates a provisional current time gait until the time at which the current time gait ends on the basis of a provisional desired ZMP pattern and other current time gait parameters.

In S702, the following processing will be carried out according to the flowchart shown in Fig. 43.

The explanation will now be given. In S800, various elements are initialized. Specifically, zero is

substituted into time k for generating a provisional gait. Furthermore, the initial state of the current time gait is obtained by converting the terminal state of the last time's desired gait (to be more specific, the end values of the gait states, including a horizontal body position and velocity, a vertical body position and velocity, a body posture angle and its angular velocity, a desired foot position/posture, and a desired arm posture) into a current time's supporting leg coordinate system.

Supplementally, the desired arm posture includes desired antiphase arm swing angle and angular velocity.

Subsequently, the processing goes through S802 and proceeds to S804 wherein it is determined whether time k for generating a provisional gait is before current time gait end time T_{curr} (whether $k \leq T_{curr}$). If the determination result is YES, then the processing proceeds to a current time gait instantaneous value determining subroutine of S806 to determine an instantaneous value of time k of the current time gait. In the gait

instantaneous value determining subroutine of S806, a provisional gait is generated as shown in Fig. 25. However, current time gait parameters are used in place of normal gait parameters, as the gait parameters, in the same manner as that of S306 previously described.

Subsequently, the processing proceeds to S808 to increment time k for generating a provisional gait by Δk , and then returns to S804.

If the determination result of S804 is NO, then the processing of the flowchart shown in Fig. 43 is completed.

The processing discussed above generates the provisional current time gait from the start and the end thereof.

Subsequently, the processing proceeds to S704 wherein a terminal divergent component $q0[k]$ ($k=Tcurr$) is determined according to the equation shown in the figure (Equation 10 given above) from the horizontal body position/velocity (Xe , Vxe) at the end of the current time gait determined in S702 as described above.

The processing then proceeds to S706 wherein a terminal divergent component error $errq$, which is the difference between a current time gait end divergent component $q0[k]$ and a normal gait initial divergent component q'' (the one determined in S224 of Fig. 23), is determined using the illustrated equation. Further, the processing proceeds to S708 wherein it is determined whether the determined terminal divergent component error $errq$ falls within a permissible range (a range in the vicinity of zero).

If the determination result of S708 is NO, then the processing proceeds to S710 wherein $a = \Delta a$ (Δa being a predetermined extremely small amount) is set, and a provisional current time gait to the end thereof is calculated, as in the aforesaid S702, on the basis of the desired ZMP obtained by adding a trapezoidal correction to

the current provisional desired ZMP pattern according to the relationship shown in Fig. 44. Here, referring to Fig. 44, "a" denotes the height of the trapezoidal pattern for correcting a provisional desired ZMP so as to make the

5 current time gait terminal divergent component agree with the normal gait initial divergent component as much as possible (so as to approximate the horizontal body position/posture trajectory of the current time gait to the horizontal body position/posture trajectory of the

10 normal gait). In this case, in the first reference example, the provisional desired ZMP is corrected during the period in which substantially the entire surface of the sole of the supporting leg foot 22 comes in contact with the ground (the entire-sole-in-contact-with-the-

15 ground period), that is, during the period in which the floor reaction force horizontal component permissible range is sufficiently wide, and the times of the break points of the above trapezoidal pattern are set to balance with the times of the break points of the provisional

20 desired ZMP in the entire-sole-in-contact-with-the-ground period. The setting $a=\Delta a$ is given in S710 to observe a change in the terminal divergent component error $errq$ when the current provisional desired ZMP trajectory is corrected by an extremely small amount according to the

25 aforesaid trapezoidal pattern.

After generating the provisional current time gait to the end with the provisional desired ZMP trajectory

corrected using $a=\Delta a$ in S710 as described above, the processing further proceeds to S712 wherein a terminal divergent component $q1[k]$ in this provisional current time gait is determined according to the equation shown in the figure (the above Equation 10) on the basis of a horizontal body position/velocity ($Xe1$, $Vxe1$) at the end of the provisional current time gait determined in S710.

In S710, Δa has been a constant of an extremely small amount appropriately set in the first reference example. Alternatively, Δa may be set such that Δa decreases as the terminal divergent component error $errq$ is decreased by repeated calculation, which will be explained below. However, even if it is set as a constant, it is possible to maintain the terminal divergent component error $errq$ within a permissible range by performing a few repetitive calculations.

Subsequently, the processing proceeds to S714 wherein a parameter sensitivity r (changing rate of the terminal divergent component error with respect to Δa) is determined according to the equation shown in the figure. The processing further proceeds to S716 wherein the correction amount of the trapezoidal pattern having, as its height a , the value obtained by $a=-errq/r$, that is, the value obtained by dividing the terminal divergent component error $errq$ determined in S706 by the parameters sensitivity r determined in S714, is added to the provisional desired ZMP pattern according to the

relationship shown in Fig. 44, thereby correcting the provisional desired ZMP pattern (a new provisional desired ZMP pattern is determined).

Then, the processing returns to S702. As long as the determination result of S708 is NO, the processing from S702 to S716 described above is repeated. When the determination result of S708 changes to YES, the processing leaves the repetition loop (S700) and moves forward to S718.

In S718, the pattern of the body posture restoring moment ZMP-converted value (ZMPrec) of the current time gait is determined primarily on the basis of the difference between a terminal body posture angle of the provisional current time gait and an initial body posture angle of a normal gait, and the difference between a terminal body posture angular velocity of the provisional current time gait and an initial body posture angular velocity of a normal gait such that the body posture angle trajectory of the current time gait approximates the body posture angle trajectory of the normal gait. The ZMPrec determined here is used for correcting a provisional desired ZMP so that the agreement between the divergent component at the end of the current time gait and the divergent component at the start of the normal gait (the condition in S708) may be maintained even when a body posture angular acceleration is generated to connect (bring close) the body posture angle trajectory to the

normal gait in the period, wherein the floor reaction
force horizontal component permissible range becomes
sufficiently wide (the period in a single stance period),
by the processing for generating a current time gait
instantaneous value, which will be described hereinafter.

The ZMPrec exhibits a trapezoidal pattern similar to
that explained in relation to the processing for
generating the normal gait. To be more precise, the
ZMPrec is determined as follows. The trapezoidal pattern
of the ZMPrec of the current time gait is set in the same
manner as that for the trapezoidal pattern of the ZMPrec
in the period of the second turning gait shown in Fig. 30,
the times (break points) of apexes of the trapezoid being
known (more specifically, the times of the break points of
the trapezoid are balanced with the break point times of
the desired ZMP), and the height of the trapezoid
(parameter) of the ZMPrec is determined as described below,
taking the height of the trapezoid as an unknown number.
In this case, the time at which the trapezoid pattern of
the ZMPrec begins to rise is denoted by T_a , and the time
at which the trapezoid pattern returns to zero is denoted
by T_b .

It is usually impossible to continuously connect both
body posture angle and body posture angular velocity to a
normal gait at the end of the current time gait if there
is only one unknown parameter of the body posture
restoring moment ZMP-converted value pattern. For this

reason, in the first reference example, an unknown parameter is determined so that the state of a gait generated gradually approximates the state of a normal gait over a plurality of steps.

5 Supplementally, the ZMPrec pattern in a single gait may be complicated to produce two or more unknown parameters to continuously connect both the body posture angle and the body posture angular velocity to the normal gait at the end of the current time gait. This, however,
10 may lead to a ZMPrec pattern with excessive staggered variation.

 The following will explain the principle of calculation and then the procedure of the calculation.

 As previously described, the difference between the
15 terminal body posture angle of the provisional current time gait that has been determined with the height of the trapezoid of the ZMPrec pattern being zero in S702 as discussed above and the initial body posture angle of the normal gait is determined, and the determined difference
20 is defined as θ_{err} . Further, the difference between the terminal body posture angular velocity of the provisional current time gait and the initial body posture angular velocity of the normal gait is determined, and the determined difference is denoted by $v\theta_{err}$.

25 Here, it is assumed that the current time gait is generated, defining the height of the trapezoid of the ZMPrec pattern as a certain value b_{curr} , and then the

first turning gait is generated by the same algorithm as that of the current time gait. It is assumed that the body posture restoring moment ZMP-converted value ZMPrec pattern of the first turning gait is based on the sum of the ZMPrec pattern of the first turning gait (the trapezoidal pattern shown in Fig. 30, the height of which is acycl as mentioned above), determined in S310 of Fig. 24 and a certain value b1.

The gait generated as described above is referred to as a ZMPrec corrected gait, and its end (the end of the first turning gait) body posture angle and angular velocity are denoted by $\theta 1$ and $v\theta 1$, respectively.

The body posture angle and angular velocity at the end of the first turning gait are denoted by $\theta 1org$ and $v\theta 1org$, respectively, of the original normal gait determined at the point when the subroutine processing for determining the initial state of the normal gait in S024 is completed (the normal gait in a case where the body posture angle and angular velocity at the start of the normal gait finally determined in S310 are taken as the initial values, and the ZMPrec pattern is the pattern determined in S310 (the trapezoidal pattern shown in Fig. 30, the height thereof being acycl)).

Here, $\Delta\theta 1$ and $\Delta v\theta 1$ are defined as follows:

$$\Delta\theta 1 = \theta 1 - \theta 1org \quad \dots \text{Equation 50}$$

$$\Delta v\theta 1 = v\theta 1 - v\theta 1org \quad \dots \text{Equation 51}$$

$\Delta\theta_1$ and $\Delta v\theta_1$ mean the differences in body posture angle and angular velocity, respectively, between the corrected ZMPrec gait and the original normal gait at the point when these two gaits have been generated to the end of the first turning gait. If $\Delta\theta_1$ and $\Delta v\theta_1$ are zero, then the second turning gait generated according to the same algorithm as that of the current time gait, setting the height of the trapezoid of the ZMPrec pattern as $acyc2$, and following the corrected ZMPrec, will agree with the original normal gait.

Thus, the height $bcurr$ of the trapezoid of the current time gait and the height $b1$ of the trapezoid of the first turning gait at which $\Delta\theta_1$ and $\Delta v\theta_1$ reach zero may be determined, and the determined $bcurr$ may be taken as the finally determined height of the trapezoid of the current time gait.

The dynamic model related to the body posture angle of the robot 1 has the linear characteristic represented by flywheels FHx and FHy shown in Fig. 12. Hence, $\Delta\theta_1$ and $\Delta v\theta_1$ carry the relationships shown below with the height $bcurr$ of the trapezoid of the current time gait, the height $b1$ of the trapezoid of the first turning gait, the difference θ_{err} between the terminal body posture angle of the provisional current time gait and the initial body posture angle of the normal gait, and the difference $v\theta_{err}$ between the terminal body posture angular velocity of the

provisional current time gait and the initial body posture angular velocity of the normal gait.

$$\Delta\theta_1 = c_{11}*b_{curr}+c_{12}*b_1+\theta_{err}+e_1*v\theta_{err} \quad \dots \text{Equation 52}$$

5 $\Delta v\theta_1 = c_{21}*b_{curr}+c_{22}*b_1+e_2*v\theta_{err} \quad \dots \text{Equation 53}$

where c_{11} , c_{12} , c_{21} , c_{22} , e_1 , and e_2 are coefficients uniquely determined primarily by the gait cycles of a current time gait and a first turning gait and the
10 parameters (particularly the parameters related to time) of a body posture restoring moment ZMP-converted value ZMPrec pattern.

Based on the aforementioned principle, the calculation procedure first determines the body posture
15 angle difference θ_{err} and the angular velocity difference $v\theta_{err}$ in the boundary between the provisional current time gait and the normal gait.

Then, the coefficients c_{11} , c_{12} , c_{21} , c_{22} , e_1 , and e_2 of Equations 52 and 53 are determined primarily on the
20 basis of the gait cycles of a current time gait and a first turning gait and the parameters (particularly the parameters related to time) of a body posture restoring moment ZMP-converted value ZMPrec pattern.

Next, the height b_{curr} of the trapezoid of the
25 current time gait and the height b_1 of the trapezoid of the first turning gait are determined such that the right sides of Equations 52 and 53 become zero. In other words,

bcurr and bl are determined by solving the simultaneous equation having the left sides of Equation 52 and Equation 53 set to zero.

5 Lastly, the height of the trapezoid of the trapezoidal pattern of the body posture restoring moment ZMP-converted value (ZMPrec) of the current time gait is set to the height bcurr of the trapezoid of the above determined current time gait.

10 Subsequently, the processing proceeds to S720 wherein the pattern obtained by adding the body posture restoring moment ZMP-converted value pattern determined as described above in relation to S718 to the current provisional desired ZMP pattern (the provisional desired ZMP pattern when the processing leaves the repetition loop of S700) is
15 determined as the desired ZMP pattern of the current time gait. This processing is the same as the processing for adding the trapezoidal pattern having the height of Δa in S710 to the provisional desired ZMP pattern.

20 The following will describe the reason for adding the body posture restoring moment ZMP-converted value pattern to the provisional desired ZMP pattern.

The provisional current time gait generated in the loop of S700 is generated by setting the body posture restoring moment ZMP-converted value ZMPrec to zero (by
25 setting the height parameter of the trapezoidal pattern of ZMPrec to zero). In the provisional current time gait finally generated in the loop of S700, the body

position/velocity continues to or approximates a normal gait, whereas the body posture angle deviates from the body posture angle of the normal gait and undesirably diverts in some cases.

5 The body posture restoring moment ZMP-converted value pattern determined in S718 is used to generate a body posture angular acceleration for approximating a deviation of a body posture angle with respect to a normal gait to zero.

10 If, however, a body posture angular acceleration based on the body posture restoring moment ZMP-converted value pattern determined in S718 is generated without correcting the provisional desired ZMP pattern finally obtained in the loop of S700, then the horizontal body
15 position trajectory has to be deviated from a horizontal body position trajectory of the above provisional current time gait in order to satisfy the dynamic balance condition (the moment in which the resultant force of the gravity and the inertial force of the robot acting on the
20 desired ZMP, excluding a vertical component, is zero). For this reason, in the present embodiment, the provisional desired ZMP pattern is corrected by ZMPrec in order to obviate the need for deviation of the horizontal body position trajectory from the one finally obtained in
25 the loop of S700.

 If a body posture angular acceleration based on the body posture restoring moment ZMP-converted value pattern

determined in S718 is generated in addition to the motion of the above provisional current time gait, then the ZMP (the point at which the moment of the resultant force of the gravity and the inertial force produced by a motion, excluding vertical component, reaches zero) deviates by the body posture restoring moment ZMP-converted value. Conversely, therefore, by using the pattern, which is obtained by adding the body posture restoring moment ZMP-converted value pattern to a provisional desired ZMP pattern, as a desired ZMP pattern, the same body translational motion as that of the above provisional current time gait can be obtained by generating the current time gait that satisfies the desired ZMP pattern while generating a body posture angular acceleration of the body inclination mode based on the body posture restoring moment ZMP-converted value pattern determined in S718.

The above is the reason why the pattern obtained by adding the body posture restoring moment ZMP-converted value pattern to the provisional desired ZMP pattern is used as the desired ZMP pattern.

Subsequently, the processing proceeds to S722 wherein an antiphase arm swing restoring angular acceleration pattern is determined such that the antiphase arm swing angle trajectory approximates to the antiphase arm swing angle trajectory of a normal gait on the basis of the difference between the terminal antiphase arm swing angle

of the provisional current time gait and the initial
antiphase arm swing angle of the normal gait and the
difference between the terminal antiphase arm swing
angular velocity of the provisional current time gait and
5 the initial antiphase arm swing angular velocity of the
normal gait. The method for determining the pattern is
almost the same as the method for determining the body
posture restoring moment ZMP-converted value pattern in
S718, except that variable names are different as shown
10 below:

Body posture restoring moment ZMP-converted value pattern
→ Antiphase arm swing restoring angular acceleration
pattern
15 Horizontal component → Moment vertical component

This will be explained in detail below. The
antiphase arm swing restoring angular acceleration pattern
is used in the processing for generating a current time
20 gait instantaneous value, which will be discussed
hereinafter, to make a correction so as to connect
(approximate) the antiphase arm swing angle trajectory to
the normal gait in the period wherein the floor reaction
force moment vertical component permissible range becomes
25 sufficient wide (a single stance period).

The antiphase arm swing restoring angular
acceleration pattern is a trapezoidal pattern similar to

that explained in relation to the processing for
generating the normal gait. To be more precise, the
antiphase arm swing restoring angular acceleration pattern
is determined as follows. The trapezoidal pattern of the
5 antiphase arm swing restoring angular acceleration of the
current time gait is set in the same manner as that for
the trapezoidal pattern of the antiphase arm swing
restoring angular acceleration pattern in the period of
the second turning gait shown in Fig. 36, the times (break
10 points) of apexes of the trapezoid being known (more
specifically, the times of the break points of the
trapezoid are matched to the break point times of the
desired ZMP), and the height of the trapezoid (parameter)
of the antiphase arm swing restoring angular acceleration
15 is determined as described below, taking the height of the
trapezoid as an unknown number. In this case, the time at
which the trapezoid pattern of the antiphase arm swing
restoring angular acceleration begins to rise is denoted
by T_a , and the time at which the trapezoid pattern returns
20 to zero is denoted by T_b .

It is usually impossible to continuously connect both
antiphase arm swing angle and antiphase arm swing angular
velocity to a normal gait at the end of the current time
gait if there is only one unknown parameter of the
25 antiphase arm swing restoring angular acceleration pattern.
For this reason, in the first reference example, an
unknown parameter is determined so that the state of a

gait generated gradually approximates the state of a normal gait over a plurality of steps.

Supplementally, the antiphase arm swing restoring angular acceleration pattern in a single gait may be complicated to produce two or more unknown parameters to continuously connect both the antiphase arm swing angle and antiphase arm swing angular velocity to the normal gait at the end of the current time gait. This, however, may lead to an antiphase arm swing restoring angular acceleration pattern with excessive staggered variation.

As previously described, the difference between the terminal antiphase arm swing angle of the provisional current time gait that has been determined with the height of the trapezoid of the antiphase arm swing restoring angular acceleration pattern set to zero in S702 as discussed above and the initial antiphase arm swing angle of the normal gait is determined, and the determined difference is defined as θ_{zerr} . Further, the difference between the terminal antiphase arm swing angular velocity of the provisional current time gait and the initial antiphase arm swing angular velocity of the normal gait is determined, and the determined difference is denoted by $v\theta_{zerr}$.

Here, it is assumed that the current time gait is generated, defining the height of the trapezoid of the antiphase arm swing restoring angular acceleration pattern as a certain value $bzcurr$, and then the first turning gait

is generated by the same algorithm as that of the current time gait. It is assumed that the antiphase arm swing restoring angular acceleration pattern of the first turning gait is based on the sum of the antiphase arm swing restoring angular acceleration pattern (the trapezoidal pattern shown in Fig. 36, the height of which is $azcycl$ as mentioned above), determined in S314 of Fig. 24 and a certain value $bz1$.

The gait generated as described above is referred to as an antiphase arm swing restoring angular acceleration corrected gait, and its end (the end of the first turning gait) antiphase arm swing angle and angular velocity are denoted by $\theta z1$ and $v\theta z1$, respectively.

The antiphase arm swing angle and angular velocity at the end of the first turning gait are denoted by $\theta z1org$ and $v\theta z1org$, respectively, of the original normal gait determined at the point when the subroutine processing for determining the initial state of the normal gait in S024 is completed (the normal gait in a case where the antiphase arm swing angle and angular velocity at the start of the normal gait finally determined in S314 are taken as the initial values, and the antiphase arm swing restoring angular acceleration pattern is the pattern determined in S314 (the trapezoidal pattern shown in Fig. 36, the height thereof being $azcycl$)).

Here, $\Delta\theta z1$ and $\Delta v\theta z1$ are defined as follows:

$$\Delta\theta_{z1} = \theta_{z1} - \theta_{z1org} \quad \dots \text{Equation 1050}$$

$$\Delta v\theta_{z1} = v\theta_{z1} - v\theta_{z1org} \quad \dots \text{Equation 1051}$$

5 $\Delta\theta_{z1}$ and $\Delta v\theta_{z1}$ mean the differences in antiphase arm swing angle and angular velocity, respectively, between the corrected antiphase arm swing restoring angular acceleration gait and the original normal gait at the point when these two gaits have been generated to the end of the first turning gait. If $\Delta\theta_{z1}$ and $\Delta v\theta_{z1}$ are zero,
10 then the second turning gait generated according to the same algorithm as that of the current time gait, setting the height of the trapezoid of the antiphase arm swing restoring angular acceleration pattern as $azcyc2$, and following the corrected antiphase arm swing restoring
15 angular acceleration gait, will agree with the original normal gait.

Thus, the height $bzcurr$ of the trapezoid of the current time gait and the height $bz1$ of the trapezoid of the first turning gait at which $\Delta\theta_{z1}$ and $\Delta v\theta_{z1}$ reach zero
20 may be determined, and the determined $bzcurr$ may be taken as the finally determined height of the trapezoid of the current time gait.

The dynamic model related to the antiphase arm swing angle of the robot 1 has the linear characteristic
25 represented by a flywheel FH_{az} shown in Fig. 12. Hence, $\Delta\theta_{z1}$ and $\Delta v\theta_{z1}$ carry the relationships shown below with the height $bzcurr$ of the trapezoid of the current time

gait, the height $bz1$ of the trapezoid of the first turning
gait, the difference $\theta zerr$ between the terminal antiphase
arm swing angle of the provisional current time gait and
the initial antiphase arm swing angle of the normal gait,
5 and the difference $v\theta zerr$ between the terminal antiphase
arm swing angular velocity of the provisional current time
gait and the initial antiphase arm swing angular velocity
of the normal gait.

$$10 \quad \Delta\theta z1 = cz11*bzcurr + cz12*bz1 + \theta zerr + ez1*v\theta zerr$$

... Equation 1052

$$\Delta v\theta z1 = cz21*bzcurr + cz22*bz1 + ez2*v\theta zerr$$

... Equation 1053

15 where $cz11$, $cz12$, $cz21$, $cz22$, $ez1$, and $ez2$ are
coefficients uniquely determined primarily by the gait
cycles of a current time gait and a first turning gait and
the parameters (particularly the parameters related to
time) of an antiphase arm swing restoring angular
20 acceleration pattern.

Based on the aforementioned principle, the
calculation procedure first determines the antiphase arm
swing angle difference $\theta zerr$ and the angular velocity
difference $v\theta zerr$ in the boundary between the provisional
25 current time gait and the normal gait.

Then, the coefficients $cz11$, $cz12$, $cz21$, $cz22$, $ez1$,
and $ez2$ of Equations 1052 and 1053 are determined

primarily on the basis of the gait cycles of a current time gait and a first turning gait and the parameters (particularly the parameters related to time) of an antiphase arm swing restoring angular acceleration pattern.

5 Next, the height bzcurr of the trapezoid of the current time gait and the height bz1 of the trapezoid of the first turning gait are determined such that the right sides of Equations 1052 and 1053 become zero. In other words, bzcurr and bz1 are determined by solving the
10 simultaneous equation having the left sides of Equation 1052 and Equation 1053 set to zero.

 Lastly, the height of the trapezoid of the trapezoidal pattern of the antiphase arm swing restoring angular acceleration of the current time gait is set to
15 the height bzcurr of the trapezoid of the above determined current time gait.

 Returning to Fig. 13, after the current time gait parameters are corrected in S028 described above or if the determination result in S016 is NO, then the processing
20 proceeds to S030 to determine a current time gait instantaneous value.

 In S030, the subroutine processing shown in Fig. 45 is carried out.

 The same processing as that from S400 to S411 of Fig.
25 25 is carried out from S1400 to S1411 of Fig. 45, and then the processing from S1000 to S1018 of Fig. 46, which is a subroutine of S1412, is carried out.

To be specific, first, in S1000, the value of the reference body yaw angle at the current time is substituted into the desired body yaw angle. Further, the value of a reference arm posture at the current time is substituted into the desired arm posture, excluding the arm posture antiphase arm swing angle and the angular velocity.

Then, the processing proceeds to S1002 wherein it is determined whether the current time is in the period of restoring a body posture angle and an antiphase arm swing angle (the period from time T_a to time T_b). The processing proceeds to S1004 if the determination result of S1002 is NO, or to S1006 if the determination result is YES.

In S1004, the same processing as that for calculating the body horizontal acceleration α , the body angular acceleration β , and the antiphase arm swing angular acceleration β_a (from S504 to S528 of Fig. 26) in a period other than the body inclination angle/antiphase arm swing angle restoring period is carried out.

In the case where the processing proceeds to S1006, the body horizontal acceleration α_{tmp} , which is required to satisfy the current time (time k) desired ZMP if a motion of the body translational mode is to be performed, is determined in S1006.

Then, the processing proceeds to S1008 wherein the instantaneous value ZMP_{prec} of a body inclination restoring

moment ZMP-converted value pattern at the current time is calculated on the basis of the parameters related to the body inclination restoring moment ZMP-converted value pattern determined in S718.

5 The processing proceeds to S1010 wherein an instantaneous value β_{arec} of the antiphase arm swing restoring angular acceleration pattern at the current time is calculated on the basis of the parameters related to the antiphase arm swing restoring angular acceleration
10 pattern determined in S722.

Subsequently, the processing proceeds to S1012 wherein the body angular acceleration (body inclination angular acceleration) β of the body inclination mode is determined according to the equation shown in the figure.

15 Subsequently, the processing proceeds to S1014 wherein the body horizontal acceleration α is determined according to the equation shown in the figure.

Subsequently, the processing proceeds to S1016 wherein the sum of the instantaneous value β_{arec} of an
20 antiphase arm swing restoring angular acceleration pattern calculated in S1010 and a reference antiphase arm swing angular acceleration β_{aref} (a value obtained by subjecting a reference antiphase arm swing angle to second order differentiation) is substituted into a desired antiphase
25 arm swing angular acceleration β_a .

Subsequently, the processing proceeds to S1018 wherein a floor reaction force horizontal component F_x

when the body horizontal acceleration is α is determined.

Subsequently, the processing proceeds to S1414 wherein the body horizontal acceleration and the body posture angular acceleration are integrated to calculate a body horizontal velocity and a body posture angular velocity (body inclination angular velocity). The calculated result is further integrated to determine a horizontal body position and a body posture (the body inclination angle). A body yaw angle in the body posture is determined by a reference body yaw angle in the first reference example.

Subsequently, the processing proceeds to S1416 wherein the antiphase arm swing acceleration is integrated to calculate an antiphase arm swing angular velocity. The calculation result is further integrated to determine an antiphase arm swing angle.

Thus, the processing of S030 of Fig. 13 is completed.

Subsequently, the processing proceeds to S032 wherein time t for generating a gait is incremented by Δt , and returns to S014 to continue to generate gaits as described above.

The above is the processing for generating desired gaits in the gait generating device 100.

The operation of the gait generating device 100 according to the first reference example will be further explained with reference to Fig. 4. In the gait generating device 100, a desired gait is generated as

described above. In the generated desired gait, a desired body position posture (trajectory) and a desired arm posture (trajectory) are sent out to a robot geometric model (an inverse kinematics calculator) 102.

5 A desired foot position/posture (trajectory), a desired ZMP trajectory (desired total floor reaction force central point trajectory), and a desired total floor reaction force (trajectory) (a desired floor reaction force horizontal component and a desired floor reaction
10 force vertical component) are sent to a composite-compliance operation determiner 104 and also to a desired floor reaction force distributor 106. In the desired floor reaction force distributor 106, the floor reaction force is distributed to the feet 22R and 22L, and a
15 desired floor reaction force central point of each foot and a desired floor reaction force of each foot are determined. The determined desired floor reaction force central point of each foot and the desired floor reaction force of each foot are sent to the composite-compliance
20 operation determiner 104.

 A corrected desired foot position/posture (trajectory) with deformation compensation is sent from the composite-compliance operation determiner 104 to the robot geometric model 102. Upon receipt of the desired
25 body position/posture (trajectory) and the corrected desired foot position/posture (trajectory) with deformation compensation, the robot geometric model 102

calculates joint displacement commands (values) of twelve joints (10R(L), etc.) of the legs 2, 2 that satisfy them and sends the calculated commands to a displacement controller 108. The displacement controller 108 performs
5 follow-up control on the displacements of the twelve joints of the robot 1, using the joint displacement commands (values) calculated by the robot geometric model 102 as desired values. In addition, the robot geometric model 102 calculates arm joint displacement commands
10 (values) that satisfy the desired arm postures and sends the calculated commands to the displacement controller 108. The displacement controller 108 performs follow-up control on the displacements of the twelve joints of the arms of the robot 1, using the joint displacement commands
15 (values) calculated by the robot geometric model 102 as desired values.

A floor reaction force generated in the robot 1 (more specifically, an actual floor reaction force of each foot) is detected by a six-axis force sensor 50. The detected
20 value is sent to the composite-compliance operation determiner 104.

In the actual body posture angular error (the difference between the desired body posture and an actual body posture (the actual posture of the body 3)) occurring
25 in the robot 1, posture inclination angle errors θ_{errx} and θ_{erry} (specifically, the error of the inclination angle of an actual body posture relative to the vertical direction

with respect to the inclination angle of a desired body posture relative to the vertical direction, a posture inclination angle error in the roll direction (about the X-axis) being θ_{errx} , and a posture inclination angle error in the pitch direction (about the Y-axis) being θ_{erry} is detected via a posture sensor 54, and the detected value is sent to a posture inclination stabilization control calculator 112. The posture inclination stabilization control calculator 112 calculates the horizontal component of a compensating total floor reaction force moment about a desired total floor reaction force central point (desired ZMP) for restoring the actual body inclination angle of the robot 1 to the desired body posture angle, and sends it to the composite-compliance operation determiner 104.

More specifically, in the first reference example, a compensating total floor reaction force moment horizontal component M_{dmdxy} is determined according to the following equation by using, for example, PD control law:

Compensation total floor reaction force moment horizontal component M_{dmdxy}

$$\begin{aligned} &= K_{\theta b} * \text{Body posture inclination angle error} \\ &+ K_{\omega b} * \text{Body posture inclination angular velocity error} \end{aligned}$$

..... d25

where $K_{\theta b}$ and $K_{\omega b}$ are predetermined gains. The body posture inclination angular velocity error is a temporal

differential value of the body posture inclination angle error, and means an error of an actual body posture inclination angular velocity with respect to a desired body posture inclination angular velocity. The body posture inclination angle error is, more specifically, a vector composed of a posture inclination angle error of the body 3 of the robot 1 in the roll direction (about the X-axis) and a posture inclination angle error thereof in the pitch direction (about the Y-axis).

Furthermore, a yaw angle error θ_{errz} in the above actual body posture angle error occurring in the robot 1 (more specifically, the posture angle error in the yaw direction (about the Z-axis) in the actual body posture angle error is θ_{errz}) is detected through the intermediary of the posture sensor 54, and the detected value is sent to a yaw stabilization control calculator 113. The yaw stabilization control calculator 113 calculates the vertical component of the compensating total floor reaction force moment about a desired total floor reaction force central point (desired ZMP) for converging an actual body yaw angle and/or an angular velocity of the robot 1 to a desired body yaw angle and/or an angular velocity, and sends it to the composite-compliance operation determiner 104. The composite-compliance operation determiner 104 corrects the desired floor reaction force on the basis of the input value. Specifically, the desired floor reaction force is corrected such that the

compensating total floor reaction force moment acts about the desired total floor reaction force central point (desired ZMP).

More specifically, in the first reference example, a compensating total floor reaction force moment vertical component M_{dmdz} is determined according to the following equation by using, for example, the PD control law:

$$\begin{aligned} \text{Compensating total floor reaction force moment vertical} \\ \text{component } M_{dmdz} = K_{\theta bz} * \text{Body yaw angle error} \\ + K_{\omega bz} * \text{Body yaw angular velocity error} \end{aligned}$$

..... d26

where $K_{\theta bz}$ and $K_{\omega bz}$ are predetermined gains. The body yaw angular velocity error is a temporal differential value of the body yaw angle error, and means an error of an actual body yaw angular velocity with respect to a desired body yaw angular velocity.

Supplementally, when the compensating total floor reaction force moment vertical component M_{dmdz} is determined according to the Equation d26 given above, $K_{\theta bz}$ is set to zero if the purpose is merely to prevent a rotational slippage about the vertical axis or a vibration about the vertical axis between the feet 22 and a floor. This is because an attempt to approximate also the body yaw angle error to zero tends to cause an increase in an actual floor reaction force moment vertical component.

The composite-compliance operation determiner 104

corrects the desired floor reaction force on the basis of the input value. Specifically, the desired floor reaction force moment horizontal component is corrected such that the compensating total floor reaction force moment horizontal component acts about the desired total floor reaction force central point (desired ZMP). In addition, the desired floor reaction force moment vertical component is corrected by adding the compensating total floor reaction force moment vertical component to the desired floor reaction force vertical component about the desired total floor reaction force central point (desired ZMP) that dynamically balances with the desired gait.

The composite-compliance operation determiner 104 determines the aforesaid corrected desired foot position/posture (trajectory) with deformation compensation such that the state of the actual robot 1 and the floor reaction force calculated from sensor detection values or the like agree with the corrected desired floor reaction force. It is actually impossible, however, to make every state agree with a desired state, so that a trade-off relationship is established therebetween to make them compromisingly agree with each other as much as possible. More specifically, control errors with respect to desired values are weighted, and control is carried out to minimize the weighting average of control errors (or squares of control errors). With this arrangement, the control is conducted such that actual foot

position/posture and a total floor reaction force almost follow desired foot position/posture and a desired total floor reaction force.

5 The main point of the present invention is the generation of gaits of the robot 1 by the gait generating device 100, and the construction and operation of the composite-compliance operation determiner 104 or the like described above are disclosed in detail primarily in Japanese Unexamined Patent Application Publication No. 11-
10 300661 previously applied by the present applicant; therefore, no more explanation will be given.

 In S028, as previously discussed, the current time gait parameters are corrected such that a terminal divergent component of the current time gait agrees with
15 q'' , which is a value obtained by observing an initial divergent component $q[0]$ of a normal turning gait from the current time's gait supporting leg coordinate system.

 Actually, the divergent component is an indicator for
20 assessing whether the horizontal body position of a generated gait converges to a normal turning gait when the gait is generated on the basis of current time gait parameters by using a dynamic model and the gait is repeatedly generated in succession on the basis of normal
25 turning gait parameters. Basically, the divergent component must be defined so that a terminal divergent component of the current time gait agrees with q'' , which

is a value obtained by observing a normal turning initial divergent component $q [0]$ from the current time's gait supporting leg coordinate system at convergence.

5 The divergent component defined by Equation 10 is actually a divergent component that approximately satisfies the aforesaid properties.

Hence, in the first reference example, it may be said that the current time gait parameters have been corrected so that the horizontal body position of a generated gait converges (approximates) to the horizontal body position of a normal turning gait when the gait is generated on the basis of current time gait parameters by using a dynamic model and the gait is repeatedly generated in succession on the basis of normal turning gait parameters. Strictly speaking, however, only the first turning gait immediately following the current time gait must be a gait that has been corrected by the heights b_1 and b_{z1} of the trapezoid of the first turning gait determined as described above. In other words, it may be said that, in the present reference example, the current time gait parameters have been corrected so that the body posture angle of a generated gait converges (approximates) to or agrees with the body posture angle of a normal turning gait formed of a second turning gait and a first turning gait when the gait is repeatedly generated as described above if the gait combining the current time gait and the first turning gait is regarded as the current gait.

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This is the same as that disclosed in PCT publication of unexamined application WO/02/40224.

Especially in the first reference example, the desired ZMP pattern of the gait parameters of the current time gait has been corrected so as to satisfy the condition (the current time gait approximating to the normal gait). This will be explained with reference to Fig. 47. The trajectory indicated by reference mark B in the figure shows the horizontal body position trajectory generated so that divergent components agree at a gait boundary, as described above.

The trajectory indicated by reference mark A in the figure shows the horizontal body position trajectory obtained when a current time gait is generated so that horizontal body positions/velocities at boundaries of normal turning gaits agree, and then a normal gait is repeatedly generated.

As shown in the figure, the trajectory indicated by reference mark B generally deviates from the trajectory indicated by reference mark A at the boundary of the current time gait and a first normal turning gait. Thereafter, however, the trajectory indicated by reference mark B gradually converges to (approximates) the trajectory indicated by reference mark A and substantially agrees with the trajectory indicated by reference mark A in the next normal turning gait period. Thus, the gait generating technique for making only the divergent

components agree at a gait boundary also permits the prevention of gait divergence, as the gait generating technique for making both position and velocity agree at a gait boundary. The example indicated by reference mark C in the figure shows an example wherein a trajectory has been generated without considering them. In such a case, the generated trajectory diverges as time elapses. It is of course possible to complicate a desired ZMP pattern and a plurality of parameters is adjusted to make both position and velocity agree. This, however, may lead to a staggered desired ZMP pattern. Incidentally, if both position and velocity agree, then divergent components also agree, so that the method for making both position and velocity agree may be said to be a special example of the method for making divergent components agree.

Furthermore, in the first reference example, it may be said that the current time gait parameters have been corrected so that the body posture angle of a generated gait converges (approximates) to or agrees with the body posture angle of a normal turning gait when the gait is generated on the basis of current time gait parameters by using a dynamic model and the gait is repeatedly generated in succession on the basis of normal turning gait parameters. However, strictly speaking, only the first turning gait immediately following the current time gait must be a gait that has been corrected by the heights b_1 and b_{z1} of the trapezoid of the first turning gait

determined as described above.

A few modifications of the first reference example will be explained below.

In the first reference example, for easier
5 understanding, it has been arranged so that the floor
reaction force horizontal component permissible range can
be independently set for the longitudinal direction (X-
axis direction) component and the lateral direction (Y-
axis direction) component. More slippage-resistant gaits
10 are generated by representing it by a relational
expression of the longitudinal direction and the lateral
direction.

For instance, a so-called friction circle shown by
the following equation may be used as a permissible range.

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$$\begin{aligned} & (X \text{ component of floor reaction force horizontal component}) \\ & * (X \text{ component of floor reaction force horizontal} \\ & \text{component}) + (Y \text{ component of floor reaction force} \\ & \text{horizontal component}) * (Y \text{ component of floor reaction} \\ & 20 \text{ force horizontal component}) \leq (k_a * \mu * F_z) * (k_a * \mu * F_z) \\ & \qquad \qquad \qquad \dots \text{Equation 59} \end{aligned}$$

where F_z denotes a desired floor reaction force
vertical component, μ denotes a frictional coefficient,
and k_a denotes a positive constant of 1 or less.

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However, if the floor reaction force horizontal
component permissible range is represented by the
relational expression of the longitudinal direction and

the lateral direction, as described above, then it is necessary to simultaneously or alternately determine a motion on a sagittal plane and a motion on a lateral plane so as to simultaneously or alternately satisfy the permissible range.

A permissible range composed of a set of a floor reaction force horizontal component and a floor reaction force moment vertical component may be set instead of setting the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range separately, as described above. As the floor reaction force horizontal component increases, the friction limit of a floor reaction force moment vertical component diminishes. Further, as the floor reaction force moment vertical component increases, the friction limit of the floor reaction force horizontal component diminishes. Taking this into account, therefore, setting a permissible range composed of the set of a floor reaction force horizontal component and a floor reaction force moment vertical component makes it possible to set a permissible range that is closer to an actual friction limit characteristic. Specifically, a permissible range may be set for a weighted average of an absolute value of a floor reaction force horizontal component and an absolute value of a floor reaction force moment vertical component.

The sum of a total center-of-gravity vertical

acceleration of a robot and gravity acceleration is proportional to a floor reaction force vertical component. Hence, a parameter defining a total center-of-gravity vertical acceleration trajectory may be explicitly set in place of a floor reaction force vertical component trajectory, as a gait parameter. This is substantially the same. Alternatively, a parameter defining a vertical acceleration trajectory of a part having its behavior approximating to a total center-of-gravity trajectory of a robot may be explicitly. For instance, if the mass of a leg is sufficiently smaller than the mass of a body, then a body vertical acceleration trajectory and the total center-of-gravity vertical acceleration trajectory of a robot will be substantially identical or proportional; therefore, the body vertical acceleration trajectory may be used in place of a floor reaction force vertical component trajectory. Similarly, a floor reaction force horizontal component and a total center-of-gravity horizontal acceleration of a robot carry a proportional relationship, so that the total center-of-gravity horizontal acceleration of a robot and its permissible range may be used in place of the floor reaction force horizontal component and its permissible range in the first reference example. Further alternatively, a parameter related to the horizontal acceleration trajectory of a part whose behavior approximates to a total center-of-gravity horizontal trajectory of a robot

may be explicitly set. For instance, if the mass of a leg is sufficiently smaller than the mass of a body, then a body horizontal acceleration trajectory and the total center-of-gravity horizontal acceleration trajectory of a robot will be substantially identical or proportional; therefore, the body horizontal acceleration and its permissible range may be used in place of a floor reaction force horizontal component and its permissible range.

Further, the vertical component of a floor reaction force moment about a desired ZMP and the vertical component of an angular momentum changing rate of an entire robot carry a proportional relationship; therefore, the vertical component of the angular momentum changing rate of the entire robot and its permissible range may be used in place of the floor reaction force moment vertical component and its permissible range in the first reference example.

In the first reference example, two motion modes, namely, the body inclination mode and the body translational mode, have been used to obtain proper values for the floor reaction force horizontal component and the floor reaction force moment horizontal component about a desired ZMP; however, motion modes other than these may be used.

For example, as shown in Fig. 48, when the body posture is turned with the hip joints being as the turning center, the angular momentum about the total center of

gravity changes and the total center of gravity also changes. Overlapping (combining) this motion and the above-mentioned body translational mode at a predetermined ratio produces almost the same motion as that of the body inclination mode, and the floor reaction force horizontal component is no longer generated. Hence, if this is regarded again as the body inclination mode, then a similar gait can be generated according to the algorithm of the first reference example.

Thus, it is not required that one of the motion modes is a motion mode that does not produce a floor reaction force horizontal component. This is because any floor reaction force horizontal component and a floor reaction force moment about a desired ZMP can be generated as in the aforesaid example by any combination of modes as long as two motion modes having different generation ratios of a floor reaction force horizontal component and a floor reaction force moment about a desired ZMP are used.

A motion mode other than the motion mode that changes a body posture may be used. It is preferable, however, to select a motion mode that allows a large floor reaction force horizontal component or a floor reaction force moment about a desired ZMP to be generated in response to a minimized displacement.

For example, a motion mode for swinging the distal positions of right and left arms in the same direction, or a motion mode for perturbing the position of a foot not

in contact with the ground (existing in the air) may be selected. However, when perturbing a free leg trajectory, the amount of perturbation should be return to virtually zero by the time immediately before landing so that a landing position will not change. It is of course possible to combine the motion mode for swinging the distal positions of right and left arms in the same direction and an antiphase arm swing mode.

Further alternatively, three or more motion modes may be used.

In at least two of selected motion modes, the ratios of a floor reaction force horizontal component to a floor reaction force moment about a desired ZMP generated by the motion modes must be different from each other. Otherwise, there will be usually no solution of a simultaneous equation (the behavior of each motion mode cannot be uniquely determined).

In addition, it is preferred to combine, as much as possible, a motion mode that allows a sufficiently large change to take place in a floor reaction force moment about a desired ZMP while minimizing the change of a floor reaction force horizontal component, and a motion mode that allows a sufficiently large change to take place in a floor reaction horizontal component while minimizing the change of a floor reaction force moment about a desired ZMP.

In other words, it is desirable to combine a motion

mode that allows a sufficiently large change to take place in an angular momentum while minimizing the change of a total center of gravity, and a motion mode that allows a sufficiently large change to take place in a total center of gravity while minimizing the change of an angular momentum. This is because a displacement of a motion mode will be smaller.

Further, a body yaw rotation mode may be used in place of the antiphase arm swing mode to prevent a floor reaction force moment vertical component from exceeding a permissible range (to cancel a spinning force). When the body yaw rotation mode is used, it is preferred to divide the body 3 of the robot 1 into a part close to the waist (e.g., the part below a member 54 shown in Fig. 1) and the part above it (e.g., the part above the member 54) such that the upper part may turn in the yaw direction (e.g., about a trunk axis of the body 3) relative to the part close to the waist. This makes it possible to allow the upper part of the body 3 to rotate so as to adjust a floor reaction force moment vertical component without affecting the postures of the legs 2 and 2. In a first reference example in such a case, the rotational angle of the upper part of the body 3, the angular velocity thereof and the angular acceleration thereof may be determined instead of determining the antiphase arm swing angle, the angular velocity thereof, and the angular acceleration thereof in, for instance, the aforementioned first reference example.

In this case, the relative positions of the two arms 5 and 5 with respect to, for example, the upper part of the body 3 may be fixed. An antiphase arm swing operation of the two arms 5 and 5 may be of course added in addition to the yaw rotation of the upper part of the body 3.

Alternatively, a motion mode may be used that displaces a part other than the arms and the body as long as it generates a floor reaction force moment vertical component.

For example, a motion mode may be used that moves the distal ends of both legs in opposite longitudinal directions in a floating period.

Alternatively, a few motion modes generating a floor reaction force moment vertical component may be used at the same time. For example, the antiphase arm swing mode and the body yaw rotation mode may be used at the same time.

The body yaw rotation mode and the antiphase arm swing mode are the modes that generate a floor reaction force moment vertical component in such a manner that a total center-of-gravity position remains unchanged (in other words, without generating a floor reaction force horizontal component). However, motions causing a total center-of-gravity position to change (in other words, motions that generate floor reaction force horizontal components) may be also used. This is because the floor reaction force horizontal component can be adjusted by

combining these modes with the body translational mode.

In addition to the dynamic model used in the aforesaid first reference example (the dynamic model shown in Fig. 12), the following models may be used.

- 5 1) Non-linear model having mass points set at a plurality of links, as shown in Fig. 49 (multi-mass-point model). Inertia (inertial moment) may be set at each link of the model.
- 2) Three-mass-point model disclosed in PCT Kokai publication WO/02/40224 by the present applicant.
- 10 3) Model that ignores the moment of an inertial force generated by the body yaw rotation mode or the antiphase arm swing mode.
- 4) Separate type model that separately has a partial model
15 representing a relationship between a resultant force of gravity and an inertial force (or a floor reaction force balancing therewith) and a body translational motion, and a partial model representing the above resultant force and a body posture rotational motion (a body inclination
20 motion and a body yaw rotational motion). For instance, the mass points shown in Fig. 12 constitute a partial model representing the relationship between the above resultant force and the body translational motion, and the flywheels shown in Fig. 12 constitute a partial model
25 representing the relationship between the above resultant force and a body posture rotational motion.

Any one of 1) through 4) shown above requires a

motion mode that generates a moment vertical component of an inertial force.

The same model may be used for each processing or models may be properly used according to processing. For example, the aforementioned normal gait is generated merely to determine a terminal state of the current time gait, so that the dynamic accuracy required of the normal gait is lower than that required of the current time gait. Hence, for example, the processing for generating the current time gait may use the dynamic model shown in Fig. 12 (the model with 3 mass points + flywheels), while the processing for generating a normal gait (particularly S408 and S412 of Fig. 21) may generate a normal gait by using a dynamic model composed of a body mass point $3m$ corresponding to the body 3 and flywheels FH_x , FH_y , FH_{az} , and FH_{bz} (the model of one mass point + flywheels, which corresponds to the model of Fig. 12 from which leg mass points $2m$ and $2m$ have been removed), ignoring the mass of each leg 2. The processing for generating the normal gait in this case may carry out the processing of S408 and S412 of Fig. 25 with the mass of the leg mass point being set to zero in the aforesaid reference example. This makes it possible to dramatically reduce the calculation volume in the processing of generating normal gaits.

In the aforesaid first reference example, the block charts, the flowcharts, and algorithms or the like may be subject to equivalent modifications, including modified

calculation processing sequences. Furthermore, a low-pass filter may be inserted, as necessary.

Although the aforesaid first reference example has been explained in conjunction with the bipedal mobile robot; however, it may be applied also to multi-legged robots having three or more feet.

Instead of using the techniques for determining the initial state of a normal gait (primarily an initial horizontal body position/velocity, and initial vertical body position/velocity and antiphase arm swing angle and angular velocity) by using exploratory techniques or partially using analyzing techniques, as in the aforesaid first reference example, diverse normal gait parameters may be calculated using the above techniques beforehand and the relationship between the normal gait parameters and the initial states of the normal gait may be mapped or processed into an approximate expression and stored so as to determine the initial values of the normal gait on the basis of the relationship, which has been mapped or formed into approximate expressions, at the time of actual travel.

Further alternatively, a function that combines the aforesaid relationship, which has been mapped or processed into an approximate expression, and the aforesaid function f may be mapped or processed into an approximate expression and stored. More specifically, from the normal gait parameters composed of the aforesaid foot trajectory parameters, the floor reaction force vertical component

trajectory parameters, etc., the functions for directly determining the divergent components of normal gaits may be mapped or processed into approximate expressions and the results may be stored. For example, a normal gait may be generated in advance for each set of a plurality of types of typical normal gait parameters, the initial state of the normal gait for each set of normal gait parameters (to be determined in S024 of Fig. 13) may be determined beforehand, and a map that shows the relationship between the normal gait parameters of each set and the normal gait initial states may be prepared in advance. Then, when generating a desired gait, the initial state of a normal gait may be determined by selecting or interpolating from among the sets of the determined normal gait parameters on the basis of the aforesaid map. This arrangement obviates the need for generating a normal gait each time a current time gait is generated, thus permitting a significant reduction in the amount of calculation for the processing of generating a desired gait.

As the method for correcting a current time gait to connect (approximate) it to a normal gait, the desired ZMP parameter of the current time gait has been corrected in the first reference example. However, other parameters may alternatively be corrected.

For instance, the trajectory of a free leg in the air in a current time gait may be changed. If, for example, a horizontal body position is likely to shift farther to the

rear than a normal gait, then a free leg is promptly moved forward after it leaves a floor so as to shift the position of the center of gravity of the free leg toward the front. This causes the horizontal body position for satisfying a desired ZMP to be unavoidably further accelerated toward the front. As a result, the horizontal body position moves further forward at the end of the current time gait, making it possible to balance with the normal gait.

Instead of correcting a desired ZMP parameter, the cycle of a current time gait may be corrected. For instance, if the horizontal body position is likely to shift farther backward than a normal gait, then the cycle of the current time gait may be extended. Extending the cycle of the current time gait will extend the time for the horizontal body position to move, permitting extra forward movement to be accomplished accordingly.

However, if a desired ZMP parameter is corrected when determining an appropriate value of the horizontal body position or the like by an exploratory technique, the horizontal body position at the end of the current time gait changes substantially proportionally to a correction amount of the desired ZMP, so that the number of explorations of the appropriate value can be reduced. In comparison to this, correcting the center-of-gravity trajectory of a free leg or the cycle of a gait requires a greater number of explorations for the appropriate value,

because the horizontal body position at the end of the current time gait changes considerably nonlinearly in response to the correction.

5 In the first reference example, the desired ZMP parameter of the current time gait has been corrected, as the method for correcting the current time gait to connect (approximate) it to the normal gait. This method may lead to an excessive correction amount (correction amount a shown in Fig. 34) of the desired ZMP parameter in some cases. For instance, if a request for an abrupt
10 changeover from the gait of hopping at a spot to a high-speed travel (a request for running) is issued, then the desired ZMP parameter must be given an extremely large shift backward relative to an advancing direction in order to ensure connection (approximation) to a high-speed
15 normal gait (normal gait for running). In this case, as discussed above, gait parameters in addition to the desired ZMP parameter are preferably corrected. In this case, however, the request for such an abrupt acceleration
20 itself is actually unreasonable, so that a required value itself may be corrected.

To correct the required value, a normal gait satisfying the request (the required parameter), for example, is determined for the time being according to the
25 procedure shown in the first reference example, and at the point when a current time gait parameter has been determined so that it connects to the normal gait, it is

determined whether the safety margin for the desired ZMP trajectory of the current time gait has been unduly reduced. If the safety margin has reduced too much (if the desired ZMP has deviated from a so-called supporting polygon or the desired ZMP is positioned near an edge of the supporting polygon), then the request may be corrected.

Alternatively, the permissible range of acceleration/deceleration of a gait (Next time gait initial velocity - Current time gait initial velocity) / Cycle of current time gait) is set beforehand, and at the point when a request (a required parameter related to a gait cycle) is received, the acceleration/deceleration based on the request is determined, and if the determined acceleration/deceleration exceeds the permissible range, then the request may be corrected so that it falls within the permissible range.

Supplementally, if simple dynamic models as discussed above are used, the aforesaid ΔM_p , ΔF_p , ΔM_r , ΔF_r , ΔM_{az} , and ΔM_{bz} may be analytically determined by dynamic calculation; however, if a general, more complicated dynamic model is used, then they may be determined as follows. A floor reaction force in a case where the body 3 is accelerated by an extremely small amount by the body translational mode or accelerated by an extremely small amount by the body inclination mode is determined, and then the difference between this determined floor reaction force and the floor reaction force obtained in a case

where the body 3 is not accelerated is determined. Then, the difference is divided by the above extremely small amount.

Alternatively, the average value of each of ΔM_p , ΔF_p , ΔM_r , ΔF_r , ΔM_{az} , ΔM_{bz} , and $\Delta M_p/\Delta M_r$ or the like in standard gaits may be determined in advance and may be used. ΔM_p , ΔF_p , ΔM_r , ΔF_r , ΔM_{az} , ΔM_{bz} , and $\Delta M_p/\Delta M_r$ vary according to a state (a posture and its changing rate), so that the accuracy slightly deteriorates, as compared with a method in which they are determined for each state at each instant; however, the amount of calculation can be significantly reduced when models that are more complicated than the aforesaid models are used.

The following method may be used as the method for determining the height bz_{curr} of the trapezoid of the antiphase arm swing restoring angular acceleration pattern of the current time gait.

The antiphase arm swing angle and the angular velocity at the end of the current time gait of the aforesaid gait with a corrected antiphase arm swing restoring angular acceleration (refer to the explanation of S722 of Fig. 42) are denoted by θz_{curr} and $v\theta z_{curr}$, respectively, and the differences between these and the antiphase arm swing angle and the angular velocity of a normal gait are denoted by $\Delta\theta z_{cerr}$ and $\Delta v\theta z_{cerr}$.

A discrete type state equation may be set up, in which a gait cycle is defined as an interval, the

differences θ_{zerr} and $v\theta_{zerr}$ between the antiphase arm swing angle and the angular velocity at the end of a provisional current time gait and the initial antiphase arm swing angle and the angular velocity of a normal gait denote a last time's state, $bzcurr$ denotes an input, and $\Delta\theta_{zcerr}$ and $\Delta v\theta_{zcerr}$ denote a current state, and then a feedback rule may be determined using a modern control theory or the like so as to converge $\Delta\theta_{zcerr}$ and $\Delta v\theta_{zcerr}$ to zero. The determined feedback rule may be used to obtain $bzcurr$.

Based mainly on the difference between desired antiphase arm swing angle/angular velocity and reference antiphase arm swing angle/angular velocity at each instant, the value of the antiphase arm swing restoring angular acceleration β_{arec} at each instant may be determined by using a state feedback rule or the like so as to converge the above difference to zero rather than using a trapezoidal pattern to determine the antiphase arm swing restoring angular acceleration β_{arec} of a current time gait and/or a normal gait.

Based on desired antiphase arm swing angle/angular velocity of a current time gait at each instant, the antiphase arm swing restoring angular acceleration β_{arec} at each instant may be determined by using a state feedback rule or the like such that these will approximate initial antiphase arm swing angle/angular velocity of a first turning gait rather than using a trapezoidal pattern

to determine the antiphase arm swing restoring angular acceleration β_{arec} of a current time gait and/or a normal gait.

To generate a gait for traveling on a slope (when
5 moving the robot 1 on a slant floor surface), the
permissible range of the floor surface horizontal
component of a translational floor reaction force (a
component parallel to the floor surface), that is, the
permissible range of fictional force, or the permissible
10 range of the floor surface horizontal component of a total
center-of-gravity acceleration (this is proportionate to a
frictional force) may be set in place of a floor reaction
force horizontal component permissible range or a total
center-of-gravity acceleration horizontal component
15 permissible range. A case, for example, where the
permissible range of the floor surface horizontal
component (frictional force) of a translational floor
reaction force will be explained (this explanation applies
also to a case where the permissible range of a floor
20 surface horizontal component of total center-of-gravity
acceleration is set). The frictional force is determined
according to Equation 72 shown below if an inclination
angle relative to the horizontal plane of a floor surface
is defined as θ_f (a slope down forward in the direction in
25 which the robot 1 advances is defined as a positive slope).
Therefore, to generate a gait according to the same
algorithm as that in the aforesaid first reference example,

the Equation 72 may be used to convert a frictional force permissible range into a floor reaction force horizontal component permissible range thereby to set the floor reaction force horizontal component permissible range. In this case, a desired floor reaction force vertical component may be used as the floor reaction force vertical component of Equation 72.

$$\begin{aligned} \text{Frictional force} &= \text{Floor reaction force horizontal} \\ &\text{component} * \cos(\theta_f) - \text{Floor reaction force vertical} \\ &\text{component} * \sin(\theta_f) \quad \dots \text{Equation 72} \end{aligned}$$

When generating a gait for traveling on a slope (when moving the robot 1 on an inclined floor surface), a floor reaction force moment vertical component can be converted into a moment in the direction of the normal line of a floor surface frictional force by Equation 1072, so that the permissible range of the component in a floor surface normal line of a floor reaction force moment, i.e., the permissible range of the moment in the direction of the normal line of a floor surface frictional force, may be set in place of the permissible range of a floor reaction force moment vertical component.

$$\begin{aligned} \text{Moment in the direction of the normal line of floor} \\ \text{surface frictional force} &= \text{Vertical component of floor} \\ \text{reaction force moment} * \cos(\theta_f) \quad \dots \text{Equation 1072} \end{aligned}$$

The parameters of a current time gait may be re-determined in the middle of the generation of a current gait, as disclosed in PCT Kokai publication WO/02/40224 by the present applicant, instead of determining them when a preceding gait is completed, as in the aforesaid first reference example. This allows an immediate response to be taken if a gait request changes, although it involves an increased calculation volume.

If correction of a gait (re-determination of a current time gait parameter) is not completed within a current control cycle, then an uncorrected gait or provisionally corrected gait (a gait in the middle of exploration, i.e., a gait that does not fully satisfy an exploration completion condition (a deviation of a gait boundary condition being less than a permissible value)) is tentatively output, and a properly corrected (non-provisional) gait may be output by the next control cycle or by a plurality of control cycles later. The corrected desired ZMP trajectory and desired floor reaction force vertical component trajectory are connected, and these do not suddenly change in a short time; therefore, the desired ZMP trajectory and the desired floor reaction force vertical component trajectory of the current time gait will hardly present a problem although they will be slightly staggered.

The aforesaid first reference example has explained

the example of the case where the running gait shown in Fig. 5 is generated; however, a desired gait can be generated in the same manner as that in the aforesaid first reference example when a walking gait of the robot 1 is generated. In this case, in the aforesaid first reference example, for instance, a desired floor reaction force vertical component may be set according to the pattern shown in, for example, Fig. 50 in place of the one shown in Fig. 6 mentioned above. In this example, a floor reaction force vertical component trajectory is set to exhibit a trapezoidal shape projecting to an increasing side of the floor reaction force vertical component in a double stance period, and to exhibit a trapezoidal shape projecting to a decreasing side of the floor reaction force vertical component in a single stance period. The details of the method for setting heights C1 and C2 of the trapezoidal portions, and others are explained in detail in, for example, PCT Kokai publication WO/03/057425/A1 by the present applicant. Hence, the explanation will be omitted.

A second reference example will now be explained with reference to Fig. 53 through Fig. 58 on the basis of the first reference example and the modifications thereof explained above. In the explanation of the second reference example, like constituent parts or like functional parts as those in the aforesaid first reference

example will be assigned like reference numerals as those in the aforesaid first reference example, and the explanation thereof will be omitted. Especially in the second reference example, the aspects explained with reference to Fig. 1 to Fig. 3 and Fig. 5 to Fig. 12 are identical to those in the aforesaid first reference example.

An outline of the aspects of the second reference example that are different from those of the aforesaid first reference example will be explained. In the second reference example, a desired gait is corrected in addition to manipulating a desired floor reaction force for compliance control in order to approximate an actual body posture angle error, which is the difference between a desired body posture angle and an actual body posture angle (an error of an inclination angle and an error of a yaw angle with respect to the vertical direction of the body 3), and/or the changing rate thereof to zero. In particular, the vertical component of a floor reaction force moment about a desired ZMP that dynamically balances with a desired gait (the resultant force of the inertial force and gravity of a motion of a desired gait balances with the vertical component of a moment generated about the desired ZMP) is also corrected on the basis of a yaw angle component and/or its angular velocity out of an actual body posture error.

A block diagram showing the functional construction

of a control unit 60 in the second reference example is shown in Fig. 53. The following will explain the aspects of the functional construction of the control unit 60 in the second reference example that are different from those of the aforesaid first reference example (those shown in Fig. 4).

In the second reference example, the compensating total floor reaction force moment horizontal component M_{dmdxy} calculated in a posture inclination stabilization control calculator 112 is supplied to a compensating total floor reaction force moment horizontal component distributor 110. The compensating total floor reaction force moment horizontal component distributor 110 divides the compensating total floor reaction force moment horizontal component M_{dmdxy} into a desired floor reaction force moment horizontal component for compliance control and a model manipulation floor reaction force moment horizontal component. In other words, based on an actual body posture inclination angle error, the desired floor reaction force moment horizontal component for compliance control and a model manipulation floor reaction force moment horizontal component are determined by the posture inclination stabilization control calculator 112 and the compensating total floor reaction force moment horizontal component distributor 110.

Specifically, in the compensating total floor reaction force moment horizontal component distributor 110,

a model manipulation floor reaction force moment horizontal component is determined first according to the equation given below. Incidentally, a permissible range of the floor reaction force moment horizontal component is determined in the gait generating device 100, as will be discussed hereinafter.

If $M_{dmdxy} >$ Upper limit value of the permissible range of a floor reaction force moment horizontal component, then

Model manipulation floor reaction force moment horizontal component = $-M_{dmdxy} +$ Upper limit value of the permissible range of a floor reaction force moment horizontal component.

If $M_{dmdxy} <$ Lower limit value of the permissible range of a floor reaction force moment horizontal component, then

Model manipulation floor reaction force moment horizontal component = $-M_{dmdxy} +$ Lower limit value of the permissible range of a floor reaction force moment horizontal component

If the lower limit value of the permissible range of a floor reaction force moment horizontal component $\leq M_{dmdxy}$, and $M_{dmdxy} \leq$ the upper limit value of the permissible range of a floor reaction force moment horizontal component, then

Model manipulation floor reaction force moment horizontal component = 0

..... Equation d27a

Then, a desired floor reaction force moment horizontal component for compliance control is determined according to the following equation.

5 Desired floor reaction force moment horizontal component for compliance control
 = M_{dmdxy} + Model manipulation floor reaction force moment horizontal component

..... Equation d27b

10 Accordingly, the floor reaction force moment horizontal components are determined such that the difference between the desired floor reaction force moment horizontal component for compliance control and the model manipulation floor reaction force moment horizontal
15 component is equal to M_{dmdxy} .

A block diagram of the compensating total floor reaction force moment horizontal component distributor 110 that performs the aforesaid calculations is shown in Fig. 54.

20 The compensating total floor reaction force moment vertical component M_{dmdz} determined in the same manner as that in the afore-mentioned first reference example in the yaw stabilization control calculator 113 (refer to the aforesaid Equation d26) is supplied to a model
25 manipulation floor reaction force moment vertical component determiner 111. The model manipulation floor reaction force moment vertical component determiner 111

determines a model manipulation floor reaction force moment vertical component on the basis of the compensating total floor reaction force moment vertical component M_{dmdz} . In other words, the compensating total floor reaction force moment vertical component M_{dmdz} and the model manipulation floor reaction force moment vertical component are determined on the basis of a body yaw angle error out of an actual body posture angle error by the yaw stabilization control calculator 113 and the model manipulation floor reaction force moment vertical component determiner 111.

Specifically, in the model manipulation floor reaction force moment vertical component determiner 111, a model manipulation floor reaction force moment vertical component is determined according to the equation given below. Incidentally, the permissible range of the floor reaction force moment vertical component compensation amount is determined in the gait generating device 100, as will be discussed hereinafter.

If $M_{dmdz} >$ Upper limit value of the permissible range of a floor reaction force moment vertical component compensation amount, then

Model manipulation floor reaction force moment vertical component = $-M_{dmdz} +$ Upper limit value of the permissible range of a floor reaction force moment vertical component compensation amount.

If $M_{dmdz} <$ Lower limit value of the permissible range

of a floor reaction force moment vertical component compensation amount, then

Model manipulation floor reaction force moment vertical component = $-M_{dmdz}$ + Lower limit value of the permissible range of a floor reaction force moment vertical component compensation amount.

If the lower limit value of the permissible range of a floor reaction force moment vertical component compensation amount $\leq M_{dmdz}$, and $M_{dmdz} \leq$ the upper limit value of the permissible range of a floor reaction force moment vertical component compensation amount, then

Model manipulation floor reaction force moment vertical component = 0

..... Equation d26b

A block diagram of the model manipulation floor reaction force moment vertical component determiner 111 that performs the aforesaid calculations is shown in Fig. 55. Thus, the model manipulation floor reaction force moment vertical component is set to the portion of the compensating total floor reaction force moment vertical component M_{dmdz} that has deviated from the permissible range of the floor reaction force moment vertical component compensation amount, the sign of the portion being reversed.

The desired floor reaction force moment horizontal component for compliance control and the compensating total floor reaction force moment vertical component M_{dmdz}

are sent to the composite-compliance operation determiner 104.

5 The model manipulation floor reaction force moment horizontal component and vertical component are sent to the gait generating device 100.

10 In place of the compensating total floor reaction force moment vertical component M_{dmdz} , the sum of the compensating total floor reaction force moment vertical component M_{dmdz} and the model manipulation floor reaction force moment vertical component may be sent as a desired value for compliance control to the composite-compliance operation determiner 104.

15 The composite-compliance operation determiner 104 corrects the desired foot position/posture such that an actual floor reaction force approximates the desired total floor reaction force corrected by adding a desired floor reaction force moment horizontal component for compliance control and the compensating total floor reaction force moment vertical component M_{dmdz} to a desired total floor reaction force generated by the gait generating device 100, while making the motion of the robot 1 follow the motion of a desired gait generated by the gait generating device 100, thereby determining a corrected desired foot position/posture (trajectory) with deformation
25 compensation.

In this case, it is actually impossible to make every state of foot position/posture of the robot 1 and floor

reaction force agree with a target, so that a trade-off relationship is provided between them to reach compromisingly closest possible agreement, as in the aforesaid first reference example.

5 Although it will be discussed in more detail hereinafter, the gait generating device 100 generates the motion of a desired gait (particularly a body position/posture trajectory) by using a dynamic model so that the floor reaction force moment horizontal component
10 about the desired ZMP determined by the gait generating device 100 becomes a model manipulation floor reaction force moment horizontal component. Furthermore, the gait generating device 100 corrects the motion of the desired gait (particularly an arm swing trajectory) such that a
15 model manipulation floor reaction force moment vertical component is additionally generated in the desired floor reaction force moment vertical component about the desired total floor reaction force central point (the desired ZMP) that dynamically balances with the desired gait
20 (provisional desired gait) generated, assuming the model manipulation floor reaction force moment is zero.

 The functional construction of the control unit 60 other than the above is identical to that of the aforesaid first reference example. Supplementally, the desired gait
25 generated in the aforesaid first reference example is identical to the desired gait generated when the model manipulation floor reaction force moment horizontal

component and the model manipulation floor reaction force moment vertical component are steadily set to zero in the second reference example.

5 An operation (processing for generating a gait) of the gait generating device 100 in the second reference example will be explained in detail below in conjunction with Fig. 56 showing its main flowchart. From S3010 to S3028, the same processing as that from S010 to S028 shown in Fig. 13 of the aforesaid first reference example is
10 carried out.

 Subsequently, the processing proceeds to S3030 wherein the parameters defining the permissible ranges of the floor reaction force moment horizontal component about a desired ZMP for compliance control and a floor reaction
15 force moment vertical component compensation amount are determined.

 A value obtained by dividing the floor reaction force moment horizontal component by the floor reaction force vertical component represents the amount of deviation of a
20 ZMP (the central point of a floor reaction force) from a desired ZMP. Alternatively, therefore, the permissible range of a floor reaction force moment horizontal component may be divided by a floor reaction force vertical component to set the parameter of the ZMP
25 permissible range converted into a floor reaction force central point (the permissible range of a floor reaction force central point).

Supplementally, based on the parameters of the permissible range of a floor reaction force moment horizontal component for compliance control and the permissible range of a floor reaction force moment vertical component compensation amount that are determined in S3030, the instantaneous values of the permissible ranges will be determined in a subroutine for determining a current time gait instantaneous value (the subroutine of S3032), which will be discussed hereinafter, and the determined instantaneous values are used for the aforesaid processing in the aforesaid compensating total floor reaction force moment horizontal component distributor 110 and model manipulation floor reaction force moment vertical component determiner 111.

Regarding the floor reaction force moment horizontal component permissible range, a method for setting a floor reaction force moment permissible range is described in detail in PCT application PCT/JP03/00435 by the present applicant. Hence, no further explanation will be given in the present description.

The floor reaction force moment vertical component compensation amount means the compensation amount of a floor reaction force moment vertical component that can be added to the floor reaction force moment generated by a motion of a desired gait if the desired gait with a floor reaction force moment vertical component limited to a floor reaction force moment vertical component permissible

range (this is set in S3026) for generating a gait is supposedly generated in the gait generating device 100. Hence, the permissible range of a floor reaction force moment vertical component compensation amount cannot be widely set unless the floor reaction force moment vertical component permissible range for generating a gait is set to be sufficiently narrower than an actual friction limit.

The permissible range of a floor reaction force moment vertical component compensation amount may be set to be similar to the floor reaction force moment vertical component permissible range for generating a gait (refer to the aforesaid Fig. 41). For a floating period of the running gait shown in the aforesaid Fig. 5, the permissible range of a floor reaction force moment vertical component compensation amount for compliance control is set to a range having an upper limit value of zero and a lower limit value of zero.

Returning to Fig. 56, after the parameters defining the permissible ranges of the floor reaction force moment horizontal component about the desired ZMP for compliance control and the permissible range of the floor reaction force moment vertical component compensation amount are determined in S3030 as described above, or if the determination result of S3016 is NO, then the processing proceeds to S3032 wherein a current time gait instantaneous value is determined. In S3032, a current time gait instantaneous value is determined such that a

model manipulation floor reaction force moment horizontal
component determined according to the above Equation d27a
is generated about the desired ZMP. However, the current
time gait instantaneous value is determined such that the
5 floor reaction force moment vertical component that
balances with the current time gait (the resultant force
of the inertial force and gravity of a motion of the
current time gait balances with the vertical component of
an inertial force moment generated about the desired ZMP)
10 does not exceed the permissible range of the floor
reaction force moment vertical component.

Specifically, gait instantaneous values are
determined according to the flowcharts shown in Fig. 57
and Fig. 58. More specifically, in S3030, the processing
15 from S3400 to S3411 of Fig. 57 is executed. The
processing from S3400 to S3411 is exactly the same as that
from S1400 to S1411 of Fig. 45 mentioned above.

Then, the processing proceeds to S3412 wherein the
instantaneous values (the current time values at the
20 current time t) of the floor reaction force moment
horizontal component permissible range $[M_{xymin}, M_{xymax}]$
and a floor reaction force moment vertical component
compensation amount permissible range $[M_{zcmin}, M_{zcmax}]$ at
the current time are determined on the basis of the
25 parameters of the floor reaction force moment horizontal
component permissible range for compliance control and the
floor reaction force moment vertical component

compensation amount permissible range that have been determined in S3030 of the aforesaid Fig. 56.

The determined floor reaction force moment horizontal component permissible range is sent to the compensating total floor reaction force moment horizontal component distributor 110 (refer to Fig. 53). Then, the current time value (the value at the current time t) of the model manipulation floor reaction force moment calculated according to the above Equation d27a by the distributor 110 is supplied to the gait generating device 100.

The determined permissible range of the floor reaction force moment vertical component compensation amount is supplied to the aforesaid model manipulation floor reaction force moment vertical component determiner 111 (refer to Fig. 53). The current time value (the value at the current time t) of the model manipulation floor reaction force moment vertical component calculated according to the aforesaid Equation d26b by the model manipulation floor reaction force moment vertical component determiner 111 is supplied to the gait generating device 100.

Subsequently, the processing of the gait generating device 100 proceeds to S3414 wherein the body horizontal acceleration and the body posture inclination angular acceleration of the current time gait are determined so that the model manipulation floor reaction force moment horizontal component supplied from the compensating total

floor reaction force moment distributor 110 is generated about the desired ZMP. However, the body horizontal acceleration and the body posture angular acceleration (the body inclination angular acceleration) are determined such that the floor reaction force horizontal component F_x does not exceed the floor reaction force horizontal component permissible range $[F_{xmin}, F_{xmax}]$ determined in S3410.

In other words, the body horizontal acceleration and the body posture angular acceleration (the body inclination angular acceleration) of the current time gait are determined so that the moment horizontal component generated about the desired ZMP by the resultant force of the inertial force and the gravity of a motion of the robot 1 will be the moment with a reversed sign of the model manipulation floor reaction force moment horizontal component. However, the body horizontal acceleration and the body posture inclination angular acceleration are determined such that the force with the reversed sign of the horizontal component of the inertial force does not exceed the floor reaction force horizontal component permissible range $[F_{xmin}, F_{xmax}]$.

In S3414, specifically, the body horizontal acceleration and the body posture angular acceleration are determined according to the flowchart shown in Fig. 58. In this flowchart, the same processing as that shown in the aforesaid Fig. 26 is performed except for S3104 and

S3130. Unlike S504 and S530 of Fig. 26, S3104 and S3130 determine a body horizontal acceleration (α_{tmp} in S3104 or α in S3130) required for the aforesaid model manipulation floor reaction force moment horizontal component to be
5 generated about the desired ZMP of the current time (time k) in a case where the robot 1 is made to perform a motion of the body translational mode, setting the angular acceleration of the body inclination mode to zero (to be more precise, balancing the angular acceleration of the
10 body inclination mode with a reference body posture angular acceleration) from the last time's instant gait state (the gait state at time $k-1$) of the robot 1.

The rest of the processing is the same as the processing shown in Fig. 26.

15 Thus, after the processing of S3414 is completed, the processing proceeds to S3416, wherein the same processing as that of S1414 of Fig. 45 is carried out to determine the horizontal body position and the body posture inclination angle (specifically, the current time values
20 thereof at the current time t).

Subsequently, the processing proceeds to S3418 wherein the same processing as that of S1416 of Fig. 45 is carried out to determine an antiphase arm swing angle and angular velocity of the current time gait (specifically,
25 the current time values thereof at the current time t).

Thus, the processing of S3032 of Fig. 56 is completed.

Then, the processing proceeds to S3034 of Fig. 56 to

correct the current time gait instantaneous value
generated in S3032 so as to additionally generate a model
manipulation floor reaction force moment vertical
component about the desired ZMP.

5 Specifically, a correction amount β_{aadd} of an
antiphase arm swing angular acceleration corresponding to
the model manipulation floor reaction force moment
vertical component is determined according to the
following equation.

10

Correction amount β_{aadd} of antiphase arm swing angular
acceleration = Model manipulation floor reaction force
moment vertical component / Equivalent inertial moment
 ΔM_{az} of antiphase arm swing motion

15

Further, β_{aadd} is integrated during the period of a
control cycle to determine a correction amount of the
antiphase arm swing angular velocity, and then this is
integrated to determine a correction amount of the
20 antiphase arm swing angle.

20

Lastly, the correction amount of the antiphase arm
swing angle and the correction amount of the antiphase arm
swing angular velocity are added to the antiphase arm
swing angle and the angular velocity, respectively, of the
25 current time gait generated in S3032, thereby correcting
the antiphase arm swing angle and the angular velocity of
the current time gait.

25

Subsequently, the processing proceeds to S3036 to add the control cycle Δt to time t , and goes back to S3014 to wait for a timer interrupt for each control cycle.

5 In the second reference example, as described above, the processing for generating a desired gait is carried out in the gait generating device 100, and instantaneous values of a desired body position/posture, a desired foot position/posture, a desired arm posture (including an antiphase arm swing angle), a desired ZMP, and a desired
10 total floor reaction force are determined and output sequentially.

In this case, regarding the desired total floor reaction force, only a component thereof that is necessary for compliance control may be output. The desired ZMP is
15 deliberately listed here as an output although it is included in the desired total floor reaction force, because it is particularly important. The model manipulation floor reaction force moment horizontal component is not output as a desired floor reaction force
20 to the composite-compliance operation determiner (the portion encircled by a dashed line in Fig. 53). More specifically, for the compliance control, the desired floor reaction force aimed at a zero floor reaction force moment horizontal component about the desired ZMP (the
25 desired floor reaction force satisfying the desired ZMP in the original meaning) is output from the gait generating device 100.

The floor reaction force moment vertical component of the current time gait that has been corrected in S3034 is output as a desired value from the gait generating device 100 to the composite-compliance control unit.

5 As a first action of the second reference example, a motion of a desired gait is generated such that a model manipulation floor reaction force moment horizontal component is produced about a desired ZMP, while the floor reaction force of the actual robot 1 is controlled so as
10 to prevent the model manipulation floor reaction force moment horizontal component from being added. Hence, there is an imbalance (unbalance) between the motion of the desired gait and the floor reaction force by the differential portion of the model manipulation floor
15 reaction force moment horizontal component. This is equivalent to applying a floor reaction force moment horizontal component, which has a sign reversed from the sign of the model manipulation floor reaction force moment horizontal component, to the actual robot 1 from the
20 aspect of the effect for converging a difference between the body posture inclination angle of the actual robot 1 and the body posture inclination angle of a desired gait.

 In other words, the actual robot 1 can be converged to a corrected desired gait (the gait for converging the
25 difference between the body posture inclination angle of the actual robot 1 and the body posture inclination angle of a desired gait) by determining a model manipulation

floor reaction force moment horizontal component as appropriate. This means that the posture inclination of the actual robot 1 can be stabilized.

As a second action, the sum of a moment with a
5 reversed sign of a model manipulation floor reaction force moment horizontal component and a desired floor reaction force moment horizontal component for compliance control provides a total inclination restoring force (a force for restoring an actual body posture inclination angle of the
10 robot 1 to a desired body posture inclination angle). This means that the difference between a desired floor reaction force moment horizontal component for compliance control and a model manipulation floor reaction force moment horizontal component provides a total posture
15 inclination restoring force.

As a third action, a model manipulation floor reaction force moment horizontal component can take any value, ignoring the range in which a ZMP can exist, thus making it possible to generate an extremely high posture
20 inclination restoring force.

As a fourth action, a body translational acceleration of the body translational mode and a body posture inclination angular acceleration of the body inclination mode are determined such that a floor reaction force
25 horizontal component does not exceed a floor reaction force horizontal component permissible range. This makes it possible to prevent slippage of the robot 1 even in a

period wherein a large floor reaction force horizontal component cannot be generated, such as immediately before a supporting leg 2 leaves a floor or immediately after it lands on a floor in a running gait, or when the robot 1 travels on a floor with a small frictional coefficient.

As a fifth action, the permissible range of a floor reaction force horizontal component is set to zero in the period wherein the translational force vertical component of a floor reaction force is zero, that is, in the period wherein neither of the legs is in contact with the ground, so that a posture inclination is automatically restored by depending upon the body inclination mode rather than depending upon the body translational mode according to the algorithm of the second reference example discussed above, thus performing the posture restoration without depending upon a frictional force between a floor and a sole. Accordingly, even in this period (floating period), the posture inclination restoring action effectively works, unlike the method wherein only the body translational mode is merely corrected. Incidentally, at this time, the gait is generated so that the floor reaction force horizontal component becomes zero; therefore, the total center-of-gravity horizontal acceleration of the gait will be zero.

Further, as a sixth action, a model manipulation floor reaction force moment horizontal component is not output as a desired floor reaction force for compliance control, as described above. More specifically, even when

a gait is generated to produce a model manipulation floor reaction force moment horizontal component about a desired ZMP, a desired floor reaction force intended for setting a floor reaction force moment horizontal component about the
5 desired ZMP to zero for compliance control is supplied from the gait generating device 100. Thus, the floor reaction force control by the compliance control will not be interfered with, allowing the floor reaction force control to be properly conducted by compliance control.

10 To be more specific, it is possible to prevent or restrain the occurrence of a problem, such as one in that an originally designed property of a foot 22 to contact the ground is deteriorated, or the sole of a foot 22 incompletely contacts the ground.

15 As it will be discussed hereinafter, a desired floor reaction force moment horizontal component for compliance control about a desired ZMP will be determined so as not to exceed a floor reaction force moment horizontal component permissible range also in the first embodiment
20 and after.

Incidentally, the first to the sixth actions are the same arts disclosed in PCT/JP03/00435 previously proposed by the present applicant.

25 As a seventh action, a motion of a desired gait is generated such that a model manipulation floor reaction force moment vertical component is additionally produced about a desired ZMP, and the actual floor reaction force

of the actual robot 1 is controlled by composite-compliance control to approximate to a desired value, the desired value being obtained by adding the compensating total floor reaction force moment vertical component M_{dmdz} to a desired floor reaction force moment vertical component that balances with the desired gait to which a model manipulation floor reaction force moment vertical component has been added by the gait generating device 100. As M_{dmdz} increases, a model manipulation floor reaction force moment vertical component in the opposite direction from M_{dmdz} is added to the desired gait. Hence, even when the actual floor reaction force is controlled to approximate it to the aforesaid desired value by the composite-compliance control, the vertical component of the moment of the actual floor reaction force will not be excessive. As a result, the effect can be implemented in which the difference between the body posture yaw angle and/or the body posture yaw angular velocity of the actual robot 1 and the body posture yaw angle and/or the yaw angular velocity of a desired gait is converged to zero without causing the actual robot 1 to spin.

In other words, appropriately determining the model manipulation floor reaction force moment vertical component makes it possible to converge the actual robot 1 to the corrected desired gait (the gait that converges the difference between the body posture yaw angle and/or the body posture yaw angular velocity of the actual robot 1

and the body posture yaw angle and/or the yaw angular velocity of the desired gait to zero), while preventing the actual robot 1 from spinning. This means that the yaw rotation of the actual robot 1 can be stabilized.

5 As an eighth action, the compensating total floor reaction force moment vertical component M_{dmdz} provides a total yaw rotation restoring force. The compensating total floor reaction force moment vertical component M_{dmdz} is determined according to a feedback control law so as to
10 approximate a yaw angle error and/or a yaw angular velocity error to zero, thus making it possible to approximate the yaw angle error and/or a yaw angular velocity error to zero while ensuring control stability of yaw angle errors.

15 As a ninth action, a model manipulation floor reaction force moment vertical component may take any value, ignoring the permissible range (or the frictional limit) of the floor reaction force moment vertical component, so that an extremely high posture yaw rotation
20 restoring force can be generated.

 As a tenth action, a final desired floor reaction force moment vertical component is determined for compliance control such that it does not exceed the sum of the permissible range of a floor reaction force moment
25 vertical component and the permissible range of a floor reaction force moment vertical component compensating amount. This makes it possible to properly conduct the

floor reaction force control based on the compliance control and therefore makes it possible to prevent the robot 1 from spinning even in a period wherein a large floor reaction force moment vertical component cannot be generated, such as immediately before a supporting leg 2 leaves a floor or immediately after it lands on a floor in a running gait, or when the robot 1 travels on a floor with a small frictional coefficient. To be more specific, it is possible to prevent or restrain the occurrence of a problem, such as one in that an originally designed property of a foot 22 to contact the ground is deteriorated, or the sole of a foot 22 incompletely comes in contact with the ground.

As an eleventh action, the permissible range of a floor reaction force vertical component and the permissible range of a floor reaction force moment vertical component compensation amount are set to zero in the period wherein the translational force vertical component of a floor reaction force is zero, that is, in the period wherein neither of the legs is in contact with the ground, so that yaw rotation is automatically restored by depending upon the antiphase arm swing mode rather than depending on an actual floor reaction force moment vertical component according to the algorithm of the second reference example discussed above, thus performing the restoration of yaw rotation without depending upon a frictional force between a floor and a sole. Accordingly,

even in this period (floating period), the yaw rotation restoring action effectively works, unlike the method wherein only the desired floor reaction force moment vertical component for compliance control is merely
5 corrected.

As a twelfth action, if a gait generated such that the moment horizontal component produced about a desired ZMP is zero is referred to as an original gait, and a gait generated such that the moment horizontal component
10 produced about a desired ZMP provides a model manipulation floor reaction force moment horizontal component and a model manipulation floor reaction force moment vertical component is additionally produced in the moment vertical component produced about the desired ZMP, as in the
15 aforesaid second reference example, is referred to as a corrected gait, then the original gait and the corrected gait are usually different gaits. The original gait is set so that it gradually approximates to a normal gait, and therefore, the corrected gait is usually a gait that
20 does not gradually approximate to a normal gait.

However, immediately following the completion of the generation of a current time gait (corrected gait), the processing from S3020 to S3028 is carried out again to determine new current time gait parameters such that a new
25 current time gait having a terminal state of the corrected gait as its new initial state gradually approximates a normal gait newly set. This makes it possible to continue

generating gaits with continuously (long-range) guaranteed stability.

The twelfth action described above is substantially the same art as that previously proposed in PCT/JP03/00435 by the present applicant. In addition thereto, however, the second reference example provides the following action. The parameters related to an antiphase arm swing angle trajectory of a new current time gait are determined such that the antiphase arm swing angle trajectory of the new current time gait, which uses the terminal state of the antiphase arm swing angle and angular velocity corrected to restore the yaw angle rotation as the new initial state, gradually approximates to the antiphase arm swing angle trajectory of the normal gait that is newly set. This makes it possible to continue generating gaits with continuously (long-range) guaranteed stability of the antiphase arm swing angle.

In the second reference example, if the compensating total floor reaction force moment horizontal component M_{dmdxy} takes a value within a floor reaction force moment horizontal component permissible range, then the model manipulation floor reaction force moment horizontal component will be zero. Alternatively, however, the model manipulation floor reaction force moment horizontal component at this time may be set according to the state amounts of the dynamic model shown in Fig. 12 (e.g., the center-of-gravity position of the robot on the dynamic

model, and the position of the body mass point 3m).

Further, in the second reference example, if the compensating total floor reaction force moment vertical component M_{dmdz} takes a value within a floor reaction force moment vertical component compensating amount permissible range, then the model manipulation floor reaction force moment vertical component compensating amount will be zero. Alternatively, however, the model manipulation floor reaction force moment vertical component compensating amount at this time may be set according to the state amounts of the dynamic model shown in Fig. 12 (e.g., the antiphase arm swing angle and angular velocity, the body yaw angle, and angular velocity of the robot 1 on the dynamic model).

Referring now to Fig. 59 through Fig. 62, a third reference example of the present invention will be explained. In the explanation of the third reference example, the like constituent parts or like functional parts as those in the aforesaid first reference example or the aforesaid second reference example will be assigned like reference numerals as those in the aforesaid first reference example or the aforesaid second reference example, and the explanation thereof will be omitted. In the third reference example, the aspects explained with reference to Fig. 1 to Fig. 3 and Fig. 5 to Fig. 12 are identical to those in the aforesaid first reference

example.

An outline of the aspects of the third reference example that are different from those of the aforesaid first reference example and the second reference example will be explained. An original gait and a corrected gait are generated at the same time. The corrected gait is obtained by correcting an original gait to stabilize a body posture (an inclination angle and a yaw angle) of the actual robot 1. Further, in the corrected gait, if the corrected gait still has an allowance (an allowance in a floor reaction force moment that can be generated about a desired ZMP) after generating a floor reaction force moment required for restoring a posture by compliance control, then it is determined to converge to the original gait as much as possible, using the allowance.

A block diagram showing a functional construction of a control unit 60 in the third reference example is shown in Fig. 59. In the third reference example, a compensating total floor reaction force moment horizontal component M_{dmdxy} determined by a posture inclination stabilization control calculator 112 is supplied to a gait generating device 100.

A compensating total floor reaction force moment vertical component M_{dmdz} determined by a yaw stabilization control calculator 113 is also supplied to the gait generating device 100.

Further, a compensating total floor reaction force

moment distributor 120 that determines a model
manipulation floor reaction force moment (a horizontal
component and a vertical component) and a desired floor
reaction force moment (a horizontal component and a
5 vertical component) for compliance control on the basis of
the M_{dmdxy} and M_{dmdz} is incorporated in the gait
generating device 100. The desired floor reaction force
moment for compliance control is output from the gait
generating device 100 to a composite-compliance operation
10 determiner 104. The compensating total floor reaction
force moment distributor 120 in the gait generating device
100 performs more complicated processing than the
compensating total floor reaction force moment horizontal
component distributor 110 and the model manipulation floor
15 reaction force moment vertical component determiner model
111 of the aforesaid second reference example. The
functional construction of the control unit 60 except for
the above is identical to that in the second reference
example.

20 Fig. 60 shows the flowchart of the main routine
processing of the gait generating device 100 in the third
reference example.

In this Fig. 60, the same processing as that from
S010 to S028 of the main flowchart (Fig. 13) of the
25 aforesaid first reference example is carried out from
S2010 to S2028. In the initialization in S800 of the
flowchart of Fig. 43 that is the subroutine of S028 (S2028

in the third reference example), the initial state of a current time gait is obtained by converting the terminal state of the last time's corrected gait (the final gait that the gait generating device 100 outputs) into a
5 current time's supporting leg coordinate system. The terminal state of the original gait determined in S2032, which will be discussed hereinafter, is not used in S800 of the subroutine of S2028.

Subsequently, the processing proceeds to S2030
10 wherein the floor reaction force moment horizontal component permissible range for compliance control is determined. The method for determining the floor reaction force moment horizontal component permissible range is the same as that in S3032 (Fig. 56) of the second reference
15 example.

After completing the processing of S2030, or if the determination result of S2016 is NO, the program proceeds to S2032 wherein an instantaneous value of the original gait (the current time value at time t) is determined.
20 The original gait is a gait that is generated so that the floor reaction force moment horizontal component about a desired ZMP is zero.

This original gait is generated according to an algorithm obtained by partly changing the subroutine
25 processing of S3032 of Fig. 56 in the aforesaid second reference example. More specifically, in S3104 and S3130 of Fig. 58, which is the subroutine processing in S3032

(precisely, the subroutine processing of S3414 of Fig. 57, which is the subroutine processing of S3032), a body horizontal acceleration α_{tmp} is determined, the model manipulation floor reaction force moment horizontal component being zero (the desired floor reaction force moment horizontal component about a desired ZMP being zero). The processing except for this may be the same as the processing of S3032 of Fig. 56.

Subsequently, the processing proceeds to S2034 wherein the instantaneous value of a corrected gait is determined. The corrected gait is the desired gait finally output from the gait generating device 100.

The processing of S2034 is implemented by the subroutine processing illustrated by the flowchart of Fig. 61. This will be explained in detail below.

First, from S2100 to S2111, the same processing as that of S3400 to S3411 of Fig. 57 explained in the second reference example is carried out.

Subsequently, the processing proceeds to S2112 wherein the floor reaction force moment horizontal component permissible range $[M_{xymin}, M_{xymax}]$ at the current time is determined on the basis of gait parameters. This is carried out in the same manner as that for determining the floor reaction force moment horizontal component permissible range $[M_{xymin}, M_{xymax}]$ in S3412 of Fig. 57.

Subsequently, the processing proceeds to S2114

wherein a model manipulation floor reaction force moment
(a horizontal component and a vertical component), a
desired floor reaction force moment for compliance control,
a body horizontal acceleration, a body posture inclination
5 angular acceleration, and an antiphase arm swing angular
acceleration are determined such that the conditions of a
floor reaction force moment horizontal component
permissible range, a floor reaction force moment vertical
component permissible range, and a floor reaction force
10 horizontal component permissible range are satisfied.

The details of S2114 will be explained below in
conjunction with the flowchart of Fig. 62 that illustrates
the processing.

First, in S2200, the difference in horizontal body
15 position between models, which is the difference between
the horizontal body position of the corrected gait and the
horizontal body position of the original gait, is
determined. At this point, the current time value (the
value at time t) of the horizontal body position of the
20 corrected gait has not yet been determined. In S2200,
therefore, the last time value (the last value determined
in the control cycle at time $t-\Delta t$) of the horizontal body
position of the corrected gait, and the last time value
(the value determined in S2032 in the control cycle at
25 time $t-\Delta t$) or a current time value (the value determined
in S2032 in the control cycle at time t) of the horizontal
body position of the original gait are used to calculate

the difference in horizontal body position between models.

Subsequently, the processing proceeds to S2202 wherein the difference in body posture inclination angle between models, which is the difference between the body posture inclination angle of the corrected gait and the body posture inclination angle of the original gait, is determined. In this S2202, the last time value of the body posture inclination angle of the corrected gait and the last time value or the current time value of the body posture inclination angle of the original gait are used to determine the difference in body posture inclination angle between models, as in the case of the processing for calculating the difference in horizontal body position between models in S2200.

Subsequently, the processing proceeds to S2204 wherein the difference in antiphase arm swing angle between models, which is the difference between the antiphase arm swing angle of the corrected gait and the antiphase arm swing angle of the original gait, is determined. In this S2204, the last time value of the antiphase arm swing angle of the corrected gait and the last time value or the current time value of the antiphase arm swing angle of the original gait are used to determine the difference in antiphase arm swing angle between models, as in the case of the processing for calculating the difference in horizontal body position between models in S2200.

Subsequently, the processing proceeds to S2206 wherein, based on the difference in horizontal body position between models, a required value M_{pfdmd} of model horizontal body position stabilization floor reaction force moment that is necessary for converging the difference to zero is determined. If the floor reaction force moment for generating a body horizontal acceleration of the body translational mode of the corrected gait is merely balanced with the floor reaction force moment for generating a body horizontal acceleration of the body translational mode of the original gait, then the difference in horizontal body position between models diverges. The required value M_{pfdmd} of model horizontal body position stabilization floor reaction force moment has a meaning as a moment resulting from subtracting the floor reaction force moment for generating the body horizontal acceleration of the body translational mode of the original gait from the floor reaction force moment generated when a motion is made to return the horizontal body position of the corrected gait to the horizontal body position of the original gait by the aforesaid body translational mode.

Specifically, the required value M_{pfdmd} of model horizontal body position stabilization floor reaction force moment is determined according to, for example, the feedback control law of the equation given below. In this example, the PD control law is used as the feedback

control law; alternatively, however, other feedback control laws, such as PID, may be applied.

Mpfdmd = Kmp * Difference in horizontal body position
5 between models + Kmpv * Temporal differential value of the
difference in horizontal body position between models

..... Equation d28

where Kmp and Kmpv denote feedback gains (a
proportional gain and a differential gain)

10

Subsequently, the processing proceeds to S2208
wherein, based on the difference in body posture
inclination angle between models, a required value Mrfdmd
of the floor reaction force moment for stabilizing a model
15 body posture inclination angle that is necessary for
converging the difference to zero is determined. If the
floor reaction force moment for generating a body posture
inclination angular acceleration of the body inclination
mode of the corrected gait is merely balanced with the
20 floor reaction force moment for generating a body posture
inclination angular acceleration of the body inclination
mode of the original gait, then the difference in body
posture inclination angle between models does not converge
to zero. The required value Mrfdmd of the floor reaction
25 force moment for stabilizing a model body posture
inclination angle has a meaning as a moment resulting from
subtracting the floor reaction force moment for generating

the body posture inclination angle acceleration of the
body inclination mode of the original gait from the floor
reaction force moment generated when a motion is made to
return the body posture inclination angle of the corrected
5 gait to the body posture inclination angle of the original
gait by the aforesaid body inclination mode.

Specifically, the required value $Mrfdmd$ of the floor
reaction force moment for stabilizing a model body posture
inclination angle is determined according to, for example,
10 the feedback control law of the equation given below. In
this example, the PD control law is used as the feedback
control law; alternatively, however, other feedback
control laws, such as PID, may be applied.

15 $Mrfdmd = Kmr * \text{Difference in body posture inclination}$
 $\text{angle between models} + Kmr_v * \text{Temporal differential value}$
 $\text{of the difference in body posture inclination angle}$
 between models

..... Equation d29

20 where Kmr and Kmr_v denote feedback gains (a
proportional gain and a differential gain)

Subsequently, the processing proceeds to S2210
wherein, based on the difference in antiphase arm swing
25 angle between models, a required value $Mafdm$ of the floor
reaction force moment for stabilizing a model antiphase
arm swing angle that is necessary for converging the

difference to zero is determined. If the floor reaction
force moment for generating an antiphase arm swing angular
acceleration of the antiphase arm swing mode of the
corrected gait is merely balanced with the floor reaction
5 force moment for generating an antiphase arm swing angular
acceleration of the antiphase arm swing mode of the
original gait, then the antiphase arm swing angle between
models does not converge to zero. The required value
Mafdm of the floor reaction force moment for stabilizing
10 a model antiphase arm swing angle has a meaning as a
moment resulting from subtracting the floor reaction force
moment for generating the antiphase arm swing angular
acceleration of the antiphase arm swing mode of the
original gait from the floor reaction force moment
15 generated when a motion is made to return the antiphase
arm swing angle of the corrected gait to the antiphase arm
swing angle of the original gait by an antiphase arm swing
mode.

Specifically, the required value Mafdm of the floor
20 reaction force moment for stabilizing a model antiphase
arm swing angle is determined according to, for example,
the feedback control law of the equation given below. In
this example, the PD control law is used as the feedback
control law; alternatively, however, other feedback
25 control laws, such as PID, may be applied.

$$Mafdm = K_a * \text{Difference in antiphase arm swing angle}$$

between models + $K_{av} * \text{Temporal differential value of the difference in antiphase arm swing angle between models}$

..... Equation d29b

where K_{ar} and K_{av} denote feedback gains (a
5 proportional gain and a differential gain).

Incidentally, the moment obtained by subtracting the floor reaction force moment horizontal component for generating a body horizontal acceleration of the body translational mode of an original gait from the floor
10 reaction force moment horizontal component generated by the body translational mode of a finally determined corrected gait is called a floor reaction force moment for stabilizing a model horizontal body position. Further,
15 the moment obtained by subtracting the floor reaction force moment horizontal component for generating a body posture inclination angular acceleration of the body inclination motion mode of an original gait from the floor reaction force moment horizontal component generated by
20 the body inclination motion mode of a finally determined corrected gait is called a floor reaction force moment for stabilizing a model body posture inclination angle.

Further, the moment obtained by subtracting the floor reaction force moment vertical component for generating an
25 antiphase arm swing angular acceleration of the antiphase arm swing mode of an original gait from the floor reaction force moment vertical component generated by the antiphase

arm swing mode of a finally determined corrected gait is called a floor reaction force moment for stabilizing a model antiphase arm swing angle.

5 Meanwhile, linearity approximately holds between a perturbative motion and a perturbation floor reaction force. In other words, the floor reaction force of a motion obtained by adding a different perturbative motion to the motion of an original gait substantially agrees with the floor reaction force of the original gait to 10 which the perturbation floor reaction force generated by each perturbative motion has been added. In the antiphase arm swing mode, a floor reaction force moment horizontal component remains unchanged. Hence, the following equation approximately holds.

15 Model manipulation floor reaction force moment horizontal component = Model horizontal body position stabilizing floor reaction force moment + Model body posture inclination angle stabilizing floor reaction force moment
20 Equation d30

Taking into account that the Equation d30 approximately holds and a floor reaction force moment vertical component changes in proportion to an antiphase 25 arm swing angular acceleration, if a model horizontal body position stabilizing floor reaction force moment is determined so that it agrees with or approximates as much

as possible to the required value M_{pfdmd} of model
horizontal body position stabilizing floor reaction force
moment, and a model body posture inclination angle
stabilizing floor reaction force moment is determined so
5 that it agrees with or approximates as much as possible to
the required value M_{rfdmd} of a model body posture
inclination angle stabilizing floor reaction force moment,
and a model antiphase arm swing angle stabilizing floor
reaction force moment is determined so that it agrees with
10 or approximates as much as possible to the required value
 M_{afdm} of a model antiphase arm swing angle stabilizing
floor reaction force moment, then a model manipulation
floor reaction force moment appropriate for a corrected
gait can be generated to converge the body horizontal
15 acceleration and the body posture inclination angular
acceleration of a corrected gait to possible ranges for
the body horizontal acceleration and the body posture
inclination angular acceleration, respectively, of an
original gait, while satisfying the restoring conditions
20 shown below.

Thus, after S2210, the processing proceeds to S2212
wherein a model horizontal body position stabilizing floor
reaction force moment (the floor reaction force moment of
the body translational mode), a model body posture
25 inclination angle stabilizing floor reaction force moment
(the floor reaction force moment of the body inclination
mode), and a model antiphase arm swing angle stabilizing

floor reaction force moment are determined to satisfy the conditions shown below (these are called "restoring conditions") as much as possible. Furthermore, the body horizontal acceleration, the body posture inclination angular acceleration, and the antiphase arm swing angular acceleration of a corrected gait are determined to satisfy the definitions of the model horizontal body position stabilizing floor reaction force moment, the model body posture inclination angle stabilizing floor reaction force moment, and the model antiphase arm swing angle stabilizing floor reaction force moment described above. Regarding the restoring conditions shown below, conditions with smaller numbers have higher priorities. In other words, if conflicting, incompatible conditions are encountered, then priority goes to a condition with a smaller number will be satisfied (met). However, restoring conditions of 1, 2 and 3 must always be satisfied (met).

Restoring condition 1) The sum of the compensating total floor reaction force moment horizontal component M_{dmdxy} and a model manipulation floor reaction force moment (this corresponds to a desired floor reaction force moment horizontal component for compliance control if the above Equation d27b holds) does not exceed a floor reaction force moment horizontal component permissible range.

Restoring condition 2) The floor reaction force

horizontal component of a corrected gait does not exceed a floor reaction force horizontal component permissible range.

Restoring condition 3) The sum of the floor reaction force moment vertical component of a corrected gait and a compensating total floor reaction force moment vertical component M_{dmdz} (this corresponds to a desired floor reaction force moment vertical component for compliance control) does not exceed a floor reaction force moment vertical component permissible range.

Restoring condition 4) A model body posture inclination angle stabilization floor reaction force moment agrees with or is close as much as possible to a required model body posture inclination angle stabilization floor reaction force moment value M_{rfdmd} . This condition is the condition for the body posture inclination angle of a corrected gait to converge to the body posture inclination angle of an original gait (originally planned gait).

Restoring condition 5) A model horizontal body position stabilization floor reaction force moment agrees with or is close as much as possible to a required value M_{pfdmd} of model horizontal body position stabilization floor reaction force moment. This condition is the condition for a horizontal body position of a corrected gait to converge to the horizontal body position of an original gait (originally planned gait).

Restoring condition 6) A model antiphase arm swing angle stabilization floor reaction force moment agrees with or is close as much as possible to a required value Mafdm of model antiphase arm swing angle stabilization floor reaction force moment. This condition is the condition for the antiphase arm swing angle of a corrected gait to converge to the antiphase arm swing angle of an original gait (originally planned gait).

Restoring condition 7) A model body posture inclination angle stabilization floor reaction force moment, a model horizontal body position stabilization floor reaction force moment, and a model antiphase arm swing angle stabilization floor reaction force moment are all continuous.

The processing of S2212 for determining a body horizontal acceleration, a body posture inclination angle acceleration, an antiphase arm swing angular acceleration, etc. that satisfy the restoring conditions 1 through 6 described above is carried out, for example, as follows.

First, in order to satisfy the aforesaid restoring conditions 1, 2, 4, and 5, a model horizontal body position stabilization floor reaction force moment and a model body posture inclination angle stabilization floor reaction force moment are determined, and further a body horizontal acceleration and a body posture inclination angular acceleration are determined. This processing is discussed in detail in the art of PCT/JP03/00435

previously proposed by the present applicant, so that the explanation thereof will be omitted here.

Subsequently, the model antiphase arm swing stabilization floor reaction force moment is determined to satisfy the aforesaid restoring conditions 3 and 6, and further, the antiphase arm swing angular acceleration is determined.

Specifically, a floor reaction force moment vertical component about a desired ZMP that is generated if a motion is provisionally implemented at the body horizontal acceleration and the body posture inclination angular acceleration determined as described above and at an antiphase arm swing angular acceleration β_{aorg} of an original gait (dynamically balancing the motion) is determined. Hereinafter, this will be referred to as a floor reaction force moment vertical component without correction.

Subsequently, a sum M_{sumz} of a floor reaction force moment vertical component without correction, the required value M_{afdm} of model antiphase arm swing angle stabilization floor reaction force moment, and a compensating total floor reaction force moment vertical component M_{dmz} is determined according to the following equation.

M_{sumz} = Floor reaction force moment vertical component without correction

$$+ M_{afdm} + M_{dmz}$$

Subsequently, a model antiphase arm swing
stabilization floor reaction force moment is determined
5 according to the following equation.

If $M_{sumz} >$ Upper limit value of a floor reaction
force moment vertical component permissible range, then
Model antiphase arm swing stabilization floor
10 reaction force moment = $-M_{dmz}$
- Floor reaction force moment vertical component
without correction
+ Upper limit value of the floor reaction force
moment vertical component permissible range.

15

If $M_{sumz} <$ Lower limit value of a floor reaction
force moment vertical component permissible range, then
Model antiphase arm swing stabilization floor
reaction force moment = $-M_{dmz}$
20 - Floor reaction force moment vertical component
without correction
+ Lower limit value of the floor reaction force
moment vertical component permissible range.

25

If a lower limit value of a floor reaction force
moment vertical component permissible range $\leq M_{sumz}$ and
 $M_{sumz} \leq$ Upper limit value of the floor reaction force

moment vertical component permissible range, then

Model antiphase arm swing stabilization floor
reaction force moment

$$\begin{aligned} &= \text{Required value } M_{afdm} \text{ of model antiphase arm} \\ 5 \quad &\text{swing angle stabilization floor reaction force moment} \\ &\dots\dots \text{Equation d26c} \end{aligned}$$

Subsequently, the antiphase arm swing angular
acceleration of a corrected gait is determined according
10 to the following equation.

Antiphase arm swing angular acceleration of corrected
gait

$$\begin{aligned} &= \text{Original gait antiphase arm swing angular} \\ 15 \quad &\text{acceleration } \beta_{aorg} \\ &+ \text{Model antiphase arm swing stabilization floor} \\ &\text{reaction force moment} \\ &/ \text{Equivalent inertial moment of arm swing motion } \Delta M_{az} \end{aligned}$$

20 The floor reaction force moment vertical component of
the corrected gait is the sum of the antiphase arm swing
angular acceleration of the original gait β_{aorg} and the
model antiphase arm swing stabilization floor reaction
force moment. Therefore, the aforesaid three restoring
25 conditions are satisfied by determining the model
antiphase arm swing stabilization floor reaction force
moment according to the above equations.

After carrying out the processing of S2212 as described above, the program processing proceeds to S2214 wherein a model manipulation floor reaction force moment horizontal component is determined according to the above equation d30. More specifically, the sum of the model horizontal body position stabilization floor reaction force moment and the model body posture inclination angle stabilization floor reaction force moment that has been obtained in S2208 is determined as the model manipulation floor reaction force moment horizontal component. Alternatively, the floor reaction force moment about a desired ZMP may be directly calculated on the basis of a current time instantaneous value of the motion of a finally determined corrected gait, and the calculation result may be defined as the model manipulation floor reaction force moment.

Subsequently, the processing proceeds to S2216 wherein a desired floor reaction force moment horizontal component for compliance control is determined according to the above equation d27b. More specifically, the sum of the compensating total floor reaction force moment horizontal component M_{dmdxy} and the model manipulation floor reaction force moment horizontal component obtained in S2214 is determined as the desired floor reaction force moment horizontal component for compliance control.

Subsequently, the processing proceeds to S2218 wherein a desired floor reaction force moment vertical

component for compliance control is determined according to the equation shown in the figure. The floor reaction force moment vertical component that balances with the corrected gait in the equation shown in the figure

5 (dynamically balances with the motion of the corrected gait) is the sum of a floor reaction force moment vertical without correction and a model antiphase arm swing stabilization floor reaction force moment. Alternatively, however, the floor reaction force moment vertical
10 component about a desired ZMP may be directly calculated on the basis of a current time instantaneous value of the motion of a finally determined corrected gait.

Thus, the processing of S2114 of Fig. 61 is finished, and then the processing proceeds to S2116. The processing
15 of this S2116 is the same as that of S3416 of Fig. 57 in the aforesaid second reference example; the current time value of a horizontal body position is determined by the second order integration of a body horizontal acceleration and the current value of a body posture inclination angle
20 is determined by the second order integration of a body posture inclination angle acceleration.

Subsequently, the processing proceeds to S2118. The processing in this S2118 is the same as that of S3418 of Fig. 57 in the aforesaid second reference example; the
25 current time value of an antiphase arm swing angle is determined by the second order integration of an antiphase arm swing angular acceleration.

Subsequently, the processing proceeds to S2036 of Fig. 60 to add a control cycle Δt to time t , and then returns to S2014 wherein it waits for a timer interrupt for each control cycle.

5 Supplementally, to determine a gait instantaneous value on the basis of a dynamic model in the third reference example, the state amount of the dynamic model (or the last time's or the last but one time's gait instantaneous values) are also necessary, so that two
10 dynamic models, for generating a corrected gait and for generating an original gait are necessary. In the third reference example, the dynamic models are the dynamic model shown in Fig. 12.

 In the third reference example, as discussed above,
15 an original gait and a corrected gait are generated in parallel, and the corrected gait is corrected to stabilize the posture (the inclination angle and the yaw angle) of the actual robot 1. If there is still an allowance even after a floor reaction force moment (a horizontal
20 component and a vertical component) required for posture restoration by compliance control is generated, then the allowance is used for convergence to an original gait as much as possible. Therefore, in addition to the actions and advantages of the aforesaid second reference example,
25 a gait close to an initially set original gait, that is, a gait approximated to the gait initially required, can be generated. Hence, if a preset travel path is provided,

then it will be possible to prevent significant deviation from the travel path. Moreover, a priority has been given to the convergence of the body posture inclination angle of the corrected gait to the body posture inclination angle of an original gait (the initially determined gait) rather than to the convergence of the horizontal body position of the corrected gait to the horizontal body position of the original gait (the initially determined gait) (the motion of the body translational mode has been adjusted as much as possible within the range in which a floor reaction force horizontal component permissible range is satisfied), thus making it possible to restrain a significant change in the body posture inclination angle.

Referring now to Fig. 63 through Fig. 71, a first embodiment of the present invention will be explained. In the explanation of the present embodiment, the like constituent parts or like functional parts as those in any one of the aforesaid first to third reference examples will be assigned like reference numerals as those in the aforesaid first to third reference examples, and detailed explanation thereof will be omitted.

Referring to Fig. 63, in the present embodiment, the functional construction of a control unit 60 is the same as that of the third reference example, that is, the same as that shown in Fig. 59 mentioned above except that the yaw stabilization control calculator 113 has been deleted

therefrom and the compensating total floor reaction force moment vertical component M_{dmz} is not supplied to the gait generating device 100. And, in the present embodiment, the algorithm for generating gaits executed by a gait generating device 100 is different from that of the aforesaid third reference example. And the processing of units other than the gait generating device 100 is identical to that of the aforesaid third reference example. Supplementally, the compensating total floor reaction force moment vertical component M_{dmz} may be supplied to the composite-compliance operation determiner 104, as in the first reference example.

Fig. 64 is a block diagram showing an outline of the processing of the gait generating device 100 in the present embodiment. Referring to this Fig. 64, an outline of the processing of the gait generating device 100 will be explained below. Incidentally, the outline of the processing to be explained below in conjunction with Fig. 64 will apply also to second to fourth embodiments to be discussed hereinafter. In the present embodiment and the second to the fourth embodiments to be discussed hereinafter, the dynamic model of the aforesaid Fig. 12 will be referred to as a simplified model.

As illustrated, the gait generating device 100 is equipped with a gait parameter determiner 100a. The gait parameter determiner 100a determines a value of a parameter of a desired gait (the parameter defining the

desired gait) or a time series table thereof. This corresponds to the processing of S3520 through S3530 of the flowchart of Fig. 66 to be discussed hereinafter.

Although details will be given hereinafter,
5 parameters determined by the gait parameter determiner 100a includes the parameters that define a desired foot position/posture trajectory, a desired arm posture trajectory, a reference body posture trajectory, a desired ZMP trajectory, a desired floor reaction force vertical
10 component trajectory, etc. in addition to a parameter that defines a floor reaction force horizontal component permissible range, a parameter that defines a ZMP permissible range (or a floor reaction force moment horizontal component permissible range), and a parameter
15 that defines a floor reaction force moment vertical component permissible range. In this case, the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range to be set in the present embodiment come
20 in two types, one for simplified model gaits set by the processing of S3526 to be described later and the other for correcting gait to be set in S3530. Meanwhile, a ZMP permissible range (or a floor reaction force moment horizontal component permissible range) comes in only one
25 type for full model correction (for correcting a gait) set by the processing of S3530. In the present embodiment, S3530 sets a parameter for defining the ZMP permissible

range. This is equivalent to setting a parameter that defines a floor reaction force moment horizontal component permissible range. This is because the value obtained by dividing a floor reaction force moment horizontal component by a desired floor reaction force vertical component represents the amount of the deviation of a ZMP (floor reaction force central point) from a desired ZMP, as has been explained in relation to S3030 of Fig. 56 in the aforesaid second reference example.

Here, the ZMP permissible range to be set in the present embodiment will be set as shown in Fig. 65. The details have been given in PCT/JP03/00435, so that further explanation will be omitted.

A gait parameter determined by the gait parameter determiner 100a is input to a desired instantaneous value generator 100b. Based on the input gait parameter, the desired instantaneous value generator 100b sequentially calculates (generates) the instantaneous values of desired foot position/posture, a desired ZMP, a desired floor reaction force vertical component, a desired arm posture, a desired total center-of-gravity vertical position, a desired vertical body position, a floor reaction force horizontal component permissible range, a ZMP permissible range, a reference body posture angle, and a reference antiphase arm swing angle at current time t (Fig. 64 describes only a part of desired instantaneous values). The processing of the desired instantaneous value

generator 100b corresponds to the processing of S3400 through S3412 of Fig. 57 carried out in the processing of S3532 of the flowchart of Fig. 66 to be discussed hereinafter and the processing of S3534 of Fig. 66. In the present embodiment, of the desired instantaneous values calculated by the desired instantaneous value generator 100b, some instantaneous values (specifically, the instantaneous value of a desired vertical body position) are provisional values, which will be corrected later. The instantaneous values of the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range calculated by the desired instantaneous value generator 100b come in the instantaneous values for simplified model gaits and the instantaneous values for correcting gaits.

Desired instantaneous values (some are provisional instantaneous values) calculated (generated) by the desired instantaneous value generator 100b are input to a full-model correction unit 100c. Also input to the full-model correction unit 100c is the compensating total floor reaction force moment horizontal component M_{dmdxy} determined by the aforesaid posture inclination stabilization control calculator 112 (refer to Fig. 63). The full-model correction unit 100c is provided with a simplified model 100c1 and a full model 100c2 as dynamic models. Based on the simplified model 100c1, the full-model correction unit 100c determines the provisional

instantaneous values or the like of a desired body position/posture and an antiphase arm swing angle from the input values, and further corrects the provisional instantaneous values or the like of the determined body position/posture and the antiphase arm swing angle by using the full model 100c2.

As an alternative construction, the simplified model 100c1 may not be included in the full-model correction unit 100c2. The full model 100c2 includes either an inverse full model (an inverse dynamic full model) or a forward full model (a forward dynamic full model), as will be discussed hereinafter.

The full-model correction unit 100c basically executes the processing of B to satisfy the following conditions A1 through A4. Specifically, the full-model correction unit 100c carries out B) given below to satisfy the following conditions:

A1) the value obtained by adding the compensating total floor reaction force moment horizontal component $M_{dm dx y}$ to the floor reaction force moment balancing the motion of a corrected gait generated by the full-model correction unit 100c agrees with the floor reaction force moment for compliance control that is output from the full-model correction unit 100c,

A2) a true ZMP (the ZMP that satisfies the original definition corrected by generating a desired floor reaction force moment for compliance control about a

desired ZMP) lies in a ZMP permissible range (a permissible range that allows a sufficient stability allowance to be maintained),

A3) a floor reaction force horizontal component lies in the floor reaction force horizontal component permissible range for correcting a gait, and

A4) a desired floor reaction force moment vertical component for compliance control to be generated about a desired ZMP lies in a floor reaction force moment vertical component permissible range.

B) The full-model correction unit 100c corrects the body position/posture of a simplified model gait determined using the simplified model, and outputs the desired floor reaction force moment for compliance control about the desired ZMP.

The above condition A2 is equivalent to restricting a floor reaction force moment generated about the desired ZMP to a floor reaction force moment horizontal component permissible range that corresponds to a ZMP permissible range.

Here, the aforesaid simplified model 100c1 and the aforesaid full model 100c2 will be explained. The simplified model 100c1 is a dynamic model with an emphasis placed on a reduced volume of calculation or the ease of behavior analysis rather than dynamic accuracy, and may ignore some dynamic elements (e.g., ignore a change in the angular momentum about the center of gravity) or may have

contradiction (lack in preciseness). In the present embodiment, the dynamic model of Fig. 12 explained in the aforesaid first reference example (the dynamic model described in conjunction with the above Equations 01 to 05) is used as the simplified model 100c1.

The full model 100c2 means a robot dynamic model that is different from the simplified model 100c1. This is desirably a robot dynamic model having a higher approximation accuracy than that of the simplified model 100c1. This will be explained in conjunction with the illustrated example. As previously described, in the present embodiment, the dynamic model shown in the above Fig. 12 is used as the simplified model 100c1; therefore, a dynamic model having a higher approximation accuracy than that, such as the robot dynamic model like the multi-mass point model (the model having a mass point for each link of the robot 1) shown in, for example, Fig. 49 mentioned above, is desirably used as a full model 100c2. In this case, the full model 100c2 may be such that an inertial moment is set about a mass point.

However, the simplified model 100c1 and the full model 100c2 do not have to necessarily have different model approximation accuracy. The simplified model 100c1 and the full model 100c2 may share the same dynamic equations and have different floor reaction force horizontal component permissible ranges and/or floor reaction force moment vertical component permissible

ranges, that is, they may be different only in the permissible range for simplified model gaits and the permissible range for gait correction (for full model correction). For instance, the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range for generating gaits by the simplified model 100c1 may be merely set to be wide (may even exceed a frictional limit), while setting narrow ranges for the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range applied for correcting gaits using the full model 100c2, thereby making it difficult for the robot 1 to slip or spin.

In the present description, the model used to calculate (output) body position/posture and an antiphase arm swing angle on the basis of (by entering) desired foot position/posture, a desired floor reaction force (particularly, a desired ZMP and a desired floor reaction force vertical component) is called the "forward dynamic model." The model used to calculate (output) a floor reaction force (especially a desired ZMP or a floor reaction force moment (a horizontal component and a vertical component) and a floor reaction force horizontal component) on the basis of (by entering) desired foot position/posture, a desired body posture, a desired body position and an antiphase arm swing angle is called the

"inverse dynamic model." An input of the forward dynamic model includes at least a desired floor reaction force, while an input of the inverse dynamic model includes at least a desired motion.

5 The full model 100c2 provided in the full-model correction unit 100c is equipped with an inverse dynamic full model (frequently referred to simply as "inverse full model") or a forward dynamic full model (frequently referred to simply as "forward full model"). In general,
10 the volume of calculation of a forward dynamic model tends to be greater than that of an inverse dynamic model.

 The above is the outline of the processing in the gait generating device 100 in the present embodiment (the first embodiment).

15 The processing of the gait generating device 100 in the present embodiment will now be explained in detail. The gait generating device 100 in the present embodiment carries out the processing shown in the flowchart of Fig. 66 to generate gaits.

20 First, the same processing as the processing from S3010 to S3028 of Fig. 56 explained in the aforesaid second reference example is carried out in S3510 to S3528. The floor reaction force horizontal component permissible range for a current time gait determined in S608 of Fig. 39, which is the subroutine of S3026, and the floor
25 reaction force moment vertical component permissible range determined in S610 require less strict consideration given

to the limit of a frictional force than in the case of the
aforementioned first reference example, the second
reference example, and the third reference example, and
may be set to ranges that exceed the limit of the
5 frictional force. This is because the floor reaction
force horizontal component and the floor reaction force
moment vertical component will be eventually restricted by
a floor reaction force horizontal component permissible
range and a floor reaction force moment vertical component
10 permissible range for full model correction by the full
model correction, which will be discussed hereinafter.

Subsequently, the processing proceeds to S3530
wherein the parameters defining the floor reaction force
horizontal component permissible range, the floor reaction
15 force moment vertical component permissible range, and the
ZMP permissible range (floor reaction force central point
permissible range) for full model correction (for gait
correction) are determined. In this case, the floor
reaction force horizontal component permissible range for
20 full model correction is set to have a pattern, as shown
in the aforesaid Fig. 30, on the basis of a floor reaction
force vertical component trajectory and the above Equation
12 for the X-axis direction (the longitudinal direction)
and the Y-axis direction (the lateral direction),
25 respectively, as in the case of, for example, the floor
reaction force horizontal component permissible range for
the aforesaid simplified model gaits. Then, for example,

the value of $k_a \mu$ of the above Equation 12 is set as the parameter that defines the floor reaction force horizontal component permissible range for full model correction.

However, the floor reaction force horizontal component permissible range is desirably set to that it securely falls within the range of a frictional limit by, for example, setting the value of coefficient k_a of Equation 12 to be smaller than the floor reaction force horizontal component permissible range for simplified model gaits.

The floor reaction force moment vertical component permissible range is set in the same manner as that for the floor reaction force horizontal component permissible range. More specifically, the floor reaction force moment vertical component permissible range is set to the pattern, as shown in the aforesaid Fig. 41, according to the aforesaid Equation 1012.

The ZMP permissible range is set in the same manner as that for the case explained in conjunction with the setting of the floor reaction force moment horizontal component permissible range in S3030 of Fig. 56 in the aforementioned second reference example. The ZMP permissible range may be of course converted into a floor reaction force moment horizontal component permissible range equivalent thereto by multiplying the ZMP permissible range by a desired floor reaction force vertical component.

Subsequently, the processing proceeds to S3532

wherein the instantaneous value of the current time gait
(the value at the current time t) is determined using the
aforesaid simplified model (the dynamic model shown in Fig.
12). The processing of this S3532 is identical to the
5 processing of S030 of Fig. 13 in the aforesaid first
reference example.

The instantaneous value of the gait at the current
time t generated by the processing up to S3532 explained
above will be hereinafter referred to as the simplified
10 model gait instantaneous value. In the present embodiment,
the simplified model gait instantaneous value is
determined using a simplified model (the dynamic model
shown in Fig. 12) such that the floor reaction force
moment horizontal component generated about a desired ZMP
15 by the resultant force of the inertial force and gravity
generated in the robot 1 by a motion thereof is zero (such
that a dynamic balance condition related to the desired
ZMP is satisfied).

In this case, of the simplified model gait
20 instantaneous values, the instantaneous values of a
horizontal body position and a body posture inclination
angle, the instantaneous value of a vertical body position,
and an instantaneous value of an antiphase arm swing angle
are provisional instantaneous values and will be corrected
25 by full model correction to be discussed later. Further,
of the simplified model gait instantaneous values in the
present embodiment, the instantaneous value of the desired

floor reaction force moment horizontal component about the desired ZMP is normally zero, whereas a desired floor reaction force moment horizontal component for compliance control as the desired value of the floor reaction force moment horizontal component generated about the desired ZMP by the full model correction, which will be discussed later, is generated.

Subsequently, the processing proceeds to S3534 wherein the instantaneous values (the values at the current time t) of the floor reaction force horizontal component permissible range, the floor reaction force moment vertical component permissible range, and the ZMP permissible range for gait correction are determined on the basis of the parameters (which have been set in S3530) that define the floor reaction force horizontal component permissible range, the floor reaction force moment vertical component permissible range, and the ZMP permissible range for gait correction (for full model correction).

Subsequently, the processing proceeds to S3536 wherein the full model is used to generate a corrected gait (to correct the gait) so as to determine the instantaneous value of a final desired gait. More specifically, as explained with reference to the aforesaid Fig. 64, the calculation (determination) of corrected desired body position/posture, a corrected desired antiphase arm swing angle, and a desired floor reaction

force moment (a horizontal component and a vertical component) for compliance control as a desired floor reaction force moment (a horizontal component and a vertical component) about a desired ZMP is mainly performed.

Subsequently, the processing proceeds to S3538 to increment the time t by Δt , and returns to S3514 again to repeat the processing from S3514 to S3538.

The processing of S3536 described above, which constitutes a characteristic of the present embodiment, will be explained in detail below. The gait correcting technique of a device in accordance with the present embodiment is a full-model feedforward correction type. Furthermore, the gait correction technique uses an inverse dynamic full model (inverse full mode), and it is a technique that does not correct an input of a simplified model gait, and it is a technique that uses a perturbation model.

Fig. 67 is a functional block diagram explaining the operation of the gait generating device 100 according to the present embodiment, specifically, the technique for correcting a gait in S3536 of the flowchart of Fig. 66. A simplified model 200 shown in Fig. 67 represents not only a dynamic model but the processing of S3510 to S3532 discussed above, namely, the processing of calculating (determining) the instantaneous value of a simplified model gait. In Fig. 67, therefore, the portion beyond the

simplified model 200 corresponds to the processing of S3536.

The processing for determining the instantaneous values of the floor reaction force horizontal component permissible range and the ZMP permissible range for gait correction (for full model correction) is shown using a reference mark S3534 of the flowchart of Fig. 66.

The actual processing is implemented by a single computer, so that it is implemented in order toward a downstream side (toward a gait output side) from an upstream side of the block diagram after the block diagram is broken up. However, a feedback amount returned to the upstream side uses a value (a state amount) calculated in the last control cycle (time $t - \Delta t$ with respect to the current time t). Hereinafter, the value calculated in the last time control cycle (time $t - \Delta t$) will be abbreviated as a last time value.

Each time the processing of S3536 is carried out, the calculation for one control cycle in the block diagram is performed.

In S3536, first, the instantaneous values of variables representing a motion (this is called a motion variable), such as the desired body posture angle (hereinafter referred to as the simplified model body posture angle. Further, an inclination angle component thereof will be referred to as the simplified model body posture inclination angle), the desired horizontal body

position (hereinafter referred to as the simplified model horizontal body position), the desired center-of-gravity position, the desired foot position/posture, and the desired arm posture (including the desired antiphase arm swing angle) of the simplified model gait obtained as described above, and the instantaneous value of a desired ZMP are input to the aforesaid inverse dynamic full model (inverse full model) 201. The floor reaction force horizontal component balancing the motion represented by the input motion variables (in other words, a full model is generated by the motion) and the floor reaction force moment about the desired ZMP (a horizontal component and a vertical component) are calculated by the calculation processing of the inverse full model 201. In the present embodiment, the floor reaction force moment horizontal component about the desired ZMP in the simplified model gait is zero, so that the floor reaction force moment horizontal component about the desired ZMP calculated by the inverse full model 201 has a meaning as an error of a simplified model gait. Incidentally, the floor reaction force horizontal component, the floor reaction force moment horizontal component, and the floor reaction force moment vertical component determined by the inverse full model 201 are called "the full-model floor reaction force horizontal component," "the full-model floor reaction force moment horizontal component," and "the full-model floor reaction force moment vertical component,"

respectively. Hereinafter, the full-model floor reaction force horizontal component will be frequently abbreviated as F_{full} , the full-model floor reaction force moment horizontal component will be frequently abbreviated as M_{fullxy} , and the full-model floor reaction force moment vertical component will be frequently abbreviated as M_{fullz} .

Furthermore, the aforesaid inverse full model 201 calculates the vertical body position that satisfies a desired center-of-gravity position. Although not shown, the inverse full model 201 also calculates the center-of-gravity horizontal position.

Supplementally, a desired total center-of-gravity vertical position is input to the full model, and a desired floor reaction force vertical component is determined from the second order differential value of the desired total center-of-gravity vertical position. Hence, there is no particular need to input a desired floor reaction force vertical component to the full model. For a reason of achieving a reduction of calculation or the like, a desired floor reaction force vertical component may be input to the full model even if it is redundant.

A perturbation model used for gait correction will now be explained.

The perturbation model is composed of a horizontal body position correcting perturbation model 202, a body posture inclination angle correcting perturbation model

203, and an antiphase arm swing angle correcting
perturbation model 231. The perturbation model may be a
single model shown in Fig. 12 rather than being composed
of such three separate models. The body posture
5 inclination angle correcting perturbation model 203 is
abbreviated as the body posture angle correcting
perturbation model 203 in the figure.

The horizontal body position correcting perturbation
model 202 represents the relationship between the
10 perturbation of a floor reaction force and the
perturbation of a horizontal body position in the
aforesaid body translational mode.

The horizontal body position correcting perturbation
model 202 receives a correction amount of a desired floor
15 reaction force moment and calculates a correction amount
of a desired horizontal body position that dynamically
balances with the received correction amount of the
desired floor reaction force moment. This input (the
correction amount of the desired floor reaction force
20 moment) is called a perturbation model moment for
correcting horizontal body position M_p . An output (the
correction amount of a desired horizontal body position)
of the horizontal body position correcting perturbation
model 202 is called a correcting perturbation model
25 horizontal body position X_c . The floor reaction force
horizontal component generated by the horizontal body
position correcting perturbation model 202 is called a

perturbation model floor reaction force horizontal component for correcting horizontal body position F_p .

5 The horizontal body position correcting perturbation model 202 is represented by an inverted pendulum composed of a support point, an inverted pendulum mass point (body mass point) and an extensible support rod connecting them, as shown in Fig. 68. The position of the support point is set so that the horizontal position of the support point agrees with the horizontal position of the origin of the
10 current time's gait supporting leg coordinate system described above, and the vertical position of the support point agrees with the vertical position of a desired ZMP. A mass m_b of the inverted pendulum mass point is identical to the mass of the body mass point of the aforesaid
15 simplified model (the model with 3 mass points + flywheels) shown in Fig. 12. A vertical position Z_c of the inverted pendulum mass point is to be identical to a vertical position Z_b of the body mass point position of the simplified model shown in Fig. 12, which corresponds
20 to a simplified gait.

The horizontal body position correcting perturbation model 202 shows the relationship between a perturbation ΔM_y of a floor reaction force moment and a perturbation ΔX_b of a body mass point horizontal position in the
25 aforesaid simplified model.

Hence, assuming that parameters other than M_y , X_b , and Z_b take constants, if the relationship between the

perturbation ΔM_y of a floor reaction force moment and the perturbation ΔX_b of a body mass point horizontal position is determined from the above Equation 03y, then the following equation will be obtained.

5

$$\Delta M_y = -m_b \cdot \Delta X_b \cdot (g + d^2 Z_b / dt^2) + m_b \cdot (Z_b - Z_{zmp}) \cdot d^2 \Delta X_b / dt^2$$

... Equation a12

10 Similarly, assuming that parameters other than F_x and X_b take constants, if the relationship between the perturbation ΔF_x of a floor reaction force horizontal component and the perturbation ΔX_b of a body mass point horizontal position is determined from the above Equation 02x, then the following equation will be obtained.

15

$$\Delta F_x = m_b \cdot d^2 \Delta X_b / dt^2 \quad \dots \text{Equation a13}$$

20 A body translational mode floor reaction force ratio h , which is the ratio of ΔM_p to ΔF_p generated by a horizontal body acceleration, is the ratio of the term generated by the horizontal body acceleration (that is, the second term) of the right side of Equation a12 to Equation a13, so that the following equation will be obtained.

25

$$h = (Z_b - Z_{zmp}) \quad \dots \text{Equation a14}$$

In other words, the body translational mode floor reaction force ratio h corresponds to the height from the support point of the body mass point (the inverted pendulum mass point) of the simplified model.

5 Accordingly, the following equation is derived from Equation a12 and Equation a14.

$$\Delta My = -m_b \cdot \Delta X_b \cdot (g + d^2 Z_b / dt^2) + m_b \cdot h \cdot d^2 \Delta X_b / dt^2 \quad \dots \text{Equation a15}$$

10 Meanwhile, the floor reaction force vertical component that balances with the translational force vertical component of the resultant force of the gravity and the inertial force acting on the body mass point (the inverted pendulum mass point) is referred to as a body
15 floor reaction force vertical component F_{bz} . Specifically, the body floor reaction force vertical component F_{bz} is defined by the following equation.

$$F_{bz} = m_b \cdot (g + d^2 Z_b / dt^2) \quad \dots \text{Equation a16}$$

20

And, from the Equation a16 and the aforesaid Equation 01, the body floor reaction force vertical component F_{bz} is determined from the following equation.

$$25 \quad F_{bz} = F_z - m_{sup} \cdot (g + d^2 Z_{sup} / dt^2) - m_{swg} \cdot (g + d^2 Z_{swg} / dt^2)$$

... Equation a17

In other words, the body floor reaction force vertical component is equal to the sum of the floor reaction force vertical component F_z and the translational force vertical component of the resultant force of the gravity and the inertial force acting on both leg mass points of the aforesaid simplified model (the model with 3 mass points + flywheels) shown in Fig. 12.

Substituting Equation a16 into Equation a15 provides the following equation.

$$\Delta My = -F_{bz} \cdot \Delta X_b + m_b \cdot h \cdot d^2 \Delta X_b / dt^2 \quad \dots \text{Equation a18}$$

Associating ΔMy of Equation a18 with the perturbation model moment for correcting horizontal body position M_p , and associating ΔX_b with the correcting perturbation model horizontal body position X_c (substituting the perturbation model moment for correcting horizontal body position M_p into ΔMy of Equation a18, and substituting the correcting perturbation model horizontal body position X_c into ΔX_b) provide the following equation.

$$M_p = -F_{bz} \cdot X_c + m_b \cdot h \cdot d^2 X_c / dt^2 \quad \dots \text{Equation a19}$$

In other words, the horizontal body position correcting perturbation model 202 is expressed by Equation a19 by using the body translational mode floor reaction force ratio h determined according to Equation a14 and the

body floor reaction force vertical component F_{bz}
determined according to Equation a17.

Further, associating ΔF_x of Equation a13 with the
perturbation model floor reaction force horizontal
component for correcting horizontal body position F_p
provides the following equation.

$$F_p = m_b * d^2 X_c / dt^2 \quad \dots \text{Equation a20}$$

In other words, the horizontal body position
correcting perturbation model 202 is described by Equation
a14, Equation a17, Equation a19, and Equation a20.

Supplementally, it is regarded here that the
perturbation of a body mass point position and the
perturbation of a body position (the position of a body
representative point) agree; strictly speaking, however,
they do not always agree. Accordingly, to determine the
relationship among M_p , F_p , and X_c , a model that expresses
a geometric relationship between the horizontal position
of a body mass point and a body position is further
necessary.

Meanwhile, a body posture inclination angle
correcting perturbation model 203 represents a
relationship between the perturbation of a floor reaction
force and a body posture inclination angle in the
aforesaid body inclination mode.

The body posture inclination angle correcting
perturbation model 203 receives a correction amount of a

floor reaction force moment horizontal component and calculates a correction amount of a desired body posture inclination angle that dynamically balances with the received correction amount of the floor reaction force moment horizontal component. This input (the correction amount of the floor reaction force moment) is called a perturbation model moment for correcting body posture inclination angle M_r (abbreviated to a perturbation model for correcting body posture angle M_r in some cases). An output (the correction amount of a desired body posture inclination angle) of the body posture inclination angle correcting perturbation model 203 is called a correcting perturbation model body posture inclination angle θ_c . The floor reaction force horizontal component generated by the body posture inclination angle correcting perturbation model 203 is called a perturbation model floor reaction force horizontal component for correcting horizontal body position F_r . F_r is zero as mentioned above. This means that the following equation always holds.

$$F_r = 0 \quad \dots \text{Equation a21}$$

The body posture inclination angle correcting perturbation model 203 is expressed by a flywheel, as shown in Fig. 69. Supplementally, Fig. 69 shows only the flywheel that rotates about the Y-axis; however, the body posture inclination angle correcting perturbation model

203 actually requires a flywheel that rotates about the X-axis in addition to the flywheel rotating about the Y-axis. The inertia of those flywheels are the same as the flywheels FHx and FHy of the aforesaid simplified model (the model with 3 mass points + flywheels) shown in Fig. 12. The rotational angle of a flywheel of the body posture inclination angle correcting perturbation model 203 corresponds to the correcting perturbation model body posture inclination angle θ_c , and the floor reaction force moment horizontal component generated by the flywheel corresponds to the perturbation model moment M_r for correcting body posture inclination angle. In the following explanation, for the convenience of understanding, the explanation will center around the flywheel that rotates about the Y-axis. The same applies to the flywheel that rotates about the X-axis.

The body posture inclination angle correcting perturbation model 203 (more specifically, the model related to a sagittal plane) expresses a relationship between the floor reaction force moment perturbation ΔM_y and the body posture inclination angle perturbation $\Delta \theta_{by}$ in the aforesaid Equation 03y of the dynamic equation of the aforesaid simplified model (the model with 3 mass points + flywheels).

Accordingly, if parameters other than M_y and θ_{by} are regarded as constants, and if the relationship between the floor reaction force moment horizontal component

perturbation ΔMy and the body posture inclination angle perturbation $\Delta \theta_{by}$ is determined according to Equation 03y, then the following equation will be obtained.

5 $\Delta My = J * d^2 \Delta \theta_{by} / dt^2$... Equation a22

Associating ΔMy of Equation a22 with the perturbation model moment for correcting body posture inclination angle M_r , and associating $\Delta \theta_{by}$ with the correcting perturbation model body posture inclination angle θ_c provide the following equation.

10

$M_r = J * d^2 \Delta \theta_c / dt^2$... Equation a23

15 In other words, the body posture inclination angle correcting perturbation model 203 is represented by equation a23. The perturbation model floor reaction force horizontal component for correcting horizontal body position F_r is determined according to Equation a21 as described above ($F_r = 0$). In the above description, the dynamics of the body posture inclination angle correcting perturbation model 203 has been explained on the sagittal plane. The dynamics on a lateral plane is represented by the same type as Equation a23.

20

25 An antiphase arm swing angle correcting perturbation model 231 shows the relationship between the perturbation of a floor reaction force and the perturbation of an

antiphase arm swing angle in the antiphase arm swing mode.

The antiphase arm swing angle correcting perturbation model 231 receives a correction amount of a floor reaction force moment vertical component and calculates a
5 correction amount of a desired antiphase arm swing angle that dynamically balances with the received correction amount of the floor reaction force moment vertical component. This input (the correction amount of the floor reaction force moment vertical component) is called a
10 perturbation model moment for correcting antiphase arm swing angle M_a . An output (the correction amount of a desired antiphase arm swing angle) of the antiphase arm swing angle correcting perturbation model 203 is called a correcting perturbation model antiphase arm swing angle
15 θ_{ca} . The floor reaction force horizontal component generated by the perturbation model for correcting antiphase arm swing angle is called a perturbation model floor reaction force horizontal component for correcting antiphase arm swing angle F_a . F_a is zero as described
20 above. This means that the following equation always holds.

$$F_a = 0 \quad \dots \text{Equation a21c}$$

25 The antiphase arm swing angle correcting perturbation model 231 is expressed by a flywheel, as shown in Fig. 70. The inertia of the flywheel is the same as the flywheel

FH_{az} of the aforesaid simplified model (the model with 3 mass points + flywheels) shown in Fig. 12. The rotational angle of the flywheel of the antiphase arm swing angle correcting perturbation model 231 corresponds to the
5 correcting perturbation model antiphase arm swing angle θ_{ca} , and the floor reaction force moment vertical component generated by the flywheel corresponds to the perturbation model moment for correcting antiphase arm swing angle M_a .

10 The antiphase arm swing angle correcting perturbation model 231 expresses a relationship between the floor reaction force moment perturbation ΔM_z and the antiphase arm swing angle perturbation $\Delta \theta_{az}$ in the aforesaid Equation 03z of the dynamic equation of the aforesaid
15 simplified model (the model with 3 mass points + flywheels).

Accordingly, if parameters other than M_z and θ_{az} are regarded as constants, and if the relationship between the floor reaction force moment perturbation ΔM_z and the
20 antiphase arm swing angle perturbation $\Delta \theta_{az}$ is determined according to Equation 03z, then the following equation will be obtained.

$$\Delta M_z = J_{az} * d^2 \Delta \theta_{az} / dt^2 \quad \dots \text{Equation a22c}$$

25 Associating ΔM_z of Equation a22c with the perturbation model moment for correcting antiphase arm

swing angle Ma , and associating $\Delta\theta_{az}$ with the correcting perturbation model antiphase arm swing angle θ_{ca} provide the following equation.

5 $Ma = J_{az} * d^2\Delta\theta_{ca}/dt^2$... Equation a23c

 In other words, the antiphase arm swing angle correcting perturbation model 231 is represented by equation a23c. The perturbation model floor reaction
10 force horizontal component for correcting antiphase arm swing angle Fr is determined according to Equation a21c as described above ($Fa = 0$).

 As it will be discussed later, in S3536, a corrected
15 gait (to be more specific, a desired instantaneous value with some instantaneous values of a simplified model gait corrected) are eventually generated (output). A desired body posture inclination angle of the corrected gait
 (hereinafter referred to as the corrected desired body
20 posture inclination angle) is obtained by adding the aforesaid correcting perturbation model body posture inclination angle θ_c (the value determined in the control cycle at the current time t) to the instantaneous value of the aforesaid determined simplified model body posture
25 inclination angle (the instantaneous value of the desired body posture inclination angle at the current time t of the current time gait determined in S3532) by a calculator

204. The desired horizontal body position of the corrected gait (hereinafter referred to as the corrected desired horizontal body position) is obtained by adding the correcting perturbation model horizontal body position X_c (the value determined in the control cycle at the current time t) to the instantaneous value of the aforesaid determined simplified model horizontal body position (the instantaneous value of the desired horizontal body position at the current time t of the current time gait determined in S3532) by a calculator 205. Further, a desired antiphase arm swing angle of a corrected gait (hereinafter referred to as the corrected desired antiphase arm swing angle) is obtained by adding the correcting perturbation model antiphase arm swing angle θ_{ca} (the value determined in the control cycle at the current time t) to the instantaneous value of the aforesaid determined simplified model antiphase arm swing angle (the instantaneous value of the desired antiphase arm swing angle at the current time t of the current time gait determined in S3532) by a calculator 232.

The desired floor reaction force of the corrected gait is also corrected. Specifically, the floor reaction force moment horizontal component about the desired ZMP is no longer zero, and the desired floor reaction force moment horizontal component for compliance control is output as a desired value. Further, the desired floor reaction force horizontal component is also corrected to a

corrected desired floor reaction force horizontal
component and output. In addition, the desired floor
reaction force moment vertical component is corrected to a
corrected desired floor reaction force moment vertical
5 component and output.

As described above, the motion of the corrected gait
is the motion obtained by adding (combining) the motions
of perturbation models (to be more specific, the motions
of the horizontal body position correcting perturbation
10 model 202 and the body posture inclination angle
correcting perturbation model 203 and the motion of the
antiphase arm swing angle correcting perturbation model
231) to the motion of a simplified model gait.

In general, the floor reaction force generated by a
15 motion obtained by adding a certain perturbative motion to
a certain reference motion is approximated by the sum of
the floor reaction force generated by the reference motion
(the floor reaction force counterbalancing the gravity and
the inertial force generated by the motion) and the
20 perturbational portion of the floor reaction force
generated by the perturbative motion.

Considering that the floor reaction force horizontal
component generated by the body inclination mode, the
floor reaction force moment vertical component generated
25 by the body inclination mode, the floor reaction force
horizontal component generated by the antiphase arm swing
mode, and the floor reaction force moment horizontal

component generated by the antiphase arm swing mode are all zero, the three equations given below must be satisfied in order for the result, which is obtained by adding the compensating total floor reaction force moment horizontal component M_{dmdxy} to the floor reaction force moment that balances with the motion of a corrected gait on the inverse full model 201, to agree with a corrected desired floor reaction force moment (to satisfy the condition of A1 described above).

10

Full-model floor reaction force moment horizontal component M_{fullxy}
+ Perturbation model moment for correcting horizontal body position M_p
+ Perturbation model moment for correcting body posture inclination angle M_r
+ Compensating total floor reaction force moment horizontal component M_{dmdxy}
= Corrected desired floor reaction force moment horizontal component

15

20

... Equation h5

Full-model floor reaction force horizontal component F_{full}
+ Perturbation model floor reaction force horizontal component for correcting horizontal body position F_p
= Corrected desired floor reaction force horizontal

25

component

... Equation h6

Full-model floor reaction force moment vertical

5 component Mfullz

+ Perturbation model moment vertical component for

correcting horizontal body position Mpz

+ Perturbation model moment vertical component for

correcting antiphase arm swing angle Maz

10 = Corrected desired floor reaction force moment vertical
component

... Equation h1006

where the perturbation model moment vertical

component for correcting horizontal body position Mpz

15 denotes the floor reaction force moment vertical component
generated on the inverse full model 201 by a motion of the
perturbation model for correcting horizontal body position.
The moments of Equation h5 and Equation h1006 are the
moments about an original (simplified model's) desired ZMP.

20 The true ZMP of a corrected gait is changed to a
point deviated from the desired ZMP (ideal desired ZMP) of
a simplified model gait by the value obtained by dividing
a corrected desired floor reaction force moment by a
desired floor reaction force vertical component.

25

True ZMP of corrected gait = Desired ZMP

+ Corrected desired floor reaction force moment /

Desired floor reaction force vertical component

... Equation h7

To calculate the component in the X direction
(longitudinal direction) of the true ZMP of a corrected
gait, the component about the Y-axis (lateral axis) of a
corrected desired floor reaction force moment is used.
Further, to calculate the component in the Y direction of
the true ZMP of a corrected gait, the component about the
X-axis (longitudinal axis) of a corrected desired floor
reaction force moment is used. However, when calculating
the component in the Y direction of the true ZMP of a
corrected gait, "+" of the right side of Equation h7 must
be changed to "-".

Supplementally, a corrected desired floor reaction
force moment vertical component about the true ZMP of a
corrected gait may be calculated, as an alternative.

The corrected desired floor reaction force moment
vertical component about the true ZMP of a corrected gait
will be the outcome obtained by adding the outer product
of the difference between the true ZMP of a corrected gait
and a desired ZMP and the corrected desired floor reaction
force horizontal component determined according to
Equation h6 to the moment about an original desired ZMP.

The true ZMP of the corrected gait determined
according to Equation h7 must fall within a ZMP
permissible range. This is called a ZMP restriction

condition.

The corrected desired floor reaction force horizontal component must fall within a floor reaction force horizontal component permissible range for correcting gait (for full-model correction). This is called a floor reaction force horizontal component restriction condition.

The corrected desired floor reaction force moment vertical component must fall within a floor reaction force moment vertical component permissible range for correcting gait (for full-model correction). This is called a floor reaction force moment vertical component restriction condition.

As described above, a corrected gait must satisfy Equation h5, Equation h6, Equation h1006, the ZMP restriction condition (the condition of a range in which the true ZMP of the corrected gait obtained from Equation h7 exists), the floor reaction force horizontal component restriction condition, and the floor reaction force moment vertical component restriction condition.

However, merely satisfying these equations and conditions would cause divergence of the aforesaid correcting perturbation model body position, the aforesaid correcting perturbation model body posture inclination angle, and the aforesaid correcting perturbation model antiphase arm swing angle.

Therefore, on the basis of the state amounts of the aforesaid horizontal body position correcting perturbation

model 202, the aforesaid body posture inclination angle
correcting perturbation model 203, and the aforesaid
antiphase arm swing angle correcting perturbation model
231 (to be more specific, correcting perturbation model's
5 horizontal body position/velocity, correcting perturbation
model's body posture inclination angle/angular velocity,
and correcting perturbation model's antiphase arm swing
angle/angular velocity, etc.), the stabilization control
of the correcting perturbation models 202, 203, and 231 is
10 conducted so as to converge (stabilize) these state
amounts to predetermined states.

First, the stabilization control of the horizontal
body position correcting perturbation model 202 will be
explained in detail.

15 The control law for converging (stabilizing) the
horizontal body position correcting perturbation model 202
to a desired steady position is referred to as a
perturbation model control law 206 for correcting
horizontal body position, and the feedback amount
20 (manipulated variable) determined by this control law is
referred to as a required value M_{pfdmd} of perturbation
model stabilization moment for correcting horizontal body
position. The term "required value" has been added
because restriction is added to the value determined
25 according to the above control law to correct it such that
the true ZMP exits in the aforesaid ZMP permissible range
and the floor reaction force horizontal component falls

within a floor reaction force horizontal component
permissible range, as it will be discussed hereinafter.
The moment corrected by adding restriction thereto is
referred to as the horizontal body position correcting
5 perturbation model stabilization moment M_{pf} .

Specifically, the perturbation model control law 206
for correcting horizontal body position uses Equation h10.
However, a desired steady position is given by Equation h8.
Further, m_{total} denotes the total weight of the aforesaid
10 robot, m_b denotes the mass of the aforesaid body mass
point (the mass of the inverted pendulum), and X_{Gf} denotes
the center-of-gravity horizontal position calculated using
a full model on the basis of an instantaneous posture of a
simplified model gait, that is, the center-of-gravity
15 horizontal position calculated by the aforesaid inverse
full model. Further, K_{pp} and K_{pv} denote the gains of
feedback control.

Desired steady position = $-m_{total}/m_b \cdot (X_{Gf} - X_{Gs})$

20 ... Equation h8

Required value M_{pfdmd} of perturbation model stabilizing
moment for correcting horizontal body position
= $K_{pp} \cdot (\text{Correcting perturbation model horizontal body}$
25 $\text{position } X_c - \text{Desired steady position})$
+ $K_{pv} \cdot \text{Correcting perturbation model horizontal body}$
velocity dX_c/dt

- Correcting perturbation model horizontal body position

$X_c \cdot \text{Body floor reaction force vertical component } F_{bz}$

... Equation h10

5 To determine the component about the X-axis
(longitudinal axis) of the required value M_{pfdmd} of
perturbation model stabilizing moment for correcting
horizontal body position, a correcting perturbation model
horizontal body position velocity and a desired steady
10 position use a component in the Y-axis direction (lateral
direction).

 To determine the component about the Y-axis (lateral
axis) of the required value M_{pfdmd} of perturbation model
stabilizing moment for correcting horizontal body position,
15 a correcting perturbation model horizontal body position
velocity and a desired steady position use a component in
the X-axis direction (longitudinal direction), and "-" in
the third term of the right side is replaced by "+".

 The details have been described in PCT/JP03/00435
20 previously proposed by the present applicant, so that
further explanation will be omitted.

 The stabilization control of the body posture
inclination angle correcting perturbation model 203 will
now be explained in detail.

25 According to the state of the body posture
inclination angle correcting perturbation model 203, a
feedback amount (manipulated variable) is determined

according to a feedback control law, such as the PI control, so that a corrected desired body posture inclination angle, that is, the inclination angle obtained by adding a correcting perturbation model body posture inclination angle to a desired body posture inclination angle based on a simplified model, stabilizes to or follows a reference body posture inclination angle (determined in S3404 of Fig. 57) output by the desired instantaneous value generator 100b or a desired body posture inclination angle (obtained in S3414 of Fig. 57) based on a simplified model, and the determined feedback amount is additionally input to the body posture inclination angle correcting perturbation model 203.

This control law is referred to as a body posture inclination angle correcting perturbation model control law 207 (abbreviated as the body posture angle correcting perturbation model control law 207 in some cases), and the feedback amount (manipulated variable) is referred to as a required value Mrfdmd of perturbation model stabilizing moment for correcting body posture inclination angle. The term "required value" has been added for the same reason as that for the required value Mpfdmd of perturbation model stabilizing moment for correcting horizontal body position. The moment corrected by adding restriction thereto is referred to as perturbation model stabilizing moment Mrf for correcting body posture inclination angle.

Specifically, the body posture inclination angle

correcting perturbation model control law 207 for
determining the required value M_{rfdmd} of perturbation
model stabilizing moment for correcting body posture
inclination angle is implemented according to the equation
5 given below.

Required value M_{rfdmd} of perturbation model stabilizing
moment for correcting body posture inclination angle
= $K_{rp} * (\text{Correcting perturbation model body posture}$
10 $\text{inclination angle } \theta_c$
- (Reference body posture inclination angle - Desired
body posture inclination angle based on simplified model))
+ $K_{rv} * \text{Correcting perturbation model body posture}$
inclination angular velocity $d\theta_c/dt$

15 ... Equation h11
where K_{rp} and K_{rv} denote feedback control gains.

In Equation h11, (Reference body posture inclination
angle - Desired body posture inclination angle based on
20 simplified model) may be replaced by zero.

The processing in S3536 will be explained by
referring back to the functional block diagram of Fig. 67.
As described above, the required value M_{pfdmd} of
perturbation model stabilization moment for correcting
25 horizontal body position is determined according to the
perturbation model control law 206 for correcting
horizontal body position (Equation h10). Further, the

required value M_{rfdmd} of perturbation model stabilization moment for correcting body posture inclination angle is determined according to the body posture inclination angle correcting perturbation model control law 207 (Equation h11).

Subsequently, an estimated (calculated) value F_0 of floor reaction force of the perturbation model for correcting body position when it is assumed that the horizontal body position correcting perturbation model stabilization moment M_{pf} is zero is determined by a F_0 calculator 208. As it will be discussed hereinafter, the full-model floor reaction force moment horizontal component M_{fullxy} to which the horizontal body position correcting perturbation model stabilization moment M_{pf} has been added is supplied to the horizontal body position correcting perturbation model 202. Hence, F_0 is the floor reaction force generated by the horizontal body position correcting perturbation model 202 if only the full-model floor reaction force moment horizontal component M_{fullxy} with a reversed sign is supplied to the horizontal body position correcting perturbation model 202.

Specifically, F_0 is determined according to the equation given below.

$$F_0 = m_b * \frac{d^2 X_c}{dt^2} - \frac{1}{h} * M_{pf} \quad \dots \text{Equation h12}$$

The first term of the right side denotes a floor

reaction force horizontal component of the horizontal body position correcting perturbation model 202 of the last time (time $t - \Delta t$).

The second term of the right side denotes the floor reaction force horizontal component directly generated in (i.e., a direct term of) the horizontal body position correcting perturbation model 202 by the horizontal body position correcting perturbation model stabilizing moment M_{pf} of the last time.

More specifically, the estimated value of the floor reaction force F_0 of a body position correcting perturbation model when it is assumed that M_{pf} is zero is determined by subtracting the value, which is obtained by dividing the horizontal body position correcting perturbation model stabilization moment M_{pf} of the last time by the body translational mode floor reaction force ratio h , from the value obtained by multiplying the body mass point horizontal acceleration of the last time of the horizontal body position correcting perturbation model 202 by the mass m_b of the body mass point.

Subsequently, if it is assumed that the horizontal body position correcting perturbation model stabilization moment M_{pf} is matched with the required value M_{pfdmd} of horizontal body position correcting perturbation model stabilization moment, the body posture inclination angle correcting perturbation model stabilization moment M_{rf} is matched with the required value M_{rfdmd} of body posture

inclination angle correcting perturbation model

stabilization moment, a desired floor reaction force

moment for compliance control as a desired floor reaction

force moment horizontal component about a desired ZMP is

5 matched with the total sum of the compensating total floor

reaction force moment horizontal component M_{dmdxy} , M_{pf} ,

and M_{rf} , while ignoring the aforesaid restriction (the

floor reaction force horizontal component restrictive

condition and the ZMP restrictive condition), then the

10 floor reaction force moment horizontal component M_{in}

generated about the desired ZMP is determined by a M_{in}

calculator 209. This floor reaction force moment

horizontal component is referred to as a corrected desired

floor reaction force moment horizontal component without

15 restriction M_{in} . The corrected desired floor reaction

force moment horizontal component without restriction M_{in}

is determined according to the following equation.

$$M_{in} = M_{pfdmd} + M_{rfdmd} + M_{dmdxy} \quad \dots \text{Equation h13}$$

20

This means that the corrected desired floor reaction

force moment horizontal component without restriction M_{in}

is obtained by adding the required value M_{pfdmd} of

horizontal body position correcting perturbation model

25 stabilization moment, the required value M_{rfdmd} of body

posture inclination angle correcting perturbation model

stabilization moment, and the compensating total floor

reaction force moment horizontal component M_{dmdxy} .

Subsequently, if it is assumed that the horizontal
body position correcting perturbation model stabilization
moment M_{pf} is matched with the required value M_{pfdmd} of
5 horizontal body position correcting perturbation model
stabilization moment, the body posture inclination angle
correcting perturbation model stabilization moment M_{rf} is
matched with the required value M_{rfdmd} of body posture
inclination angle correcting perturbation model
10 stabilization moment, and a desired floor reaction force
moment for compliance control is matched with the total
sum of the compensating total floor reaction force moment
horizontal component M_{dmdxy} , M_{pf} , and M_{rf} , while ignoring
the aforesaid restriction (the floor reaction force
15 horizontal component restrictive condition and the ZMP
restrictive condition), then the floor reaction force
horizontal component F_{in} to be generated is determined by
a F_{in} calculator 210. This floor reaction force
horizontal component is referred to as a corrected desired
20 floor reaction force horizontal component without
restriction F_{in} .

The corrected desired floor reaction force horizontal
component is obtained by the above Equation h6. As
described above, no floor reaction force horizontal
25 component is generated in the body posture inclination
angle correcting perturbation model 203 by a behavior of
the body posture inclination angle correcting perturbation

model 203, meaning that F_r is zero. Accordingly, the corrected desired floor reaction force horizontal component without restriction F_{in} is obtained by adding the floor reaction force horizontal component, which is increased by changing the horizontal body position correcting perturbation model stabilization moment M_{pf} from zero to the required value M_{pfdmd} of horizontal body position correcting perturbation model stabilization moment, to the corrected desired floor reaction force horizontal component in a case where it is assumed that the horizontal body position correcting perturbation model stabilization moment M_{pf} is zero.

Incidentally, the floor reaction force horizontal component, which is increased by changing the horizontal body position correcting perturbation model stabilization moment M_{pf} from zero to the required value M_{pfdmd} of horizontal body position correcting perturbation model stabilization moment, takes a value obtained by dividing the required value M_{pfdmd} of horizontal body position correcting perturbation model stabilization moment by the body translational mode floor reaction force ratio h .

Hence, as shown by Equation h15, the corrected desired floor reaction force horizontal component F_{in} without restriction is obtained by adding the aforesaid determined full-model floor reaction force horizontal component F_{full} to the value obtained by dividing the required value M_{pfdmd} of horizontal body position

correcting perturbation model stabilization moment by the
body translational mode floor reaction force ratio h , and
further by adding the calculated value F_0 of the floor
reaction force of the body position correcting

5 perturbation model when it is assumed that the horizontal
body position correcting perturbation model stabilization
moment M_{pf} is zero.

$$F_{in} = 1/h * M_{pfdmd} + F_{full} + F_0 \quad \dots \text{Equation h15}$$

10

Subsequently, based on the corrected desired floor
reaction force moment horizontal component without
restriction M_{in} and the corrected desired floor reaction
force horizontal component without restriction F_{in} , a
15 corrected desired floor reaction force moment horizontal
component with restriction M_{ltd} and a corrected desired
floor reaction force horizontal component with restriction
 F_{ltd} (about a desired ZMP), which are the values that have
added restriction thereto, are determined by a restricting
20 means (restriction processing unit) 211. In the present
embodiment, a desired floor reaction force moment
horizontal component for compliance control agrees with
the corrected desired floor reaction force moment
horizontal component with restriction M_{ltd} , and the floor
25 reaction force horizontal component of a corrected gait
agrees with a corrected desired floor reaction force
horizontal component with restriction F_{ltd} .

The corrected desired floor reaction force moment horizontal component with restriction M_{ltd} and the corrected desired floor reaction force horizontal component with restriction F_{ltd} are determined such that the true ZMP of the corrected gait (including the desired floor reaction force moment horizontal component for compliance control) falls within the aforesaid ZMP permissible range and the floor reaction force horizontal component of the corrected gait falls within a floor reaction force horizontal component permissible range. In other words, M_{ltd} and F_{ltd} are determined such that the ZMP restrictive condition and the floor reaction force horizontal component restrictive condition are satisfied.

Furthermore, under the aforesaid restrictive condition, a horizontal body position correcting perturbation model stabilization moment M_p is determined to agree with or approximate to the required value M_{pfdmd} of horizontal body position correcting perturbation model stabilization moment as much as possible. Similarly, a body posture inclination angle correcting perturbation model stabilization moment M_r is determined to be a value that agrees with or approximate to the required value M_{rfdmd} of body posture inclination angle correcting perturbation model stabilization moment as much as possible. This stabilizes the aforesaid correcting perturbation model body position X_c and the aforesaid correcting perturbation model body posture inclination

angle θ_c , thus preventing divergence.

The details of the restricting means (restriction processing unit) 211 are given in PCT/JP03/00435 previously proposed by the present applicant, so that
5 further explanation will be omitted herein.

Subsequently, according to the following equation, the horizontal body position correcting perturbation model stabilization moment M_{pf} and the body posture inclination angle correcting perturbation model stabilization moment
10 M_{rf} are determined by an M_{pf} calculator 212 and an M_{rf} calculator 213, respectively.

$$M_{pf} = (F_{ltd} - F_{full} - F_0) * h \quad \dots \text{Equation h20}$$

$$M_{rf} = M_{ltd} - M_{pf} - M_{dmdxy} \quad \dots \text{Equation h21}$$

15

More specifically, the M_{pf} calculator 212 multiplies the value, which is obtained by subtracting the full-model floor reaction force horizontal component F_{full} from the corrected desired floor reaction force horizontal
20 component with restriction F_{ltd} and subtracting therefrom the calculated value F_0 of the floor reaction force of the body position correcting perturbation model 202 in the case where M_p is assumed to be zero, by the body translational mode floor reaction force ratio h so as to
25 obtain the horizontal body position correcting perturbation model stabilization moment M_{pf} . The M_{rf} calculator 213 subtracts the aforesaid horizontal body

position correcting perturbation model stabilization
moment M_{pf} and the compensating total floor reaction force
moment horizontal component M_{dmdxy} from the corrected
desired floor reaction force moment horizontal component
5 with restriction M_{ltd} about the desired ZMP to obtain the
body posture inclination angle correcting perturbation
model stabilization moment M_{rf} .

Subsequently, according to the equations shown below,
the horizontal body position correcting perturbation model
10 floor reaction force moment M_p and the body posture
inclination angle correcting perturbation model floor
reaction force moment M_r are determined.

$$M_p = M_{pf} - M_{full} \quad \dots \text{Equation h22}$$

15 $M_r = M_{rf} \quad \dots \text{Equation h23}$

This means that an M_p calculator 214 subtracts a
full-model floor reaction force moment horizontal
component M_{fullxy} from the horizontal body position
20 correcting perturbation model stabilizing moment M_{pf} to
obtain the horizontal body position correcting
perturbation model floor reaction force moment M_p . The
body posture inclination angle correcting perturbation
model floor reaction force moment M_r takes the same value
25 as that of the body posture inclination angle correcting
perturbation model stabilization moment M_{rf} .

Subsequently, the horizontal body position correcting

perturbation model floor reaction force moment M_p is
supplied to the body position correcting perturbation
model 202 in which the correcting perturbation model body
position X_c balancing the supplied floor reaction force
5 moment is calculated.

Further, the body posture inclination angle
correcting perturbation model floor reaction force moment
 M_r is supplied to the body posture inclination angle
correcting perturbation model 203 in which the correcting
10 perturbation model body posture inclination angle θ_c
balancing the supplied floor reaction force moment
horizontal component is calculated.

Subsequently, calculators 205 and 204 determine a
corrected desired horizontal body position and a corrected
15 desired body posture inclination angle according to the
following Equation h24 and Equation h25, respectively, and
the determined values are output as the final desired
instantaneous values of the horizontal body
position/posture.

20

Corrected desired horizontal body position
= Simplified model horizontal body position + Corrected
perturbation model body position X_c

... Equation h24

25

Corrected desired body posture inclination angle
= Simplified model body posture inclination angle +

Corrected perturbation model body posture inclination
angle θ_c

... Equation h25

5 In other words, the correcting perturbation model
body position X_c is added to the simplified model
horizontal body position to obtain the corrected desired
horizontal body position, and this is output as a final
desired horizontal body position. The correcting
10 perturbation model body posture inclination angle θ_c is
added to the simplified model body posture inclination
angle to provide the corrected desired body posture
inclination angle, and this is output as a final desired
body posture inclination angle.

15 In addition, the corrected desired floor reaction
force moment horizontal component with restriction M_{ltd} is
output as a desired floor reaction force moment horizontal
component for compliance control about the desired ZMP,
and a corrected desired floor reaction force horizontal
20 component with restriction F_{ltd} is output as a corrected
desired floor reaction force horizontal component.

 More specifically, according to Equation h26 and
Equation h27 shown below, the corrected desired floor
reaction force horizontal component and the corrected
25 desired floor reaction force moment horizontal component
about the desired ZMP are determined as the final desired
instantaneous values of the floor reaction force

horizontal component and the floor reaction force moment
horizontal component (the moment horizontal component
about the desired ZMP), respectively, and these are output.

5 Desired floor reaction force moment horizontal component
for compliance control
= Corrected desired floor reaction force moment horizontal
component with restriction Mltd

... Equation h26

10

Corrected desired floor reaction force horizontal
component
= Corrected desired floor reaction force horizontal
component with restriction Fltd

15

... Equation h27

The processing up to the above in S3536 is as per
PCT/JP03/00435 by the present applicant, so that no
further explanation will be given.

20

Further, in the present embodiment, an antiphase arm
swing angle correcting perturbation model moment Ma and a
desired floor reaction force moment vertical component to
be input to the antiphase arm swing angle correcting
perturbation model 231 are determined in the antiphase arm
swing angle correcting perturbation model moment
25 determiner 230. Then, an antiphase arm swing angle
correcting perturbation model moment Ma is input to the

antiphase arm swing angle correcting perturbation model
231 to determine a correcting perturbation model antiphase
arm swing angle θ_{ca} .

Supplementally, the antiphase arm swing angle
5 correcting perturbation model moment determiner 230
determines a feedback amount (manipulated variable)
according to a feedback control law on the basis of the
state of the antiphase arm swing angle correcting
perturbation model 231, such as the PI control, so that a
10 corrected desired antiphase arm swing angle, that is, the
arm swing angle obtained by adding a correcting
perturbation model antiphase arm swing angle to a desired
antiphase arm swing angle based on a simplified model,
stabilizes to or follows a reference antiphase arm swing
15 angle (determined in S3404 of Fig. 57) output by the
desired instantaneous value generator 100b or a desired
antiphase arm swing angle (obtained in S3414 of Fig. 57)
based on a simplified model, and the determined feedback
amount is additionally input to the antiphase arm swing
20 angle correcting perturbation model 231.

This control law is referred to as an antiphase arm
swing angle correcting perturbation model control law, and
the feedback amount (manipulated variable) is referred to
as a required value M_{afdm} of perturbation model
25 stabilizing moment for correcting antiphase arm swing
angle. The term "required value" has been added for the
same reason as that for the required value M_{pfdm} of

perturbation model stabilizing moment for correcting horizontal body position. The moment corrected by adding restriction thereto is referred to as perturbation model stabilizing moment M_{af} for correcting antiphase arm swing angle. In the present embodiment, this M_{af} is supplied as an antiphase arm swing angle correcting perturbation model moment M_a to the antiphase arm swing angle correcting perturbation model 231.

Specifically, the antiphase arm swing angle correcting perturbation model control law for determining the required value M_{afdmd} of perturbation model stabilizing moment for correcting antiphase arm swing angle is implemented according to the equation given below.

Required value M_{afdmd} of perturbation model stabilizing moment for correcting antiphase arm swing angle
 $= K_{ap} * (\text{Correcting perturbation model antiphase arm swing angle } \theta_{ca}$

$- (\text{Reference antiphase arm swing angle} - \text{Desired antiphase arm swing angle based on simplified model}))$
 $+ K_{av} * \text{Correcting perturbation model antiphase arm swing angular velocity } d\theta_{ca}/dt$

... Equation h30

where K_{ap} and K_{av} denote feedback control law gains.

In Equation h30, $(\text{Reference antiphase arm swing angle} - \text{Desired antiphase arm swing angle based on simplified$

model) may be replaced by zero.

The operation of the antiphase arm swing angle
correcting perturbation model moment determiner 230 will
be explained in conjunction with Fig. 71 showing the
functional block diagram thereof.

First, as described above, the required value M_{afdm}
of perturbation model stabilizing moment for correcting
antiphase arm swing angle is determined according to the
antiphase arm swing angle correcting perturbation model
control law 230a (Equation h30).

Subsequently, a floor reaction force moment vertical
component perturbation amount M_{pz} resulting from the
correction of a horizontal body position using the
horizontal body position correcting perturbation model 202
is determined by a calculator 230b of a floor reaction
force moment vertical component perturbation amount
resulting from a correction of a horizontal body position.

Specifically, it is determined according to the
following equation.

$$\begin{aligned} M_{pz} = & (\text{Position of simplified model body mass point} \\ & + \text{Correcting perturbation model body position } X_c - \\ & \text{Desired ZMP}) \\ & * (\text{Simplified model body mass point horizontal} \\ & \text{acceleration} \\ & + \text{Correcting perturbation model body acceleration} \\ & d^2X_c/dt^2) \end{aligned}$$

- (Simplified model body mass point position -
Desired ZMP)

* (Simplified model body mass point horizontal
acceleration)

5 ... Equation h31

Alternatively, the following equation approximating
the above equation may be used.

$M_{pz} \approx$ Correcting perturbation model body position X_c

10 * (Simplified model body mass point horizontal
acceleration

+ Correcting perturbation model body
acceleration d^2X_c/dt^2)

+ (Simplified model body mass point position - Desired
15 ZMP)

* Correcting perturbation model body acceleration
 d^2X_c/dt^2)

... Equation h32

20 Subsequently, if it is assumed that the antiphase arm
swing angle correcting perturbation model stabilization
moment M_{af} is matched with the required value M_{afdm} of
antiphase arm swing angle correcting perturbation model
stabilization moment, and a desired floor reaction force
25 moment vertical component for compliance control as a
desired floor reaction force moment vertical component
about a desired ZMP is matched with a total sum of M_{af} ,

Mfullz, and Mpz, while ignoring the aforesaid restrictive condition on floor reaction force moment vertical component, then the floor reaction force moment vertical component Minz generated about the desired ZMP is
5 determined by a calculator 230c. This floor reaction force moment vertical component is referred to as a corrected desired floor reaction force moment vertical component without restriction Minz. The corrected desired floor reaction force moment vertical component without
10 restriction Minz is determined according to the following equation.

$$\text{Minz} = \text{Mafdm} + \text{Mfullz} + \text{Mpz} \quad \dots \text{Equation h33}$$

15 This means that the corrected desired floor reaction force moment vertical component without restriction Minz is obtained by adding the required value Mafdm of antiphase arm swing angle correcting perturbation model stabilization moment, the full-model floor reaction force
20 moment vertical component Mfullz, and the horizontal body position correcting perturbation model moment vertical component Mpz.

Subsequently, based on the corrected desired floor reaction force moment vertical component without
25 restriction Minz, a corrected desired floor reaction force moment vertical component with restriction Mltdz (about a desired ZMP), which is the value that has added

restriction thereto, is determined by a restricting means
(restriction processing unit) 230d. In the present
embodiment, a desired floor reaction force moment vertical
component for compliance control agrees with the corrected
5 desired floor reaction force moment vertical component
with restriction Mltdz.

The corrected desired floor reaction force moment
vertical component with restriction Mltdz is determined
such that it falls within a floor reaction force moment
10 vertical component permissible range. In other words,
Mltdz is determined so that it satisfies a floor reaction
force moment vertical component restrictive condition.

Furthermore, under the aforesaid floor reaction force
moment vertical component restrictive condition, the
15 antiphase arm swing angle correcting perturbation model
stabilization moment Maf is determined to agree with or be
as close as possible to the required value Mafdm of
antiphase arm swing angle correcting perturbation model
stabilization moment. This stabilizes the aforesaid
20 correcting perturbation model antiphase arm swing angle
 θ_{ca} , thus preventing divergence.

A restricting means (restriction processing unit)
230d is a function having a saturation characteristic
represented by the following equation.

25
If $Minz > \text{Upper limit value of a floor reaction force}$
moment vertical component permissible range, then

Mltdz = Upper limit value of the floor reaction force moment vertical component permissible range.

If Minz < Lower limit value of a floor reaction force moment vertical component permissible range, then

5 Mltdz = Lower limit value of the floor reaction force moment vertical component permissible range.

If the lower value of a floor reaction force moment vertical component permissible range \leq Minz, and Minz \leq Upper limit value of the floor reaction force moment vertical component permissible range, then

10

$$Mltdz = Minz$$

..... Equation h34

Subsequently, according to the equation shown below, an antiphase arm swing angle correcting perturbation model moment Ma (= Antiphase arm swing angle correcting perturbation model stabilization moment Maf) is determined by a Maf calculator 230e.

15

20 $Ma = Mltdz - (Mfullz + Mpz)$... Equation h35

This means that in the Maf calculator 230e, an antiphase arm swing angle correcting perturbation model moment Ma as the antiphase arm swing angle correcting perturbation model stabilization moment Maf is obtained by subtracting the full-model floor reaction force moment vertical component Mfullz and the horizontal body position

25

correcting perturbation model moment vertical component
Mpz from the corrected desired floor reaction force moment
vertical component with restriction Mltdz.

5 Meanwhile, the corrected desired floor reaction force
moment vertical component with restriction Mltd is output
as the desired floor reaction force moment vertical
component for compliance control about a desired ZMP.

10 More specifically, according to the following
Equation h35, a corrected desired floor reaction force
moment vertical component about the desired ZMP is
determined as the final desired instantaneous value of the
floor reaction force moment vertical component (the moment
vertical component about the desired ZMP), these are
output.

15

Desired floor reaction force moment vertical component for
compliance control
= Corrected desired floor reaction force moment vertical
component with restriction Mltdz

20

... Equation h36

25 After the processing of the antiphase arm swing angle
correcting perturbation model moment determiner 230 is
carried out as described above, the antiphase arm swing
angle correcting perturbation model moment Ma is supplied
to the antiphase arm swing angle correcting model 231
shown in Fig. 67, and the correcting perturbation model

antiphase arm swing angle θ_{ca} that balances with the supplied antiphase arm swing angle correcting perturbation model moment M_a is calculated by using Equation a23c (by integrating).

5 Subsequently, in the calculator 232, the corrected desired antiphase arm swing angle is determined according to the following Equation h37, and this is output as the final desired instantaneous value of the antiphase arm swing angle.

10

Corrected desired antiphase arm swing angle
= Simplified model antiphase arm swing angle
+ Correcting perturbation model antiphase arm swing angle
 θ_{ca}

15

... Equation h37

This means that the corrected desired antiphase arm swing angle is obtained by adding the correcting perturbation model antiphase arm swing angle θ_{ca} to the
20 simplified model antiphase arm swing angle, and this is output as the final desired antiphase arm swing angle.

The gait correction of S3536 is made as described above.

25 Supplementally, the present embodiment is the feedforward type correction, and the perturbation dynamic models are not precise models. For this reason, even if gaits are corrected so as to satisfy Equation h5, Equation

h6, and Equation h1006, as described above, dynamic balance conditions are not satisfied in the strict sense although the dynamic balance conditions are approximately satisfied.

5 Furthermore, in the present embodiment, at the end of a one-step gait (the end of the current time gait), for example, the state amounts of the horizontal body position correcting perturbation model 202, the body posture inclination angle correcting perturbation model 203, and
10 the antiphase arm swing angle correcting perturbation model 231, e.g., the horizontal position of the body mass point (the inverted pendulum mass point) of the horizontal body position correcting perturbation model 202, the rotational angle of the flywheel of the body posture
15 inclination angle correcting perturbation model 203, and the rotational angle of the flywheel of the antiphase arm swing angle correcting perturbation model 231, are added as the state amount of the simplified model 200. In other words, the state amount of the simplified model 200 at the
20 end of the current time gait is corrected to the state amount obtained by adding the body motion of the horizontal body position correcting perturbation model 202 and the state amounts of the body posture inclination angle correcting perturbation model 203 and the antiphase
25 arm swing angle correcting perturbation model 231. Further, the state amount of each of the perturbation models 202, 203, and 231 is initialized (e.g., the

horizontal position of the body mass point (the inverted pendulum mass point) of the horizontal body position correcting perturbation model 202, the rotational angle of the flywheel of the body posture inclination angle correcting perturbation model 203, and the rotational angle of the flywheel of the antiphase arm swing angle correcting perturbation model 231 are reset to zero). Then, a next time gait is generated, taking the state amount of the simplified model 200 that has been corrected as described above as the initial value of the next time gait, and the correcting perturbation model horizontal body position X_c , the correcting perturbation model body posture inclination angle θ_c , and the correcting perturbation model antiphase arm swing angle θ_{ca} of the individual perturbation models 202, 203, and 231 are calculated. This makes it possible to further enhance the stability of the behaviors of the individual perturbation models 202, 203, and 231. The state amounts of the simplified model 200 described above may be corrected as necessary while a gait is being generated. Conversely, the correction of the state amounts of the simplified model 200 or the resetting of the perturbation models described above may not be carried out while a gait is being generated.

The aforesaid correction of state amounts of the simplified model 200 will be implemented in the same manner in second and third embodiments, which will be

discussed hereinafter.

The present embodiment satisfies all the restoring conditions except for the aforementioned restoring condition 3). In this case, M_{dmdz} is not supplied to the gait generating device 100 in the present embodiment, so that restoring condition 3') below is satisfied instead of restoring condition 3).

Restoring condition 3') A floor reaction force moment vertical component of a corrected gait (this corresponds to a desired floor reaction force moment vertical component for compliance control) does not exceed a floor reaction force moment vertical component permissible range.

Furthermore, in addition to the operations and advantages of the third reference example, the calculation volume can be reduced to be relatively small when determining a horizontal body position, a body posture inclination angle, and an antiphase arm swing angle so as to satisfy the aforementioned restoring conditions 1, 2, 3', and 4 to 7.

The first embodiment explained above provides the embodiments of the first to the third inventions, the fifth to the eighth inventions, and the eleventh to the thirteenth inventions. In this case, the floor reaction force moment vertical component in the first embodiment corresponds to a control object amount. Further, the floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$ for generating a gait (for full-model

correction) in the first embodiment corresponds to the permissible range of the amount to be limited. Further, a motional component of a simplified model gait corresponds to a provisional instantaneous value of a desired motion, and the provisional instantaneous value corrected in S3536 corresponds to the instantaneous value of the desired motion. A full model (including an antiphase arm swing angle correcting perturbation model) corresponds to the dynamic model in the invention. And the aforesaid antiphase arm swing angle correcting perturbation model moment M_a corresponds to a perturbation model manipulated variable in the third invention and the correcting perturbation model antiphase arm swing angle θ_{ca} corresponds to the correction amount of a desired motion in the third invention. Further, the corrected desired floor reaction force moment vertical component without restriction M_{inz} in the first embodiment corresponds to an estimated value of a restriction object amount in the seventh invention, and the antiphase arm swing angle correcting model stabilization moment M_{afdm} corresponds to the required value of a perturbation model manipulated variable. The full-model floor reaction force moment vertical component M_{fullz} in the first embodiment to which the floor reaction force moment vertical component M_{pz} resulting from the correction of a horizontal body position has been added corresponds to the instantaneous value of a model restriction object amount.

In the first embodiment, Mafdm does not steadily become zero; however, if this is steadily set to zero, then an embodiment of the fourth invention of the present invention will be constructed.

5

A second embodiment of the present invention will now be explained with reference to Fig. 72 and Fig. 73. The correcting technique of a device according to the second embodiment differs from that of the aforesaid first
10 embodiment only in the processing of the gait generating device 100 (the processing of S3536 of Fig. 66), and it is a full-model feedback correction type. It is a technique that uses an inverse dynamic full model (inverse full model), does not correct an input of a simplified model
15 gait, and uses a perturbation model.

Fig. 72 is a functional block diagram explaining an operation of the device according to the second embodiment, specifically, the gait correcting technique of S3536 of the flowchart of Fig. 66. However, a simplified model 200
20 shown in Fig. 72 represents not only a dynamic model but also the processing from S3510 to S3532 of Fig. 66, i.e., the processing for calculating (determining) a simplified model gait instantaneous value, as in the case of the aforesaid first embodiment. Hence, in Fig. 72, the
25 portion beyond the simplified model 200 corresponds to the processing of S3536. Of the functional portions in Fig. 72, like functional portions as those in Fig. 67 according

to the first embodiment will be assigned like reference marks in Fig. 67 and detailed explanation thereof will be omitted.

Since the construction other than the processing of S3536 is the same as that of the third embodiment, the explanation thereof will be omitted, and the following will explain the processing of S3536 in detail in conjunction with Fig. 72.

In S3536, first, as previously described, a correcting perturbation model horizontal body position X_c , which will be discussed later, calculated at the last time control cycle (time $t - \Delta t$) is added by a calculator 205 to an instantaneous value of a desired horizontal body position of a simplified model gait determined in S3532 of Fig. 66, thereby determining a final desired horizontal body position (corrected desired horizontal body position). Further, a correcting perturbation model body posture inclination angle θ_c , which will be discussed later, calculated at the last time control cycle (time $t - \Delta t$) is added by a calculator 204 to an instantaneous value (a provisional instantaneous value determined in the control cycle at current time t) of a desired body posture inclination angle of a simplified model gait determined in S3532 of Fig. 66, thereby determining a final desired body posture inclination angle (corrected desired body posture inclination angle). Further, a correcting perturbation model antiphase arm swing angle θ_{ca} , which will be

discussed later, calculated at the last time control cycle
(time $t - \Delta t$) is added by a calculator 232 to an
instantaneous value (provisional instantaneous value
determined in the control cycle at current time t) of a
5 desired antiphase arm swing angle of a simplified model
gait determined in S3532 of Fig. 66, thereby determining a
final desired antiphase arm swing angle (corrected desired
antiphase arm swing angle).

Then, these corrected desired horizontal body
10 position, corrected desired body posture inclination angle,
and corrected desired antiphase arm swing angle are output
as the final desired instantaneous values of the
horizontal body position, the body posture inclination
angle, and the antiphase arm swing angle, respectively.

15 More specifically, the corrected desired horizontal
body position, the corrected desired body posture
inclination angle, and the corrected desired antiphase arm
swing angle are determined according to the aforesaid
Equation h24, Equation h25, and Equation h37.

20 Subsequently, the desired horizontal body position
(the corrected desired horizontal body position), the
desired body posture inclination angle (the corrected
desired body posture inclination angle), and the desired
antiphase arm swing angle (the corrected desired antiphase
25 arm swing angle) obtained by correcting the simplified
model gait as described above, and the instantaneous
values of the motional variables, such as the desired

center-of-gravity position, the desired foot position/posture, and the desired arm posture, of the simplified model gait obtained as previously described, and the instantaneous value of the desired ZMP are input
5 to the aforesaid inverse dynamic full model 201, and then the floor reaction force horizontal component and the floor reaction force moment about the desired ZMP (a horizontal component and a vertical component) that balance with the motion expressed by the input motional
10 variables (i.e., that are generated by the inverse full model 201 by the motion) are calculated. Thus, according to the present embodiment, in addition to the simplified model horizontal body position, body posture inclination angle, and antiphase arm swing angle, the correcting
15 perturbation model horizontal body position X_c , the correcting perturbation model body posture inclination angle θ_c , and a correcting perturbation model antiphase arm swing angle θ_{ca} are also input to the inverse full model 201. Hereinafter, as in the first embodiment, the
20 floor reaction force horizontal component, the floor reaction force moment horizontal component, and the floor reaction force moment vertical component calculated by the inverse full model 201 will be referred to as a full-model floor reaction force horizontal component F_{fullxy} , a full-
25 model floor reaction force moment horizontal component M_{fullxy} , and a full-model floor reaction force moment vertical component M_{fullz} .

The full-model floor reaction force horizontal component F_{full} is output as a corrected desired floor reaction force horizontal component (a final desired instantaneous value of the floor reaction force horizontal component at the current time t).

More specifically, a corrected desired floor reaction force horizontal component is determined according to the equation given below and output.

Corrected desired floor reaction force horizontal component = Full-model floor reaction force horizontal component F_{full}

... Equation h48

As can be seen from the above processing, according to the present embodiment, a full-model corrected gait is constituted by adding a behavior of the horizontal body position correcting perturbation model 202, a behavior of the body posture inclination angle correcting perturbation model 203, and a behavior of the antiphase arm swing angle correcting perturbation model 231 to a simplified model gait. Further, the equation shown below holds, considering that the floor reaction force horizontal component generated by the body inclination mode and the floor reaction force horizontal component generated by the antiphase arm swing mode are both zero. However, a simplified model floor reaction force horizontal component

is the translational force horizontal component of the floor reaction force generated by a motion of a simplified model gait, the floor reaction force being calculated using the inverse full model 201.

5

Full-model floor reaction force horizontal component F_{full}
= Simplified model floor reaction force horizontal
component

+ Horizontal body position correcting perturbation model
10 floor reaction force horizontal component F_p

... Equation h51

Subsequently, a required value M_{pfdmd} of horizontal
body position correcting perturbation model stabilization
15 moment is determined according to a horizontal body
position correcting perturbation model control law 206.
The horizontal body position correcting perturbation model
control law 206 in the present embodiment is set as
proposed by the present applicant in Japanese Patent
20 Application No. 2001-133621. For example, the control law
206 is determined according to the following equation.

Required value M_{pfdmd} of horizontal body position
correcting perturbation model stabilization moment
25 = $K_{pg} * \text{Difference in center of gravity} + K_{vg} * \text{Correcting perturbation model horizontal body velocity}$
 dX_c/dt

Equation h52

where the difference in center of gravity is determined according to the following equation.

5 Difference in center of gravity = Horizontal position of
full-model center of gravity - Horizontal position of
simplified model center of gravity

... Equation h53

10 where Kpg and Kvg in Equation h52 denote the gains of
a feedback control law, the horizontal position of full-
model center of gravity, the horizontal position of
simplified model center of gravity, and the correcting
perturbation model horizontal body velocity dX_c/dt are the
horizontal position of the center of gravity of a full-
15 model gait instantaneous value, the horizontal position of
the center of gravity of a simplified model gait
instantaneous value (a center-of-gravity horizontal
position XG_s calculated using a simplified model on the
basis of an instantaneous posture of a simplified model
20 gait), and a correcting perturbation model horizontal body
velocity dX_c/dt , respectively, which are calculated last
time (time $t - \Delta t$), as it will be discussed later.

More specifically, a perturbation model control
feedback amount (manipulated variable) is calculated on
25 the basis of the difference in center of gravity obtained
by subtracting the center-of-gravity horizontal position
of a simplified model from the center-of-gravity

horizontal position of a full model and a perturbation
model body velocity, which is one of the state amounts of
a perturbation model. Such a perturbation model control
law makes it possible to control the temporal average
5 value of the difference in center of gravity to
substantially zero.

Subsequently, a required value M_{rfdmd} of a body
posture correcting perturbation model stabilization moment
is determined according to a body posture inclination
10 angle correcting perturbation model control law 207. For
this purpose, the same control law as that in the first
embodiment may be used. Thus, as the control law 207, the
aforesaid Equation h11, for example, may be used.

Subsequently, a corrected desired floor reaction
15 force moment without restriction M_{in} is determined
(estimated) by a M_{in} calculator 209. As in the first
embodiment, the corrected desired floor reaction force
moment without restriction M_{in} is the floor reaction force
moment horizontal component generated about a desired ZMP
20 when a horizontal body position correcting perturbation
model stabilization moment M_{pf} is matched with the
required value M_{pfdmd} of horizontal body position
correcting perturbation model stabilization moment, a body
posture inclination angle correcting perturbation model
25 stabilization moment M_{rf} is matched with the required
value M_{rfdmd} of body posture inclination angle correcting
perturbation model stabilization moment, and a desired

floor reaction force moment horizontal component for compliance control as a desired floor reaction force moment about a desired ZMP is matched with the total sum of a compensating total floor reaction force moment

5 horizontal component M_{dmdxy} , M_{pf} , and M_{rf} , while ignoring the aforesaid restriction (the ZMP restrictive condition and the floor reaction force horizontal component restrictive condition).

A corrected desired floor reaction force moment
10 horizontal component without restriction M_{in} is determined by the calculation according to the aforesaid Equation h13, as in the first embodiment. More specifically, the corrected desired floor reaction force moment horizontal component without restriction M_{in} is obtained by adding
15 the required value M_{pfdmd} of horizontal body position correcting perturbation model stabilization moment, the required value M_{rfdmd} of body posture inclination angle correcting perturbation model stabilization moment, and the total sum of a compensating total floor reaction force
20 moment horizontal component M_{dmdxy} .

Furthermore, a corrected desired floor reaction force horizontal component without restriction F_{in} is also determined (estimated) by a F_{in} calculator 210. As in the first embodiment, the corrected desired floor reaction
25 force horizontal component without restriction F_{in} is the floor reaction force horizontal component (corresponding to F_{full}) generated by the inverted full model 201 when

the horizontal body position correcting perturbation model
stabilization moment M_{pf} is matched with the required
value M_{pfdmd} of horizontal body position correcting
perturbation model stabilization moment, the body posture
5 inclination angle correcting perturbation model
stabilization moment M_{rf} is matched with the required
value M_{rfdmd} of body posture inclination angle correcting
perturbation model stabilization moment, and the desired
floor reaction force moment horizontal component for
10 compliance control is matched with the total sum of the
compensating total floor reaction force moment horizontal
component M_{dmdxy} , M_{pf} , and M_{rf} , while ignoring the
aforesaid restriction (the ZMP restrictive condition and
the floor reaction force horizontal component restrictive
15 condition).

Unlike the first embodiment, the corrected desired
floor reaction force horizontal component without
restriction F_{in} is determined according to the following
equation.

20

Corrected desired floor reaction force horizontal
component without restriction F_{in}
= Full-model floor reaction force horizontal component
 F_{full}
25 + $1/h$

* (Required value M_{pfdmd} of horizontal body position
correcting perturbation model stabilization moment

- Horizontal body position correcting perturbation model
stabilization moment M_{pf})

... Equation h54

where the horizontal body position correcting
5 perturbation model stabilization moment M_{pf} uses a last
time value (the value at time $t - \Delta t$). More specifically,
the difference between the required value M_{pfdmd} of
horizontal body position correcting perturbation model
stabilization moment and the horizontal body position
10 correcting perturbation model stabilization moment M_{pf} is
determined, and the amount of an increase in a full-model
floor reaction force horizontal component F_{full} resulting
from increasing the input of the horizontal body position
correcting perturbation model by the above difference is
15 estimated by dividing the above difference by a body
translational mode floor reaction force ratio h . Further,
the full-model floor reaction force horizontal component
 F_{full} is added thereto so as to estimate the corrected
desired floor reaction force horizontal component without
20 restriction F_{in} .

Subsequently, based on the corrected desired floor
reaction force moment horizontal component without
restriction M_{in} and the corrected desired floor reaction
force horizontal component without restriction F_{in} , a
25 corrected desired floor reaction force moment horizontal
component with restriction M_{ltd} and a corrected desired
floor reaction force horizontal component with restriction

Fltd (about a desired ZMP), which are the values that have added restriction thereto, are determined by a restricting means (restriction processing unit 211) similar to that in the first embodiment such that the aforesaid restrictions (the ZMP restrictive condition and the floor reaction force horizontal component restrictive condition) are satisfied. This processing technique is the same as that in the first embodiment.

In the present embodiment also, the desired floor reaction force moment horizontal component for compliance control is matched with the corrected desired floor reaction force moment horizontal component with restriction Mltd, and the corrected desired floor reaction force horizontal component substantially agrees with the corrected desired floor reaction force horizontal component with restriction Fltd; therefore, the desired floor reaction force moment horizontal component for compliance control and the corrected desired floor reaction force horizontal component substantially satisfy the ZMP restrictive condition and the floor reaction force horizontal component restrictive condition by determining the corrected desired floor reaction force moment horizontal component with restriction Mltd and the corrected desired floor reaction force horizontal component with restriction Fltd as described above.

Subsequently, the horizontal body position correcting perturbation model stabilization moment M_{pf} is determined

by an Mpf calculator 215. More detailedly, the value
obtained by multiplying the value, which is obtained by
subtracting the full-model floor reaction force horizontal
component Ffull from the corrected desired floor reaction
5 force horizontal component with restriction Fltd, by the
gain Kc is integrated by an integrator 215a, and further,
the obtained integrated value is multiplied by the body
translational mode floor reaction force ratio h to
determine the horizontal body position correcting
10 perturbation model stabilization moment Mpf. In other
words, the horizontal body position correcting
perturbation model stabilization moment Mpf is obtained
according to the following equation.

15
$$Mpf = h * \int Kc(Fltd - Ffull)dt \quad \dots \text{Equation h55}$$

Subsequently, by an Mrf calculator 214, the body
posture inclination angle correcting perturbation model
stabilization moment Mrf is determined by subtracting the
20 horizontal body position correcting perturbation model
stabilization moment Mpf and the compensating total floor
reaction force moment horizontal component Mdmdxy from the
corrected desired floor reaction force moment horizontal
component with restriction Mltd. In other words, the body
25 posture inclination angle correcting perturbation model
stabilization moment Mrf is obtained according to the
aforesaid Equation h21.

Furthermore, according to the aforesaid Equation h23, the body posture inclination angle correcting perturbation model floor reaction force moment M_r is determined. In other words, the body posture inclination angle correcting perturbation model stabilization moment M_{rf} , which is an output of the M_{rf} calculator 214, is directly determined as the body posture inclination angle correcting perturbation model floor reaction force moment M_r .

Subsequently, a full-model floor reaction force moment error M_{err} defined by the following equation is calculated by a M_{err} calculator 216.

Full-model floor reaction force moment error M_{err}
= Full-model floor reaction force moment horizontal component M_{fullxy}
- Corrected desired floor reaction force moment horizontal component with restriction M_{ltd}

... Equation h56

Subsequently, an M_p calculator 217 determines the horizontal body position correcting perturbation model floor reaction force moment M_p according to the following equation.

$$M_p = M_{pf} - \int K_m * M_{err} dt \quad \dots \text{Equation h57}$$

This means that the value obtained by multiplying the

full-model floor reaction force moment error M_{err} by an integration gain K_m is integrated by the integrator 217a, and the sign of the integrated value is reversed. Further, the output of the integrator 217a is added to the horizontal body position correcting perturbation model stabilization moment M_{pf} to determine the horizontal body position correcting perturbation model floor reaction force moment M_p .

Subsequently, the horizontal body position correcting perturbation model floor reaction force moment M_p is supplied to the body position correcting perturbation model 202, and a correcting perturbation model body position X_c that balances with the supplied floor reaction force moment horizontal component is calculated.

In addition, the body posture inclination angle correcting perturbation model floor reaction force moment M_r is supplied to a body posture inclination angle correcting perturbation model 203, and the correcting perturbation model body posture inclination angle θ_c that balances with the supplied floor reaction force moment horizontal component is calculated.

The processing up to the above in S3536 is as per PCT/JP03/00435, so that no further explanation will be given.

Further, in the present embodiment, an antiphase arm swing angle moment correcting perturbation model M_a is determined in the antiphase arm swing angle correcting

perturbation model moment determiner 230.

Furthermore, the antiphase arm swing angle correcting perturbation model moment M_a is input to an antiphase arm swing angle correcting perturbation model to determine a
5 correcting perturbation model antiphase arm swing angle θ_{ca} .

The following will explain in detail the operation of the antiphase arm swing angle correcting perturbation model moment determiner 230 in conjunction with Fig. 73,
10 which is a functional block diagram thereof.

First, the required value M_{afdm} of antiphase arm swing angle correcting perturbation model stabilization moment is determined according to an antiphase arm swing angle correcting perturbation model control law. For this
15 purpose, the same control law as that in the first embodiment may be used. Thus, as the control law, the aforesaid Equation h30, for example, may be used.

Then, in a calculator 230g, a corrected desired floor reaction force moment vertical component without
20 restriction M_{inz} is determined by subtracting the last time value (an output of an integrator, which will be discussed later) of the antiphase arm swing correcting perturbation model moment M_a from the sum of the full-model floor reaction force moment vertical component
25 M_{fullz} and the required value M_{afdm} of antiphase arm swing angle correcting perturbation model stabilization moment. Then, in a restricting means (restriction

processing unit) 230h, a restriction is added to the corrected desired floor reaction force moment vertical component without restriction $Minz$ so that it does not exceed a floor reaction force vertical component moment permissible range (that is, passing it through a shown saturation characteristic function), thereby determining the corrected desired floor reaction force moment vertical component with restriction $Mltdz$. Next, the value obtained by subtracting the sum of the full-model floor reaction force moment vertical component $Mfullz$ and the required value $Mafdm$ of antiphase arm swing angle correcting perturbation model stabilization moment from the corrected desired floor reaction force moment vertical component with restriction $Mltdz$ is integrated by an integrator 230i using an integration gain Ka so as to determine the antiphase arm swing angle correcting perturbation model moment Ma , which is output. In addition, the corrected desired floor reaction force moment vertical component with restriction $Mltdz$ is output as the desired floor reaction force moment vertical component for compliance control.

The antiphase arm swing angle correcting perturbation model moment Ma and the desired floor reaction force moment vertical component for compliance control are determined in the antiphase arm swing angle correcting perturbation model moment determiner 230 as described above.

The determined correcting perturbation model body position X_c , the correcting perturbation model body posture inclination angle θ_c , the correcting perturbation model antiphase arm swing angle θ_{ca} , the horizontal body position correcting perturbation model stabilization moment M_{pf} , and the antiphase arm swing angle correcting perturbation model moment M_a are used as the last time values at the next time control cycle (time $t + \Delta t$) as previously described.

The rest of the construction and processing are the same as those of the first embodiment. According to the second embodiment, the same operations and advantages as those of the first embodiment can be obtained.

The second embodiment explained above provides the embodiments of the first to the third inventions and the fifth to the thirteenth inventions in the present invention. In this case, the floor reaction force moment vertical component in the second embodiment corresponds to a control object amount. Further, the floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$ for generating a gait (for full-model correction) in the second embodiment corresponds to the permissible range of a restriction object amount. Further, a motional component of a simplified model gait corresponds to a provisional instantaneous value of a desired motion, and this provisional instantaneous value corrected in S3536 corresponds to the instantaneous value of the desired

motion. In addition, a full model (including an antiphase arm swing angle correcting perturbation model) corresponds to the dynamic model in the invention. And the aforesaid antiphase arm swing angle correcting perturbation model moment M_a corresponds to a perturbation model manipulated variable in the third invention, and the correcting perturbation model antiphase arm swing angle θ_{ca} corresponds to the correction amount of a desired motion in the third invention. Furthermore, the corrected desired floor reaction force moment vertical component without restriction M_{inz} in the second embodiment corresponds to an estimated value of a restriction object amount in the seventh invention, and the antiphase arm swing angle correcting model stabilization moment M_{afdm} corresponds to a required value of a perturbation model manipulated variable. Further, the full-model floor reaction force moment vertical component M_{fullz} in the second embodiment corresponds to the instantaneous value of a model restriction object amount. In the second embodiment, the correction amount of a desired motion (correcting perturbation model antiphase arm swing angle θ_{ca}) is additionally supplied to a full model, which is a dynamic model, as in the ninth invention.

In the second embodiment, M_{afdm} does not steadily become zero; however, if this is steadily set to zero, then an embodiment of the fourth invention in the present invention will be constructed.

A third embodiment according to the present invention will now be explained with reference to Fig. 74 and Fig. 75. The third embodiment is based on a technique that
5 generates a gait while correcting the gait by using a forward dynamic model (to be more precise, a pseudo forward dynamic model) in place of the inverse dynamic full model (inverse full model) 201 used in the aforementioned first and second embodiments.

10 Fig. 74 is a functional block diagram explaining an operation of a device according to the third embodiment. As shown in Fig. 74, the present embodiment is provided with a pseudo forward full model (pseudo forward dynamic full model) 222.

15 The pseudo forward full model 222 receives the required value M_{pfdmd} of horizontal body position stabilization moment, the required value M_{rfdmd} of body posture inclination angle stabilization moment, the required value M_{afdm} of antiphase arm swing angle
20 stabilization moment, a desired ZMP, a desired floor reaction force vertical component, a compensating total floor reaction force moment horizontal component M_{dmdxy} , and the motional states of parts excluding a body 3, such as desired foot position/posture and a desired arm posture,
25 and outputs a desired vertical body position, a desired horizontal body position, a desired body posture inclination angle, a desired antiphase arm swing angle, a

desired floor reaction force moment (a horizontal component and a vertical component) for compliance control as the desired floor reaction force moment about a desired ZMP, and a desired floor reaction force horizontal component. A desired value input of the pseudo forward full model 222 is generated by a desired instantaneous value generator 100b on the basis of a gait parameter determined by a gait parameter determiner 100a, as explained with reference to the aforesaid Fig. 64.

Specifically, the above pseudo forward full model 222 is represented by the functional block diagram of Fig. 75, and the portion encircled by a dashed line in Fig. 75 corresponds to the pseudo forward full model 222. In this functional block diagram, the same functional parts as those in Fig. 72 of the aforementioned second embodiment will use the same reference marks as those in Fig. 72.

A simplified model 200 in Fig. 75 represents not merely represents a dynamic model, but it also represents the processing from S3510 to S3532 of Fig. 66 described above, namely, the processing for calculating (determining) a simplified model gait instantaneous value. Further, in the processing for calculating (determining) a current time gait instantaneous value (the gait instantaneous value of a simplified model) in S3532, as explained in the above first embodiment, the instantaneous value of a gait is generated, setting the model manipulation floor reaction force moment horizontal

component about a desired ZMP to zero, then a
perturbational motion of a body inclination mode that
generates a simplified gait body posture inclination angle
correcting moment M_r (last time value), which corresponds
5 to the body posture inclination angle correcting
perturbation model moment M_r described in the first
embodiment, a perturbational motion of a body
translational mode that generates a simplified model
horizontal body position correcting moment M_p (last time
10 value), which corresponds to the horizontal body position
correcting perturbation model moment M_p described in the
first embodiment, and a perturbational motion of an
antiphase arm swing mode that generates a simplified model
antiphase arm swing angle correcting moment M_a (last time
15 value), which corresponds to the antiphase arm swing angle
correcting perturbation model moment M_a described in the
first embodiment are added thereto. Thus, the
instantaneous value of a gait output by the simplified
model 200 is corrected.

20 To explain more specifically, in the processing of
S3532 of Fig. 66 in the present embodiment, the body
horizontal acceleration obtained by adding, as a
perturbational portion, a body horizontal acceleration
(d^2X_b/dt^2) determined according to an equation in which
25 the second term of the right side of the aforesaid
Equation 03y is equal to M_p (last time value), namely, the
equation of $M_p = m_b \cdot (Z_b - Z_{zmp}) \cdot (d^2X_b/dt^2)$, to the body

horizontal acceleration determined by the simplified model 200 is integrated to the second order from the beginning of the current time gait to current time t , thereby determining the instantaneous value of the horizontal body position at the current time t in S3414 and S3416 of Fig. 57, which constitute subroutine processing thereof. Furthermore, in S3414 of Fig. 57, the body posture inclination angular acceleration obtained by adding, as a perturbational portion, a body posture inclination angular acceleration ($d^2\theta_{by}/dt^2$) determined according to an equation in which the seventh term of the right side of the aforesaid Equation 03y is equal to M_r (last time value), namely, the equation of $M_r = J \cdot d^2\theta_{by}/dt^2$, to the body posture inclination angular acceleration determined by the simplified model 200 is integrated to the second order from the beginning of the current time gait to the current time t , thereby determining the instantaneous value of the body posture inclination angle at the current time t . Furthermore, in S3414 of Fig. 57, the antiphase arm swing angular acceleration obtained by adding, as a perturbational portion, an antiphase arm swing angular acceleration ($d^2\theta_{az}/dt^2$) determined according to an equation in which the eighth term of the right side of the aforesaid Equation 03z is equal to M_a (last time value), namely, the equation of $M_a = J_{az} \cdot d^2\theta_{az}/dt^2$, to the antiphase arm swing angular acceleration determined by the simplified model 200 is integrated to the second order

from the beginning of the current time gait to the current time t , thereby determining the instantaneous value of the antiphase arm swing angle at the current time t .

Supplementally, for the horizontal body position and
5 the body posture inclination angle, the description has been given of the instantaneous values on a sagittal plane; however, the instantaneous values on a lateral plane are also determined in the same manner.

In Fig. 75, the portion beyond the simplified model
10 200 is the portion that carries out the processing that corresponds to the processing of S3536. The processing in S3536 will be explained in detail in conjunction with Fig. 75.

In S3536, first, the horizontal body position a
15 simplified model that has been corrected on the basis of the simplified model horizontal body position correcting moment M_p (to be specific, the last time value in the control cycle at time $(t-\Delta t)$) as described above is output as a desired horizontal body position (a final desired
20 instantaneous value of the horizontal body position at time t) in S3032. Furthermore, a simplified model body posture inclination angle that has been corrected on the basis of a simplified model body posture inclination angle correcting moment M_r (to be specific, the last time value
25 in the control cycle at time $(t-\Delta t)$) is output as a desired body posture inclination angle (a final desired instantaneous value of the body posture inclination angle

at time t). Furthermore, a simplified model antiphase arm swing angle that has been corrected on the basis of a simplified model antiphase arm swing angle correcting perturbation model moment M_a (to be specific, the last time value in the control cycle at time $(t-\Delta t)$) is output as a desired antiphase arm swing angle (a final desired instantaneous value of the antiphase arm swing angle at time t).

More specifically, the final desired horizontal body position and desired body posture inclination angle are determined according to Equation h100, Equation h101, and Equation h102.

Desired horizontal body position = Simplified model
horizontal body position ... Equation h100
Desired body posture inclination angle = Simplified model
body posture inclination angle ... Equation h101
Desired antiphase arm swing angle = Simplified model
antiphase arm swing angle ... Equation h102

Subsequently, the desired horizontal body position (i.e., the simplified model horizontal body position), the desired body posture inclination angle (i.e., the simplified model body posture inclination angle), the desired antiphase arm swing angle (i.e., the simplified model antiphase arm swing angle), and the instantaneous values of the motion variables, such as the desired total

center-of-gravity position, the desired foot position/posture, and the desired arm posture of the simplified model gait, and the instantaneous value of the desired ZMP obtained as described above are input to the
5 aforesaid inverse dynamic full model (inverse full model) 201, and then a floor reaction force horizontal component and a floor reaction force moment (a horizontal component and a vertical component) about the desired ZMP that balance with the motion represented by the input motional
10 variables (i.e., the inverse full model 201 is generated by the motion) are calculated. Thereafter, as in the fourth embodiment, these calculated floor reaction force horizontal component, the floor reaction force moment horizontal component, and the floor reaction force moment
15 vertical component will be referred to as a full-model floor reaction force horizontal component F_{full} , the full-model floor reaction force moment horizontal component M_{fullxy} , and the floor reaction force moment vertical component M_{fullz} .

20 As in the second embodiment, the full-model floor reaction force horizontal component F_{full} is output as a desired floor reaction force horizontal component (a final desired instantaneous value of the floor reaction force horizontal component at time t).

25 The present embodiment is not provided with a body posture inclination angle correcting perturbation model, a horizontal body position correcting perturbation model,

and an antiphase arm swing angle correcting perturbation model. Therefore, the processing that corresponds to the horizontal body position correcting perturbation model control law, the body posture inclination angle correcting perturbation model control law, and the antiphase arm swing angle correcting perturbation model control law is different from that in the second embodiment, as it will be discussed later.

Except for this, after the aforesaid processing, the same processing as that for determining the body posture inclination angle correcting perturbation model moment M_r , the horizontal body position correcting perturbation model moment M_p , and the antiphase arm swing angle correcting perturbation model moment M_a in the second embodiment is carried out until the simplified model body posture inclination angle correcting moment M_r , the simplified model horizontal body position correcting moment M_p , and the simplified model antiphase arm swing angle correcting moment M_a are determined. In other words, the processing of a Min calculator 209, a Fin calculator 210, a restriction processing unit 211 (restricting means), an M_{pf} calculator 215, a M_{err} calculator 216, an M_{rf} calculator 217 (= M_r calculator), and an M_p calculator 214 is the same as that in the second embodiment. Moreover, except for the processing that corresponds to the antiphase arm swing angle correcting perturbation model control law, the processing of a simplified model

antiphase arm swing angle correcting moment determiner 230 is identical to the processing of the antiphase arm swing angle correcting perturbation model moment determiner 230 in the second embodiment. In the present embodiment, Mr, Mp and Ma correspond to the body posture inclination angle correcting perturbation model moment Mr, the horizontal body position correcting perturbation model moment Mp, and the antiphase arm swing angle correcting perturbation model moment Ma, respectively, in the second embodiment; however, unlike the second embodiment, they are input to the simplified model 200 rather than being input to a perturbation model. For this reason, the Mr, Mp and Ma are referred to as the simplified model body posture inclination angle correcting moment, the simplified model horizontal body position correcting moment, and the simplified model antiphase arm swing angle correcting moment.

The simplified model body posture inclination angle correcting moment Mr, the simplified model horizontal body position correcting moment Mp, and the simplified model antiphase arm swing angle correcting moment Ma determined as described above are used as last time values when determining (generating) simplified model gait instantaneous values at the next time control cycle (time $t + \Delta t$), as previously described.

The rest of the construction and processing is the same as that of the second embodiment.

The following will explain the processing for determining the required value Mrfdmd of body posture inclination angle stabilization moment, the required value Mpfdmd of horizontal body position stabilization moment, and the required value Mafdm of antiphase arm swing angle stabilization moment with reference to Fig. 74.

As shown in Fig. 74, the present embodiment is provided with a simplified model 223 separate from the simplified model 200 provided in the pseudo forward full model 222, as previously mentioned. The function of the simplified model 223 in the present embodiment is identical to that of the aforesaid simplified model 200, and the simplified model 223 represents not only a dynamic model but also the processing from S3510 to S3532 of Fig. 66 described above, i.e., the processing for calculating (determining) simplified model gait instantaneous values. The simplified model 223, in actual operation, does not necessarily have to perform all processing from S3510 to S3532 of Fig. 66, as long as it is capable of determining the instantaneous values of body posture inclination angles and the instantaneous values of horizontal body positions.

The following will explain in detail the processing for determining Mpfdmd and Mrfdmd in the present embodiment in conjunction with Fig. 74.

In the present embodiment, the differences in the horizontal body position, the body posture inclination

angle, and the antiphase arm swing angle between the gaits generated using the simplified model 223 and the gaits calculated as described above using the aforesaid pseudo forward dynamic full model 222 are determined by calculators 224, 225 and 228. Then, based on these differences, the required value M_{pfdmd} of horizontal body position stabilization moment, the required value M_{rfdmd} of body posture inclination angle stabilization moment, and the required value M_{afdmd} of antiphase arm swing angle stabilization moment are determined by a feedback control law, such as PID, so as to converge the differences to zero. More specifically, M_{pfdmd} is determined by a horizontal body position stabilization control law 226 composed of a feedback control law on the basis of the difference between the horizontal body position by the simplified model 223 and the horizontal body position by the pseudo forward full model 222. Further, M_{rfdmd} is determined by a body posture inclination angle stabilization control law 227 composed of a feedback control law on the basis of the difference between the body posture inclination angle by the simplified model 223 and the body posture inclination angle by the pseudo forward full model 222. Further, M_{afdmd} is determined by an antiphase arm swing angle stabilization control law composed of a feedback control law on the basis of the difference between the antiphase arm swing angle by the simplified model 223 and the antiphase arm swing angle by

the pseudo forward full model 222. Then, the determined Mpfmdmd, Mrfdmd and Mafmdmd are fed back and input to the aforesaid pseudo forward dynamic full model.

In the present embodiment, the gait generating device
5 100 outputs, as the final desired instantaneous values of
a current time gait, a desired ZMP, a desired floor
reaction force vertical component, desired foot
position/posture, and a desired arm posture or the like,
which are some of inputs to the aforesaid pseudo forward
10 dynamic full model 222, and a desired vertical body
position, a desired horizontal body position, a desired
body posture inclination angle, a desired antiphase arm
swing angle, a desired floor reaction force horizontal
component, and a desired floor reaction force moment (a
15 horizontal component and a vertical component) for
compliance control, which are outputs from the aforesaid
pseudo forward dynamic full model 222.

The third embodiment explained above is capable of
providing the operations and advantages similar to those
20 of the aforementioned second embodiment.

In the aforementioned third embodiment, the required
value Mrfdmd of body posture inclination angle
stabilization moment, the required value Mpfmdmd of
horizontal body position stabilization moment, and the
25 required value Mafmdmd of antiphase arm swing angle
stabilization moment have been input only to the pseudo
forward full model 222. Alternatively, however, Mrfdmd,

Mpfdmd and Mafdmmd may be input to the simplified model 223 or they may be divided and supplied to the simplified model 223 and the pseudo forward full model 222.

5 The third embodiment explained above is the embodiment of twenty-seventh to thirtieth inventions in the present invention. In this case, the floor reaction force moment vertical component in the third embodiment corresponds to a control object amount. The floor reaction force moment vertical component permissible range
10 [Mzmin, Mzmax] for generating gaits (for full-model correction) in the third embodiment corresponds to the permissible range of a restriction object amount. A motional component of a simplified model gait corresponds to a provisional instantaneous value of a desired motion,
15 and the result of correcting this in S3536 corresponds to the instantaneous value of the desired motion. The simplified model 223 and the pseudo forward full model 222 shown in Fig. 74 correspond to a first dynamic model and a second dynamic model in the twenty-seventh invention. The
20 simplified model in Fig. 12, the inverse full model in Fig. 75, and the simplified model 223 in Fig. 74 correspond to a first dynamic model, a second dynamic model, and a third dynamic model, respectively, in the thirtieth invention. The antiphase arm swing angle stabilization moment Mafdmmd
25 in the third embodiment corresponds to the manipulated variable of the floor reaction force moment in the twenty-seventh invention, and this is additionally input to a

full model (a pseudo forward full model).

A fourth embodiment of the present invention will now be explained with reference to Fig. 76. Fig. 76 is a functional block diagram illustrating the operation of a device according to the fourth embodiment of the present invention, specifically, a gait correcting technique in S3536 of the flowchart of Fig. 66. Incidentally, in Fig. 76, the same functional parts as those in the first embodiment or the second embodiment will use the same reference marks as those in Fig. 67 or Fig. 72.

The fourth embodiment is provided with a horizontal body position correcting perturbation model 202, a body posture inclination angle correcting perturbation model 203, and an antiphase arm swing angle correcting perturbation model 231. The fourth embodiment is provided also with three distributors 220, 221, and 241.

The distributors 220, 221, and 241 are all defined as 1-input, 2-output transmission blocks, and they are transmission blocks that determine one output on the basis of an input (e.g., signal processing of a frequency characteristic, a dead-zone characteristic, a saturation characteristic, or the like is carried out on an input to determine one output) and determine the other output such that the sum of the two outputs agrees or substantially agrees with the input.

A body posture inclination angle correcting moment Mr,

which is the value (an output of an Mr calculator 214)
obtained by subtracting a horizontal body position
correcting perturbation model stabilization moment Mpf and
a compensating total floor reaction force moment
5 horizontal component Mdmdxy from a corrected desired floor
reaction force moment horizontal component with
restriction Mltdxy, is supplied to the distributor 220,
and divided into a body posture inclination angle
correcting perturbation model input Mri to be supplied to
10 the body posture inclination angle correcting perturbation
model 203 and a simplified model body posture inclination
angle correcting moment Mrs to be supplied to the
simplified model 200. At this time, the body posture
inclination angle correcting perturbation model input Mri
15 and the simplified model body posture inclination angle
correcting moment Mrs are determined (output) such that
the sum of the body posture inclination angle correcting
perturbation model input Mri and the simplified model body
posture inclination angle correcting moment Mrs agrees
20 with the body posture inclination angle correcting moment
Mr.

To be more specific, the body posture inclination
angle correcting perturbation model input Mri is
determined on the basis of the body posture inclination
25 angle correcting moment Mr. For example, the body posture
inclination angle correcting moment Mr is subjected to the
processing of signals having a dead-zone characteristic, a

saturation characteristic or a frequency characteristic so as to determine body posture inclination angle correcting perturbation model input M_{ri} . The result obtained by subtracting the body posture inclination angle correcting perturbation model input M_{ri} from the body posture inclination angle correcting moment M_r is determined as the simplified model body posture inclination angle correcting moment M_{rs} . To explain more specifically, in the present embodiment, the distributor 220 outputs a low-frequency component (DC component), which is obtained by passing an input (Body posture inclination angle correcting moment $M_r = M_{ltd} - M_{pf} - M_{dmdxy}$) through a low-pass filter, as a simplified model body posture inclination angle correcting moment M_{rs} , and also outputs the component obtained by subtracting M_{rs} from the input (body posture inclination angle correcting moment M_r) as the body posture inclination angle correcting perturbation model input M_{ri} . In this case, the dead-zone characteristic is imparted to the simplified model body posture inclination angle correcting moment M_{rs} , which is the low-frequency component (DC component), such that, in a state wherein an output of the low-pass filter lies within a predetermined range centering around a certain predetermined value, the M_{rs} is maintained at that predetermined value (e.g., zero).

The body posture inclination angle correcting perturbation model input M_{ri} , which is an output of the

distributor 220, is supplied to the body posture inclination angle correcting perturbation model 203, and a correcting perturbation model body posture inclination angle θ_c is determined by the body posture inclination angle correcting perturbation model 203.

The simplified model body posture inclination angle correcting moment M_{rs} , which is the other output of the distributor 220, is supplied to the simplified model 200. This corresponds to supplying the simplified model body posture inclination angle correcting moment M_r to the simplified model 200 in Fig. 75 in the aforementioned third embodiment.

The distributor 221 receives a value obtained by integrating the value, which is obtained by multiplying a full-model floor reaction force moment horizontal component error M_{err} by a gain K_m , by an integrator 217a and reversing the sign thereof.

An input to the distributor 221 is divided into a simplified model horizontal body position correcting moment M_{ps} to be supplied to the simplified model 200 and an error correcting moment M_e to be supplied to a horizontal body position correcting perturbation model 202, as in the case of the distributor 220. To be more specific, an error correcting moment M_e is determined on the basis of an output of the integrator 217a. For instance, the error correcting moment M_e is determined by subjecting an output of the integrator 217a (an input of

the distributor 220) to the processing of signals having a dead-zone characteristic, a saturation characteristic or a frequency characteristic. The result obtained by subtracting the error correcting moment M_e from an output of the integrator 217a is determined as the simplified model body posture inclination angle correcting moment M_{rs} . To explain more specifically, in the present embodiment, the distributor 221 outputs a low-frequency component (DC component), which is obtained by passing an input (an output of the integrator 217a) through a low-pass filter, as a simplified model horizontal body position correcting moment M_{ps} , and also outputs the component obtained by subtracting M_{ps} from the input (the output of the integrator 217a) as the error correcting moment M_e . In this case, the dead-zone characteristic is imparted to the simplified model horizontal body position correcting moment M_{ps} , which is the low-frequency component (DC component), such that, in a state wherein an output of the low-pass filter lies within a predetermined range centering around a certain predetermined value, the M_{ps} is maintained at that predetermined value (e.g., zero).

The horizontal body position correcting perturbation model moment M_p is determined by adding a horizontal body position correcting model stabilization moment M_{pf} to the error correcting moment M_e , which is an output of the distributor 221, by an M_p calculator 217b. Then, the horizontal body position correcting perturbation model

moment M_p is supplied to the horizontal body position
correcting perturbation model 202, and the correcting
perturbation model horizontal body position X_c is
determined by the horizontal body position correcting
5 perturbation model 202.

The simplified model horizontal body position
correcting moment M_{ps} , which is the other output of the
distributor 221, is supplied to the simplified model 200.
This is equivalent to supplying the simplified model
10 horizontal body position correcting moment M_p to the
simplified model 200 in Fig. 75 of the aforementioned
third embodiment.

An antiphase arm swing angle correcting perturbation
model moment determiner 230 is identical to the antiphase
15 arm swing angle correcting perturbation model moment
determiner shown in Fig. 73 used in the second embodiment.
However, the antiphase arm swing angle correcting
perturbation model moment M_a , which is an output shown in
Fig. 73, is supplied to the distributor 241 rather than
20 being directly supplied to the antiphase arm swing angle
correcting perturbation model 231. In the present
embodiment, therefore, the designation of the antiphase
arm swing angle correcting perturbation model moment M_a is
modified to the antiphase arm swing angle correcting model
25 moment M_a .

The distributor 241 receives, as an input, the
antiphase arm swing angle correcting model moment M_a

determined by the antiphase arm swing angle correcting perturbation model moment determiner 230.

As in the case of the distributor 220, an input to the distributor 241 is divided into a simplified model antiphase arm swing angle correcting moment M_{as} to be
5 supplied to the simplified model 200 and an antiphase arm swing angle correcting perturbation model input M_{ai} to be supplied to the antiphase arm swing angle correcting perturbation model 231.

10 At this time, the antiphase arm swing angle correcting perturbation model input M_{ai} and the simplified model antiphase arm swing angle correcting moment M_{as} are determined (output) such that the sum of the antiphase arm swing angle correcting perturbation model input M_{ai} and
15 the simplified model antiphase arm swing angle correcting moment M_{as} agrees with the antiphase arm swing angle correcting model moment M_a .

To be more specific, antiphase arm swing angle correcting perturbation model input M_{ai} is determined on
20 the basis of the antiphase arm swing angle correcting model moment M_a . For example, the antiphase arm swing angle correcting model moment M_a is subjected to the processing of signals having a dead-zone characteristic, a saturation characteristic or a frequency characteristic so
25 as to determine antiphase arm swing angle correcting perturbation model input M_{ai} . The result obtained by subtracting the antiphase arm swing angle correcting

perturbation model input M_{ai} from the antiphase arm swing angle correcting model moment M_a is determined as the simplified model antiphase arm swing angle correcting moment M_{as} . To explain more specifically, in the present embodiment, the distributor 241 outputs a low-frequency component (DC component), which is obtained by passing an input (the antiphase arm swing angle correcting model moment M_a) through a low-pass filter, as a simplified model antiphase arm swing angle correcting moment M_{as} , and also outputs the component obtained by subtracting the M_{as} from the input (antiphase arm swing angle correcting model moment M_a) as the antiphase arm swing angle correcting perturbation model input M_{ai} .

In this case, the dead-zone characteristic is imparted to the simplified model antiphase arm swing angle correcting moment M_{as} , which is the low-frequency component (DC component), such that, in a state wherein an output of the low-pass filter lies within a predetermined range centering around a certain predetermined value, the M_{as} is maintained at that predetermined value (e.g., zero).

The antiphase arm swing angle correcting perturbation model input M_{ai} , which is an output of the distributor 241, is supplied to the antiphase arm swing angle correcting perturbation model 231, and a correcting perturbation model antiphase arm swing angle θ_{ca} is determined by the antiphase arm swing angle correcting perturbation model 231.

The simplified model antiphase arm swing angle correcting moment M_{as} , which is the other output of the distributor 241, is supplied to the simplified model 200. This corresponds to supplying the simplified model antiphase arm swing angle correcting moment M_a to the simplified model 200 in Fig. 75 in the aforementioned third embodiment.

As in the aforesaid third embodiment, the simplified model 200 generates the instantaneous value of a gait such that no floor reaction force moment horizontal component is generated about a desired ZMP (setting the model manipulation floor reaction force moment to zero) in the processing for calculating (determining) the instantaneous value of a simplified model gait, adds a perturbational motion of a body inclination mode that generates a simplified model body posture inclination angle correcting moment M_{rs} (last time value), adds a perturbational motion of a body translational mode that generates a simplified model horizontal body position correcting moment M_{ps} (last time value), and further adds a perturbational motion of an antiphase arm swing mode that generates the simplified model antiphase arm swing angle correcting moment M_{as} , thereby correcting the instantaneous value of the gait.

In the present embodiment, in S800 of Fig. 43, which is a part of the processing of S3528 of Fig. 66, the state amount of a simplified model at the end of the last time gait is used as the terminal state of the last time gait.

Therefore, if there is a moment when Mrs, Mps and Mas
output to a simplified model from the distributors 220,
221, and 241 take values other than zero, then the
behavior of the simplified model deviates from its
5 original behavior, so that gait parameters are corrected
accordingly as necessary in S3528. As the aforesaid dead-
zone area is set to be wider, then the absolute values of
Mrs, Mps, and Mas become smaller, so that the absolute
values of the correction amounts of the gait parameters
10 become also smaller.

The rest of the construction and processing are the
same as those of the second embodiment. More detailedly,
the processing of calculators 204 and 205, a calculator
for calculating a desired horizontal body position, a Merr
15 calculator 216, a body posture inclination angle
correcting perturbation model control law 207, a
horizontal body position correcting perturbation model
control law 206, a Min calculator 209, a Fin calculator
210, a restriction processing unit 211, an Mpf calculator
20 215, and an antiphase arm swing angle correcting
perturbation model moment determiner 240 is the same as
that of the aforementioned second embodiment.

In the present embodiment, it is not necessary to
carry out the processing for correcting the state amount
25 of the simplified model 200 on the basis of the state
amounts of the perturbation models 202, 203, and 231 at
the end of a current time gait or the like as explained in

the aforesaid first embodiment. This is because the simplified model body posture inclination angle correcting moment M_{rs} , the simplified model horizontal body position correcting moment M_{ps} , and the simplified model antiphase arm swing angle correcting moment M_{as} are additionally
5 supplied from the distributors 220, 221, and 241.

In the present embodiment described above is capable of providing the operations and advantages similar to those of the aforesaid second embodiment or the third
10 embodiment.

In the present embodiment, one of the two outputs of each of the distributors 220, 221, and 241 may be set to zero, while the other is matched with an input.

In this case, if, for example, the simplified model
15 body posture inclination angle correcting moment M_{rs} , which is an output of the distributor 220, is set to zero, the simplified model horizontal body position correcting moment M_{ps} , which is an output of the distributor 221, is set to zero, and the simplified model antiphase arm swing
20 angle correcting moment M_{as} , which is an output of the distributor 241, is set to zero, then the same operations and advantages of the second embodiment will be provided (actually, the same construction as that of the second embodiment will be provided).

25 Alternatively, the value obtained by adding the horizontal body position correcting model stabilization moment M_{pf} to the error correcting moment M_e may be

supplied to a third distributor, not shown, and one of the outputs thereof may be supplied to the horizontal body position correcting perturbation model, while the other output may be added to the simplified model horizontal body position correcting moment M_{ps} . In this case, the simplified model horizontal body position correcting moment M_{ps} , which is an output of the distributor 221, may be set to zero. In other words, the distributor 221 may be omitted, and the value obtained by multiplying the full-model floor reaction force moment error M_{err} by the gain K_m may be integrated. The sign of the integrated value may be reversed and added to the horizontal body position correcting model stabilization moment M_{pf} , and the resulting value may be supplied to the third distributor.

The fourth embodiment explained above is the embodiment of first to third inventions, fifth to fifteenth inventions, seventeenth to twenty-fourth inventions, and a twenty-sixth invention in the present invention. In this case, the floor reaction force moment vertical component in the fourth embodiment corresponds to a control object amount. A floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$ for generating gaits (for full-model correction) in the fourth embodiment corresponds to the permissible range of a restriction object amount. A motional component of a simplified model gait corresponds to a provisional

instantaneous value of a desired motion, and the result of correcting this in S3536 corresponds to the instantaneous value of the desired motion. A full model corresponds to the dynamic model in the first to the third inventions and the fifth to the fourteenth inventions. The simplified model and the full model of Fig. 12 correspond to the first dynamic model and the second dynamic model in the fifteenth invention, the seventeenth to the twenty-fourth inventions, and the twenty-sixth invention. And, M_a in the antiphase arm swing angle correcting moment M_a corresponds to the perturbation model manipulated variable in the third invention, and the correcting perturbation model antiphase arm swing angle θ_{ca} corresponds to the correction amount of a desired motion in the third invention. Furthermore, a corrected desired floor reaction force moment vertical component without restriction M_{inz} in the fourth embodiment corresponds to the estimated value of a restriction object amount in the seventh invention, and the antiphase arm swing angle correcting model stabilization moment M_{afdm} corresponds to the required value of a perturbation model manipulated variable. Furthermore, the full-model floor reaction force moment vertical component M_{fullz} in the fourth embodiment corresponds to the instantaneous value of a model restriction object amount. In the fourth embodiment, the correction amount (the correcting perturbation model antiphase arm swing angle θ_{ca}) of a desired motion is

additionally supplied to a full model, which is a dynamic model, as in the ninth invention.

The antiphase arm swing angle correcting moment M_a corresponds to the manipulated variable of a floor
5 reaction force moment in the nineteenth invention, and the simplified model antiphase arm swing angle correcting moment M_{as} in the M_a corresponds to the floor reaction force moment correction amount in the fourteenth invention, and M_{ai} corresponds to the perturbation model manipulated
10 variable in the nineteenth invention. Further, the required value M_{afdm} of the antiphase arm swing angle correcting model stabilization moment in the fourth embodiment corresponds to the required value of a floor reaction force moment manipulated variable, and the
15 correcting perturbation model antiphase arm swing angle θ_{ca} corresponds to the correction amount of a desired motion in the eighteenth invention. Furthermore, a corrected desired floor reaction force moment vertical component without restriction M_{inz} in the fourth
20 embodiment corresponds to the estimated value of a restriction object amount in the twenty-sixth invention, and the antiphase arm swing angle correcting model stabilization moment M_{afdm} corresponds to the required value of a perturbation model manipulated variable.
25 Furthermore, the full-model floor reaction force moment vertical component M_{fullz} in the fourth embodiment corresponds to the instantaneous value of a model

restriction object amount. In the fourth embodiment, the correction amount (the correcting perturbation model antiphase arm swing angle θ_{ca}) of a desired motion is additionally supplied to a full model, which is a dynamic model, as in the eighteenth invention.

In the aforesaid fourth embodiment, $Mafdm$ does not steadily become zero, but if this is steadily set to zero, then it constitutes the embodiment of the fourth invention, the sixteenth invention, and the twenty-fifth invention in the present invention.

In the first to the fourth embodiments explained above, the compensating total floor reaction force moment horizontal component M_{dmx} may be determined on the basis of the state amounts of other postures of the robot 1, such as total center-of-gravity horizontal position/velocity, in place of the body posture angle/angular velocity.

A fourth reference example related to the present invention will now be explained with reference to Fig. 77 to Fig. 84. This fourth reference example is related to a fifth embodiment of the present invention, which will be discussed hereinafter.

The functional block diagram of a control unit 60 in the fourth reference example is shown in Fig. 77. In the present embodiment, the same constituent parts or the same functional parts as those of the aforesaid third reference

example will be assigned the same reference marks as those of the third reference example.

In comparison with the third reference example (refer to Fig. 59), the fourth reference example has added thereto a slippage determiner 114 that determines the presence of slippage of an actual robot 1. A slippage determination result output from the slippage determiner 114 is supplied to a gait generating device 100. The gait generating device 100 narrows a floor reaction force horizontal component permissible range and a floor reaction force moment vertical component permissible range that are determined on the basis of gait parameters if a slippage determination result indicates the presence of a slippage. If a slippage determination result indicates the absence of a slippage, then the gait generating device 100 restores the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range that are determined on the basis of gait parameters. The rest of the construction and processing are the same as those of the aforesaid third reference example.

The slippage determiner 114 will be explained in detail in conjunction with Fig. 80, which is a flowchart illustrating the processing thereof. First, a spin determining subroutine is implemented in S5210. The spin determining subroutine proceeds to S5310 of Fig. 81, which is the flowchart thereof, to determine a ground angular

velocity vertical component ω_{supz} of a supporting leg foot
22 on the basis of an actual body posture angular velocity
and a joint angle command (detection value). Then, the
processing proceeds to S5312 wherein a changing rate
5 $dM_{supactz}/dt$ of a supporting leg floor reaction force
moment vertical component, which is the temporal changing
rate of an actual floor reaction force moment vertical
component acting on the supporting leg is determined on
the basis of a detection value (actual floor reaction
10 force) of a 6-axis force sensor 50 of the foot 22. Next,
the processing proceeds to S5314 wherein it is determined
whether the absolute value of the ground angular velocity
vertical component ω_{supz} of the supporting leg foot 22
exceeds a predetermined value ω_e . If the absolute value
15 exceeds it, then the processing proceeds to S5316 wherein
the changing rate $dM_{supactz}/dt$ of the supporting leg floor
reaction force moment vertical component is divided by the
aforesaid ground angular velocity vertical component ω_{supz}
of the supporting leg foot, and the sign of the obtained
20 value is reversed to determine an apparent torsion spring
constant K_{supt} of the supporting leg. Then, the
processing proceeds to S5318 wherein it is determined
whether K_{supt} is smaller than a predetermined value
 $K_{suptmin}$, and if it is smaller, then the processing
25 proceeds to S5320 wherein the presence of a spin is
determined as a spin determination result, or if it is not,
then the processing proceeds to S5322 wherein the absence

of a spin is determined as the spin determination result. Furthermore, if it is determined in S5314 that the absolute value of the ground angular velocity vertical component ω_{supz} of the supporting leg foot does not exceed the aforesaid predetermined value ω_e , then the processing proceeds to S5324 wherein the absence of a spin is determined as a spin determination result. Determining the presence of a spin as described above makes it possible to avoid such a situation wherein the presence of a spin is erroneously determined when the absolute value of ω_{supz} exceeds the predetermined value ω_e due to flexure (elastic deformation) of the foot 22 or the like.

After finishing the processing of S5210 as described above, the processing proceeds to S5212 wherein a translational slippage determining subroutine is implemented.

The translational slippage determining subroutine proceeds to S5410 of Fig. 82, which is the flowchart thereof, to determine a ground translational velocity horizontal component V_{supxy} of a supporting leg foot 22 on the basis of an actual body posture angular velocity, an acceleration detection value, and a joint angle command (detection value). Then, the processing proceeds to S5412 wherein a changing rate $dF_{supactxy}/dt$ of a supporting leg floor reaction force horizontal component, which is the temporal changing rate of an actual floor reaction force horizontal component acting on the supporting leg is

determined on the basis of a detection value (actual floor reaction force) of the 6-axis force sensor 50 of the foot 22. Next, the processing proceeds to S5414 wherein it is determined whether the absolute value of the ground

5 translational velocity horizontal component V_{supxy} of the supporting leg foot exceeds a predetermined value V_e . If the absolute value exceeds it, then the processing proceeds to S5416 wherein the changing rate $dF_{supactxy}/dt$ of the supporting leg floor reaction force horizontal

10 component is divided by the aforesaid ground translational velocity horizontal component V_{supxy} of the supporting leg foot 22, and the sign of the obtained value is reversed to determine an apparent shear spring constant K_{sups} ($= (-dF_{supactxy}/dt) / V_{supxy}$) of the supporting leg. Then, the

15 processing proceeds to S5418 wherein it is determined whether K_{sups} is smaller than a predetermined value $K_{supsmin}$, and if it is smaller, then the processing proceeds to S5420 wherein the presence of a translational slippage is determined as a translational slippage

20 determination result, or if it is not, then the processing proceeds to S5422 wherein the absence of a translational slippage is determined as the translational slippage determination result. Furthermore, if it is determined in S5414 that the absolute value of the ground translational

25 velocity horizontal component V_{supxy} of the supporting leg foot does not exceed the aforesaid predetermined value V_e , then the processing proceeds to S5424 wherein the absence

of a translational slippage is determined as a translational slippage determination result. Determining the presence of a translational slippage as described above makes it possible to avoid such a situation wherein the presence of a translational slippage is erroneously determined when the absolute value of K_{sups} exceeds the predetermined value $K_{supsmin}$ due to flexure (elastic deformation) of the foot 22 or the like.

After finishing the processing of S5212 as described above, the processing proceeds to S5214 wherein a slippage vibration determining subroutine is implemented.

The slippage vibration determining subroutine proceeds to S5510 of Fig. 83, which is the flowchart thereof, and passes the detection value (a translational force horizontal component and/or a moment vertical component) of the 6-axis force sensor 50 of the foot 22 through a band-pass filter to extract a slippage vibration component. Instead of using the detection value of the 6-axis force sensor 50 of the foot 22, the foot 22 may be provided with a yaw rate sensor, an acceleration sensor or the like to use the detection values thereof. The passing frequency band of the band-pass filter is preset according to the material or the like of the sole of the foot 22 and a floor surface. Then, the processing proceeds to S5512 wherein it is determined whether the absolute value of the size of the detected slippage vibration component exceeds a certain predetermined value A_{mpe} . If the absolute value

exceeds the predetermined value, then the processing proceeds to S5514 wherein a slippage vibration determination result that indicates the presence of a slippage vibration is given. If the absolute value does not exceed it, then the processing proceeds to S5516 wherein a slippage vibration determination result that indicates the absence of a slippage vibration is given.

After finishing the processing of S5214 as described above, the processing proceeds S5216, and if a spin determination result indicates the presence of a spin, or if a translational slippage determination result indicates the presence of a translational slippage, or if a slippage vibration determination result indicates the presence of a slippage vibration, then the processing proceeds to S5218 wherein a slippage determination result, which is an overall determination result, is given to indicate the presence of a slippage. If not, then the processing proceeds to S5220 wherein the slippage determination result, which is the overall determination result, is given to indicate the absence of a slippage. This completes the processing of the slippage determiner 114.

Fig. 78 shows the flowchart of the main routine processing of the gait generating device 100 in the fourth reference example.

In this Fig. 78, from S2310 to S2332, the same processing as that from S2010 to S2032 of the flowchart (Fig. 60) of the third reference example is carried out.

Subsequently, the processing proceeds to S2334 wherein a subroutine for determining a corrected gait instantaneous value is implemented.

5 In the fourth reference example, a corrected gait instantaneous value determining subroutine determines a corrected gait instantaneous value such that a desired ZMP and an antiphase arm swing restoring angular acceleration pattern are corrected so as to approximate them to an original gait, and also a model manipulation floor
10 reaction force moment (a horizontal component and a vertical component) is additionally generated about a corrected desired ZMP. The floor reaction force permissible range is changed according to a slippage determination result. This aspect is different from the
15 third reference example.

Fig. 79 shows the flowchart of the corrected gait instantaneous value determining subroutine. In the corrected gait instantaneous value determining subroutine, the processing from S5100 to S5114 is first carried out in
20 the same manner as that from S2100 to S2112 of Fig. 61, which is the corrected gait instantaneous value determining subroutine of the third reference example. Then, the processing proceeds to S5116 wherein it determines whether the slippage determination result by
25 the aforesaid slippage determiner 114 indicates the presence of a slippage, and if the slippage determination result indicates the presence of a slippage, then the

processing proceeds to S5118 wherein a permissible range
reducing rate att is gradually approximated to zero
(decreased substantially continuously). Incidentally, the
permissible range reducing rate is to take a value from 0
5 to 1. If it is determined in S5116 that the slippage
determination result indicates no slippage, then the
processing proceeds to S5120 wherein the permissible range
reducing rate att is gradually approximated to 1
(increased substantially continuously).

10 Subsequently, the processing proceeds to S5122
wherein F_{xmin} , F_{xmax} , M_{zmin} and M_{zmax} , which are the upper
limit values and the lower limit values of the permissible
ranges of the floor reaction force horizontal component
and the floor reaction force moment vertical component,
15 respectively, determined in S5110 and S5112, are
multiplied by the permissible range reducing rate att so
as to narrow the floor reaction force horizontal component
permissible range and the floor reaction force moment
vertical component permissible range. Hereinafter, the
20 floor reaction force horizontal component permissible
range and the floor reaction force moment vertical
component permissible range determined in this S5122 will
be generically referred to as final floor reaction force
permissible ranges. It is a matter of course that, if the
25 reducing rate is 1, then the final floor reaction force
permissible range agrees with the permissible ranges of
the floor reaction force horizontal component and the

floor reaction force moment vertical component determined in S5110 and S5112 (hereinafter referred to original floor reaction force permissible ranges), and the original floor reaction force permissible ranges will not be narrowed.

5 Fig. 84 shows an example illustrating how the permissible range reducing rate att, the final floor reaction force permissible ranges (specifically, a floor reaction force horizontal component permissible range and a floor reaction force moment vertical component
10 permissible range) change according to slippage determination results.

 If a slippage occurs, the robot 1 may fall unless a gripping state is promptly restored. Hence, if it is determined that a slippage has occurred, then the final
15 floor reaction force permissible range should be quickly narrowed. However, unduly sudden narrowing would lead to an excessive change in acceleration of a gait with a resultant impact; therefore, a proper value that does not lead to a sudden change should be set.

20 If it is determined that there is no longer a slippage, then the final floor reaction force permissible range should be quickly set back to the original floor reaction force permissible range. If the final floor reaction force permissible range remains narrower, then a
25 corrected gait will significantly deviate from an original gait. However, unduly sudden restoration would lead to an excessive change in acceleration of the motion of the gait,

resulting in a slippage again due to an impact; therefore, a proper value that does not cause an unduly sudden restoration should be set.

Subsequently, the processing proceeds to S5124
5 wherein a model manipulation floor reaction force moment horizontal component, a desired floor reaction force moment for compliance control (a horizontal component and a vertical component), a horizontal body acceleration, a body posture inclination angular acceleration, and an
10 antiphase arm swing angular acceleration are determined such that the conditions of the floor reaction force moment horizontal component permissible range, the floor reaction force moment vertical component permissible range, and the floor reaction force horizontal component
15 permissible range are satisfied, as in S2114 of Fig. 61.

Subsequently, the processing proceeds from S5126 to S5128 to carry out the same processing as that of S2116 to S2118 of Fig. 61.

The corrected gait instantaneous value determining
20 subroutine is implemented as described above. Then, the processing proceeds to S2336 of Fig. 77 wherein current time t is incremented by Δt , and returns to S2314 again to continue generating gaits.

The above is the processing of the gait generating
25 device 100 in the fourth reference example.

As described above, in the fourth reference example, the floor reaction force horizontal component permissible

range and the floor reaction force moment vertical component permissible range are changed according to a slippage determination result. Alternatively, however, only one of the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range may be changed.

Generally, if the foot 22 slips parallel on a floor surface (if it slips in a shearing direction), then the gripping force in a spin direction (yaw direction) accordingly decreases. Conversely, if the foot 22 slips in the spin direction (yaw direction), then the foot 22 easily slips parallel on the floor surface. Hence, narrowing (setting to zero) both the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range when either slippage is detected will achieve more effective recovery from the slippage.

The fourth reference example has used, as the gait generating device 100, the one in the aforesaid third reference example; alternatively, however, it may use the gait generating device in any one of the aforesaid first to the fourth embodiments. As described above, in the first to the fourth embodiments, the floor reaction force horizontal component permissible range and the floor reaction force moment vertical component permissible range come in two types, namely, one for simplified model gaits and the other for gait correction (for full-model

correction). All these permissible ranges may be changed. Alternatively, at least the permissible range of either one for gait correction should be changed according to a slippage determination result. In this case, in the

5 aforesaid first embodiment, for example, before implementing the processing of the aforesaid restricting means (restriction processing unit) 211 and 230d, the processing of S5116 to S5122 of Fig. 79 may be implemented to set the permissible range in a variable manner. This

10 constitutes a fifth embodiment. Alternatively, in one of the aforesaid second to the fourth embodiments, before implementing the processing of the processing of the aforesaid restricting means (restriction processing unit) 211 and 230h, the processing of S5116 to S5122 of Fig. 79

15 may be carried out to set the permissible range in a variable manner, thereby constituting the fifth embodiment.

As in the aforesaid first embodiment, the aforesaid fifth embodiment comprised of the aforesaid first embodiment to which variable setting of a permissible

20 range has been applied obviously provides the embodiments of the first to the third inventions, the fifth to the eighth inventions, and the eleventh to the thirteenth inventions in the present invention. In addition, the fifth embodiment also provides the embodiments of the

25 thirty-third to the thirty-sixth inventions. The embodiments comprised of the aforesaid second to the fourth embodiments to which the variable setting of a

permissible range has been applied provide embodiments of the present invention, as in the second to the fourth embodiments, and further provide the embodiments of the thirty-third to the thirty-sixth inventions.

5

In the fourth reference example and the fifth embodiment, as the method for determining slippages, any one of the following may be used in addition to the methods described in the embodiments. Alternatively,
10 these results may be comprehensively determined (using logical operations, including logical sums and products).

1) The angular velocity of the foot 22 with respect to a floor is determined using an angular velocity detector or the like, and if the absolute value of this
15 value exceeds a predetermined value, then it is determined that a slippage has occurred.

2) If the absolute value of a floor reaction force moment of either leg 2 exceeds a predetermined value, then it is determined that a slippage has occurred.

20 3) If the absolute value of a total floor reaction force moment (the moment of the resulting force of the floor reaction forces of both legs 2 and 2) exceeds a predetermined value, then it is determined that a slippage has occurred.

25 4) In a double stance period, if the value obtained by multiplying the ratio of the changing rate of a total floor reaction force moment to a body posture angular

velocity error by (-1) is smaller than a predetermined value (the torsional rigidity when both legs are in contact with the ground), then it is determined that a slippage has occurred.

- 5 5) If the absolute values of detections values (estimated values) of a non-contact type ground velocity or angular velocity detector using a visual sensor, a spatial filter or the like, or of a contact-type ground velocity or angular velocity detector exceed a
10 predetermined value, then it is determined that a slippage has occurred.

Modifications according to the aforementioned first to fifth embodiments will now be explained.

- 15 In the aforesaid first to fifth embodiments, the compensating total floor reaction force moment horizontal component has been determined; alternatively, however, it may be set to zero. In this case, however, full-model correction is used merely to enhance the accuracy of a
20 desired gait based on a simplified model, and the body posture inclination restoring effect provided by correcting a gait by using a full model is not available.

- In the aforementioned first to fifth embodiments, the generation of gaits by the simplified model 200 (the
25 generation of simplified model gaits) may be performed using the gait generating devices according to the first embodiment and the second embodiment in the Japanese

Unexamined Patent Application Publication No. 5-337849
previously proposed by the present applicant. The
correction amount by a full model can be reduced, making
it possible to prevent a corrected gait from significantly
5 deviating from a simplified model gait.

In the aforesaid first to fifth embodiments, if the
sum of the compensating total floor reaction force moment
horizontal component M_{dmdxy} and a model manipulation floor
reaction force moment horizontal component exceeds a floor
10 reaction force moment permissible range, then a desired
floor reaction force moment horizontal component for
compliance control takes an upper limit value or a lower
limit value of the floor reaction force moment horizontal
component permissible range. Alternatively, however, the
15 desired floor reaction force moment horizontal component
for compliance control may be increased or decreased as
the sum of the compensating total floor reaction force
moment horizontal component M_{dmdxy} and a model
manipulation floor reaction force moment horizontal
20 component increases or decreases even if the sum of the
compensating total floor reaction force moment horizontal
component M_{dmdxy} and a model manipulation floor reaction
force moment horizontal component exceeds the floor
reaction force moment horizontal component permissible
25 range. This is because, as the desired floor reaction
force moment horizontal component for compliance control
approximates to a floor reaction force moment horizontal

component permissible range, an actual floor reaction force moment horizontal component controlled by the compliance control tends to be smaller than the desired value, and therefore, even if the desired floor reaction force moment horizontal component for compliance control slightly exceeds a permissible range, it is very likely that this does not immediately cause a problem, such as a deteriorated intrinsic ground contacting property of the foot 22 or floating of the sole of the foot 22.

For the same reason, the floor reaction force moment horizontal component permissible range may be set to exceed a permissible range obtained by converting the range, in which ZMP can exist and which is represented by a supporting polygon (in a strict expression, the permissible range in which actual floor reaction force points of action exist), into moment horizontal components.

Undue dependence on the floor reaction force moment horizontal component produced by compliance control causes a problem, such as a deteriorated intrinsic ground contacting property of the foot 22 or floating of the sole of the foot 22, as described above. Hence, the floor reaction force moment horizontal component permissible range may be said to be the permissible range of actual floor reaction force moment horizontal components that posture control expects of the compliance control.

The floor reaction force moment horizontal component permissible range may alternatively be determined on the

basis of also detected actual floor reaction forces rather than only on the basis of gait parameters. Further, it may be also determined on the basis of detection values of ground contact regions of the foot 22, such as edge position detection values on stairs.

The processing of the main flowchart may be changed so as to implement the correction of a current time gait parameter (the correction of a desired ZMP) in S3028 of Fig. 56 of the second reference example for each control cycle.

If a corrected gait (desired gait) considerably deviates (diverges) from an original gait, it will have excessively deviated (excessively diverged) by the time the gait parameter correction of the next gait is implemented, making it difficult to generate a desired gait that continuously remains stable for long periods simply by correcting gait parameters of the next gait. This problem can be solved to a great extent by correcting the current time gait parameter (by correcting a desired ZMP) for each control cycle.

Furthermore, depending on deviation from an original gait, a foot landing position or landing time of the current time gait may be changed for each control cycle.

Specifically, the processing flow is changed so as to carry out the processing from S3020 to S3030 for each control cycle, and then in S3020, at least one of the next time's gait supporting leg coordinate system (the next

time's gait supporting leg coordinate system corresponding to the next foot landing position/posture), the next but one time's gait supporting leg coordinate system (the next but one time's gait supporting leg coordinate system corresponding to the next but one time foot landing position/posture), the current time gait cycle (the current time gait cycle corresponding to the next foot landing time), and the next time gait cycle (the next time gait cycle corresponding to the cycle of normal gait) may be changed as necessary to reduce the correction of the current time gait parameter in S3028 (the correction of the desired ZMP in particular) (that is, to maintain a high stability allowance of the current time gait).

Furthermore, different gait parameters from those mentioned above may be changed.

The deviation of a corrected gait from an original gait can be estimated, using a dynamic model, primarily from a simplified model body posture inclination angle correcting moment M_r , a simplified model horizontal body position correcting moment M_p , and a simplified model antiphase arm swing angle correcting moment M_a . Hence, based on M_r , M_p and M_a , model behavior deviations may be estimated and gait parameters may be corrected on the basis of the estimated behavior deviations. Alternatively, the relationship between M_r , M_p and M_a and the proper values of gait parameter correction amounts may be determined beforehand and mapped so as to determine the

correction amounts of gait parameters according to the map on the basis of Mr, Mp and Ma.

The processing flow may be changed also for the aforesaid first to fifth embodiments.

5 In addition to the aforementioned conditions, other kinematic conditions and dynamic conditions, e.g., whether joint angles exceed a permissible range, whether legs or the like are interfering, or whether a joint angular velocity or torque is too high, may be added to the
10 restoring conditions described above.

 Accordingly, the following may be added as one of the restoring conditions: if the processing of a main flowchart has been changed so as to implement the correction of a current time gait parameters (the
15 correction of a desired ZMP or a landing position, time or the like) for each control cycle as described above, then the value of the gait parameter, which is changed as necessary to maintain a high stability allowance of a current gait, is set to a proper value (to satisfy a
20 certain restrictive condition).

 The landing position and the landing time determined (read in) at a gait switching point are determined in response to an instruction from a higher control unit (mainly an instruction from a walking plan determiner or
25 from an operator. This is referred to as an original request). Thus, the landing position and the landing time of a corrected gait should be returned to the landing

position and the landing time determined (read in) at the gait switching point as much as possible. For this reason, the landing position and the landing time determined (read in) at the gait switching point may be stored, and the

5 landing position and the landing time of a corrected gait may be matched to or approximated to the stored landing position and landing time as much as possible. This may be added to the restoring conditions. Actually, however, the landing position and the landing time of a corrected

10 gait are arranged so as to gradually return, as much as possible, to the landing position and the landing time determined (read in) at a gait switching point by the aforementioned restoring conditions 4, 5 and 6; therefore, it is not essential to add the above additional condition.

15 Another condition, in which an original request is changed in response to a change of a situation and the gait parameter changed as necessary to maintain a high stability allowance of a gait as described above is matched with or approximated to, as much as possible, a

20 gait parameter that satisfies the changed request, may be added to the restoring conditions. In this case, the aforementioned aforementioned restoring conditions 4, 5 and 6 should be deleted.

25 As the method for determining a model horizontal body position stabilization floor reaction force moment and a model body posture inclination angle stabilization floor reaction force moment that satisfy the various restoring

conditions described above, a linear programming (e.g., simplex method) or a retrieval method for determining optimum values under restrictive conditions may be used. Alternatively, a fuzzy inference may be used.

5 When changing a landing position, a situation wherein obstacles in a walking environment or the like have to be taken into account is conceivable. To make it possible to cope with such a situation, a corrected gait should be determined by also adding the processing that belongs to
10 the field of artificial intelligence, such as recognition of environments and determination of actions.

 The same applies to the method for determining a model antiphase arm swing angle stabilization floor reaction force moment.

15 The block diagrams before and after the limiting means (the restriction processing unit) in the aforementioned first to fifth embodiments may be subjected to equivalent conversion or approximate conversion as shown in, for example, PCT/JP02/13593 by the present
20 applicant.

 In this case, the value obtained by subtracting the value obtained by passing the value, which has been obtained by dividing a horizontal body position correcting model stabilization moment M_{pf} by h , through a low-pass
25 filter from a corrected desired floor reaction force horizontal component (a full-model floor reaction force horizontal component F_{full}) corresponds to a biased

estimated value $destm$ in the above PCT application. Hence, for example, the integration of the gain K_c in the aforementioned second to fourth embodiments may be replaced into a positive feedback system having the first-order lag of a time constant $1/K_c$ as a feedback element to perform the approximate conversion as shown in Fig. 85. In this example, the Mpf calculator 215 in the second to the fourth embodiments is subjected to the approximate conversion as illustrated in the figure.

The antiphase arm swing angle correcting perturbation model moment may be also determined by implementing the equivalent conversion or approximate conversion in the same manner.

In the aforementioned first embodiment, for the aforesaid antiphase arm swing angle correcting perturbation model moment, the processing of the functional block diagram shown in Fig. 86 may be carried out in place of the functional block diagram shown in Fig. 71. This will be explained below, taking this as a sixth embodiment. In Fig. 71, the behavior of an antiphase arm swing angle correcting model has been decided by determining whether a floor reaction force moment vertical component, including the moment vertical component generated by a motion restored by an antiphase arm swing angle correcting model, exceeds a floor reaction force moment vertical component permissible range. In the processing of the functional block diagram shown in Fig.

86, the moment vertical component generated by the motion restored by an antiphase arm swing angle correcting model is ignored in determining whether the floor reaction force moment permissible range is exceeded.

5 The processing of the functional block diagram shown in Fig. 86 will be explained in detail. The sum of a full-model floor reaction force moment vertical component M_{fullz} and a floor reaction force moment vertical component perturbation amount M_{pz} attributable to the
10 correction of a horizontal body position is defined as a corrected desired floor reaction force moment vertical component without restriction M_{inz} , and a restriction is added thereto in the same manner as that shown in Fig. 70 to determine a corrected desired floor reaction force
15 moment vertical component with restriction M_{ltdz} . The corrected desired floor reaction force moment vertical component with restriction M_{ltdz} is output as a desired floor reaction force moment vertical component for compliance control. Furthermore, the value obtained by
20 subtracting the corrected desired floor reaction force moment vertical component without restriction M_{inz} from the corrected desired floor reaction force moment vertical component with restriction M_{ltdz} , i.e., a portion M_{aa} , which is the portion of the corrected desired floor
25 reaction force moment vertical component without restriction M_{inz} that exceeds the floor reaction force moment vertical component permissible range, is determined.

Then, based on the last time value of a correcting
perturbation model antiphase arm swing angle θ_{ca} , a
required value M_{afdm} of antiphase arm swing angle
correcting model stabilization moment is determined
5 according to an antiphase arm swing angle correcting
perturbation model control law using PD control or the
like, and the value (moment) obtained by subtracting the
determined value from M_{aa} is supplied to an antiphase arm
swing angle correcting perturbation model to obtain the
10 correcting perturbation model antiphase arm swing angle
 θ_{ca} .

The transfer functions from M_{aa} to the correcting
perturbation model antiphase arm swing angle θ_{ca} provide
the transfer functions of a low-pass filter.

15 More specifically, in other words, a floor reaction
force moment vertical component (a floor reaction force
moment vertical component without restriction) generated
when the floor reaction force moment vertical component by
the antiphase arm swing angle correcting model is not
20 canceled (excess preventing operation is not performed) is
passed through a restricting means (saturating means) that
restricts it so as not to exceed the floor reaction force
moment vertical component permissible range, thereby
obtaining a desired floor reaction force moment vertical
25 component for compliance control (a corrected desired
floor reaction force moment vertical component with
restriction M_{ltdz}). In addition, the value obtained by

passing the floor reaction force moment vertical component without restriction through a dead-zone means for determining the portion exceeding the floor reaction force moment vertical component permissible range is passed
5 through a low-pass filter (i.e., a high-cut filter) to obtain the correcting perturbation model antiphase arm swing angle θ_{ca} .

The sixth embodiment explained above provides the embodiment of the thirty-first and the thirty-second
10 inventions of the present invention. In this case, the floor reaction force moment vertical component in the sixth embodiment corresponds to a control object amount. The floor reaction force moment vertical component permissible range $[M_{zmin}, M_{zmax}]$ for generating gaits (for
15 full-model correction) in the sixth embodiment corresponds to the permissible range of a restriction object amount. The motional component of a simplified model gait corresponds to the provisional instantaneous value of a desired motion, and the value obtained by correcting this
20 in S3536 corresponds to the instantaneous value of the desired motion. Full models (including an antiphase arm swing angle correcting perturbation model) correspond to the dynamic models in the inventions. And the value
(M_{inz}) obtained by adding the floor reaction force moment
25 vertical component M_{pz} resulting from the correction of a horizontal body position to the full-model floor reaction force moment vertical component M_{fullz} in the sixth

embodiment corresponds to the instantaneous value of a model restriction object amount, and the difference between this and the desired floor reaction force moment vertical component M_{ltdz} for compliance control corresponds to "the deviating portion" in the thirty-first invention.

Supplementally, in the aforementioned second reference example, in addition to the construction described in Japanese Unexamined Patent Application Publication No. 5-337849 proposed by the present applicant, the behaviors of two motion modes having different generating ratios of a floor reaction force horizontal component and the floor reaction force moment horizontal component about a desired ZMP, e.g., the body translational acceleration of the body translational motion mode and the body posture inclination angle acceleration of the body inclination motion mode, are determined such that the translational force horizontal component of a floor reaction force does not exceed the permissible range of floor reaction force horizontal component, thus allowing the actual robot 1 to converge to a corrected desired gait (the gait lastly output from the gait generating device 100). This means that the posture of the actual robot 1 can be stabilized.

The difference between a desired floor reaction force moment horizontal component for compliance control and a

model manipulation floor reaction force moment horizontal component provides a total restoring force.

5 The model manipulation floor reaction force moment horizontal component can take any value, ignoring the range in which a ZMP can exist, so that it is possible to generate an extremely high restoring force.

10 The translational force horizontal component of a floor reaction force does not exceed the permissible range of a floor reaction force horizontal component, making it possible to prevent slippages of the robot 1.

15 A floor reaction force moment vertical component (a desired floor reaction force moment vertical component for compliance control) and eventually an actual floor reaction force moment vertical component do not exceed the permissible range of floor reaction force moment vertical component, making it possible to effect further prevention of slippages of the robot 1.

20 During a period in which a floor reaction force vertical component is zero, that is, during a period in which neither of both legs 2 and 2 is in contact with the ground, posture restoration depending on a body rotation motion mode is carried out without depending on the body translational motion mode, so that the posture restoration is effectively implemented without dependence on the frictional force between a floor and the foot 22.

25 An actual floor reaction force moment can be prevented from unduly increasing, thus making it possible

to prevent or restrain the occurrence of a problem, such as deteriorated intrinsic ground contacting property of the foot 22 or the sole of the foot 22 floating.

A current time gait parameter is determined or
5 changed such that a new current time gait using the terminal state of a corrected gait for one step as its initial state gradually approximates to a normal gait, thus making it possible to continue generating gaits with continuously (long-term) ensured stability.

10 In the aforementioned third reference example, as described above, an original gait and a corrected gait are simultaneously generated, and the corrected gait is corrected to stabilize the posture of the actual robot 1. In addition, if there is still an allowance after
15 generating the floor reaction force moment (a horizontal component and a vertical component) necessary for posture restoration by compliance control, then this allowance is used to converge to the original gait within a possible range. Hence, in addition to the advantages of the second
20 reference example, it is possible to generate a gait that is close to the original gait initially set, i.e., the gait as per an initial request. Thus, if there is a preset travel path, significant deviation from the travel path can be prevented. Furthermore, a priority is given
25 to the convergence of the body posture angle of a corrected gait to the body posture angle of the original gait (originally determined gait) rather than to the

convergence of the horizontal body position of a corrected gait to the horizontal body position of the original gait (originally determined gait), making it possible to restrain a body posture angle from considerably varying.

5 In the aforementioned first to sixth embodiments, the floor reaction force horizontal component permissible range has been set. Alternatively, however, since a floor reaction force horizontal component and the total center-of-gravity horizontal acceleration of the robot carry a
10 proportional relationship, the total center-of-gravity horizontal acceleration of the robot and its permissible range may be used in place of the floor reaction force horizontal component and its permissible range in each of the aforesaid embodiments. Furthermore, a parameter
15 related to the horizontal acceleration trajectory of a part having a behavior close to a total center-of-gravity horizontal trajectory of the robot may be explicitly set. For instance, if the mass of the legs 2 and 2 is
20 sufficiently smaller than the mass of the body 3, then the body horizontal acceleration trajectory and the total center-of-gravity horizontal acceleration trajectory of the robot 1 are substantially identical or have a
25 proportional relationship. Therefore, the body horizontal acceleration and its permissible range may be used in place of a floor reaction force horizontal component and its permissible range.

 Similarly, since a floor reaction force vertical

component and the total angular momentum changing rate
vertical component of the robot carry a proportional
relationship, the total angular momentum changing rate
vertical component of the robot and its permissible range
5 may be used in place of the floor reaction force moment
vertical component and its permissible range in each of
the aforesaid embodiments.

Moreover, when generating gaits for traveling on a
slope (when moving the robot 1 on an inclined floor
10 surface), the floor surface parallel component (the
component parallel to the floor surface) of a
translational floor reaction force, that is, the
permissible range of a frictional force, or the
permissible range of the floor surface parallel component
15 of a total center-of-gravity acceleration (this is
proportional to a frictional force, provided a gravity
component is excluded) may be set in place of the floor
reaction force horizontal component permissible range or
the permissible range of total center-of-gravity
20 acceleration horizontal component. An explanation of, for
example, a case where the permissible range of a floor
surface parallel component (frictional force) of a
translational floor reaction force is set will be given
(this explanation applies also to the case where the
25 permissible range of the floor surface parallel component
of a total center-of-gravity acceleration is set). For
the frictional force, the relationship of Equation c72

given below holds when the inclination angle with respect to the horizontal plane of the floor surface is denoted by θ_f (defined as positive for a slope inclining forward in the direction in which the robot 1 advances). Hence, to
5 generate a gait according to the algorithm similar to that in the aforementioned embodiment, a frictional force permissible range may be converted into a floor reaction force horizontal component permissible range by using the relationship of the Equation c72 so as to set the floor
10 reaction force horizontal component permissible range. In this case, a desired floor reaction force vertical component may be used as the floor reaction force vertical component in Equation c72.

15 Frictional force = Floor reaction force horizontal component * $\cos(\theta_f)$ - Floor reaction force vertical component * $\sin(\theta_f)$... Equation c72

In generating a gait for traveling on a slope (when
20 moving the robot 1 on an inclined floor surface), the component in the direction of floor surface normal line of a floor reaction force moment, i.e., the permissible range of a frictional force moment, may be set in place of a floor reaction force moment vertical component permissible
25 range. For example, the relationship of Equation c73 given below holds for the frictional force moment when the inclination angle with respect to the horizontal plane of

the floor surface is denoted by θ_f (defined as positive for a slope inclining forward in the direction in which the robot 1 advances). Hence, to generate a gait according to the algorithm similar to that in the
5 aforementioned embodiment, this relationship of Equation c73 may be used to calculate the frictional force moment from a floor reaction force moment vertical component and a floor reaction force moment horizontal component, and then the processing may be changed so that this value does
10 not exceed the permissible range of the frictional force moment.

Frictional force moment = Floor reaction force moment
vertical component * $\cos(\theta_f)$ + Floor reaction force moment
15 horizontal component * $\sin(\theta_f)$

... Equation c73

The two motion modes, namely, the body inclination mode and the body translational mode, have been used in
20 the aforementioned embodiment to set the floor reaction force horizontal component and the floor reaction force moment horizontal component about a desired ZMP to proper values; however, different motion modes from them may alternatively be used. In this case, it is not required
25 that one of the motion modes be a motion mode that does not generate a floor reaction force horizontal component. This is because, arbitrary floor reaction force horizontal

component and floor reaction force moment about a desired ZMP can be generated as in the above example by any combination of modes as long as two motion modes that generate a floor reaction force horizontal component and a floor reaction force moment about a desired ZMP at different ratios are used.

Furthermore, a motion mode other than a body posture may be used. However, a motion mode should be selected that permits generation of a large floor reaction force horizontal component or a large floor reaction force moment about a desired ZMP with a minimum of displacement as much as possible.

For instance, a motion mode for swing right and left arms in the same rotational direction or a motion for perturbing the position of a foot not in contact with the ground (floating) may be selected. However, if a free leg trajectory is to be perturbed, the perturbation amount should be reset virtually to zero by immediately before landing so as not to disturb a landing position.

Alternatively, three or more motion modes may be used.

The ratios of generating a floor reaction force horizontal component and a floor reaction force moment about a desired ZMP of at least two of selected modes must be different from each other. Otherwise, in general, no solution of a simultaneous equation will be obtained.

In addition, it is desirable to combine, as much as possible, a motion mode that allows a sufficiently large

change to take place in the floor reaction force moment about a desired ZMP without changing a floor reaction force horizontal component much, and a motion mode that allows a sufficiently large change to take place in the floor reaction force horizontal component without changing a floor reaction force moment about a desired ZMP much.

In other words, it is desirable to combine a motion mode that allows a sufficiently large change to take place in an angular momentum without changing a total center of gravity much and a motion mode that allows a sufficiently large change to take place in the total center of gravity without changing the angular momentum much. This is because displacements in the motion modes will be smaller.

In the aforementioned embodiments, the antiphase arm swing mode has been used to set the floor reaction force moment vertical component to a proper value; however, other motion mode may be used. For example, as explained about the modification of the aforementioned first reference example, the body yaw rotation mode may be used or the body yaw rotation mode and the antiphase arm swing mode may be used in combination.

Further, it is not required that the motion mode used to set the floor reaction force moment vertical component to a proper value be a motion mode that does not generate a floor reaction force horizontal component and a floor reaction force moment horizontal component. For instance, a motion mode for swing a free leg back and forth may be

used. This is because the floor reaction force horizontal component and the floor reaction force moment horizontal component generated by the motion mode can be offset by adjusting the two motion modes, namely, the body inclination mode and the body translational mode.

In an embodiment using the full model, the following models, in addition to the dynamic model (the model of Fig. 12) used in the aforementioned embodiments, may be used as the aforementioned simplified models.

1) A nonlinear model having mass points set on a plurality of links, as shown in Fig. 49 (multi-mass-point model)

2) Three-mass-point model disclosed in Japanese Patent Application No. 2000-352011 by the present applicant

3) One-mass-point model having a mass only in the body

4) Model that ignores the moment of the inertial force generated by a change in the angular momentum about a total center of gravity

5) Separate type model that separately has a partial model representing the relationship between a resultant force of gravity and an inertial force (or a floor reaction force) and a body translational motion, and a partial model representing the relationship between the above resultant force and a body rotational motion. For instance, the mass points shown in Fig. 12 constitute a

partial model indicating the relationship between the
above resultant force and a body translational motion, and
the flywheel shown in Fig. 12 is a partial model
indicating the relationship between the above resultant
5 force and a body rotational motion.

However, for an embodiment in which a simplified
model body posture inclination angle correcting moment is
added to a simplified model, the models of 2), 3) and 4)
above cannot be used.

10 Preferably, a full model basically uses a dynamic
model having a higher approximation accuracy than that of
a simplified model; however, a dynamic model having an
approximation accuracy equivalent to that of a simplified
model may be used.

15 Furthermore, in the embodiments described above, the
block diagrams, the flowcharts, the algorithms and the
like may be subjected to equivalent modifications, such as
changing the order of calculation processing. In addition,
low-pass filters may be inserted, as necessary.

20 The aforementioned embodiments have been explained in
conjunction with bipedal mobile robots; however, the
present invention can be applied also to one-foot or
multi-leg robots having three or more legs.

25 Industrial Applicability

As described above, even in a circumstance in which
the frictional force between a legged mobile robot, such

as a bipedal mobile robot, and a floor surface is small, the present invention usefully permits generation of gaits that enable the robot to smoothly travel without causing a spin of the robot.